

Flood Plain Mapping Study Dunsford Creek

Final Technical Appendices
March 2019



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Appendix A

Modeling Parameters Selection

Hydrology Modeling Parameters Selection
Hydrologic Modeling (Visual OTTHYMO v 2.4
For Flood Plain Mapping Project, City of Kawartha Lakes
(September 2013)

HYDROLOGICAL MODEL (Visual OTTHYMO 2.4)																							
COMMAND and PROPOSED ACTION REQUIRED	PARAMETER	PROPOSED HYDROLOGY FOR DERIVING PARAMETER VALUES																					
STANDHYD (should only be used when catchment area TIMP>20%)	AREA	LiDAR Survey, GIS ARC-HYDRO, will be used to delineate subcatchment areas. The detail is provided at the end of the document–engineer will confirm GIs catchment delineation																					
	XIMP	<p>Directly connected imperviousness to be obtained from SWM reports or site plans. Otherwise, based on a review of the OP, Zoning By-Law and/or air photos to determine land use within the developed area, calculate area-weighted XIMP based on the following table:</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: left;">Land use</th> <th style="text-align: center;">¹XIMP (Roof Leaders to Road)</th> <th style="text-align: center;">²XIMP (Roof Leaders to Lawn)</th> </tr> </thead> <tbody> <tr> <td>Estate Residential (>3/4 Acre Lot)</td> <td style="text-align: center;">0.14</td> <td style="text-align: center;">0.09</td> </tr> <tr> <td>2 Acre Lot (180 ft wide)</td> <td style="text-align: center;">0.11</td> <td style="text-align: center;">0.08</td> </tr> <tr> <td>1½Acre Lot (150 ft wide)</td> <td style="text-align: center;">0.14</td> <td style="text-align: center;">0.09</td> </tr> <tr> <td>1 Acre Lot (130 ft wide)</td> <td style="text-align: center;">0.17</td> <td style="text-align: center;">0.10</td> </tr> <tr> <td>Low Density Residential (1/3 to 3/4 Acre Lot)</td> <td style="text-align: center;">0.23</td> <td style="text-align: center;">0.15</td> </tr> <tr> <td>¾ Acre Lot (110 ft wide)</td> <td style="text-align: center;">0.18</td> <td style="text-align: center;">0.13</td> </tr> </tbody> </table>	Land use	¹ XIMP (Roof Leaders to Road)	² XIMP (Roof Leaders to Lawn)	Estate Residential (>3/4 Acre Lot)	0.14	0.09	2 Acre Lot (180 ft wide)	0.11	0.08	1½Acre Lot (150 ft wide)	0.14	0.09	1 Acre Lot (130 ft wide)	0.17	0.10	Low Density Residential (1/3 to 3/4 Acre Lot)	0.23	0.15	¾ Acre Lot (110 ft wide)	0.18	0.13
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	LOSS	<p>Rainfall loss can be either Halton's Infiltration Method, SCS Modified Curve Number Method or Proportional Loss Coefficient Method when using VO2. <u>However it is proposed to use the SCS Modified Curve Number Method to calculate pervious area losses for the following reasons:</u></p> <ul style="list-style-type: none"> Horton is not recommended for storm durations ≥ 12 hours as predicted flows are often erroneous (may under estimate runoff if rainfall intensity is < sol infiltration capacity rate); Horton's not recommended if there is significant soil variability; Horton's typically used for urban conditions with short duration, high intensity storms (e.g. Chicago distribution) and not much soil variability; and SCS Modified CN Method is generally more suitable for subwatershed studies and master drainage plans. 																																	
	CN	<p>Same approach as NASHYD. This parameter can be "tweaked" during calibration to adjust runoff volume. Typically, the pervious components within a STANDHYD represents lawn or other grassed</p>																																	

		area. The pervious area curve number value should be determined table xx in Appendix xx. If the assumed pervious area is lawn, the following CN values are recommended:																						
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	SLPP	Pervious surface slope measured from site plans, LiDAR DEM, other wise assume 2%.																						
	LGP	Length of pervious overland flow typically set to 40 m, unless can be calculated otherwise.																						
	MNP	Manning’s pervious “n” value determined by looking at tables, otherwise assume 0.25																						
	DPSI	For roads, driveways and roofs typically use value between 0.8 and 1.5 mm, otherwise assume 1.0 mm																						
	SLPI	Impervious surface slope measured from site plan (typically ranges between 0.5% and 2.0% otherwise assume 1%																						
	LGI	Length of impervious overland flow can be measured if subdivision plans available, however, typically best to use $A= 1.5 (LGI)^2$																						
	MNI	Manning’s impervious “n” value determined using tables if nature of impervious surface is known, otherwise assume 0.013.																						
NASHYD	AREA	Same approach as STANDHYD area. NASHYD typically used to model rural catchments with little																						

		or widely distributed development
	CN	<p>CN values are a function of land use and HSG. Use the same table as STANDHYD CN based on the following approach:</p> <ol style="list-style-type: none"> 1. Area-weighted land use and soils data to be calculated using GIS, Soils information must be transformed to hydrologic soil group (HSG) classification using soil texture or reference tables such as Chart H2-6A in MTC Drainage Manual (1986). use chart 1.09 MTO Drainage Manual 1007 2. CN values to be calculated on an area-weighted basis using table 1.1 in Attachment 1. 3. Traditional SCS Curve Number (CN) to be calculated based on area-weighted CN calculations and then must be transformed from CN to CN* using procedure outlined in the VO2 Reference Manual. <p>This parameter can be “tweaked” during calibration to adjust runoff volume.</p>
	IA	Same as STANDHYD (typically set between 1.0 and 5.0 if using CN*) note chart about shows 1 - 10
	N	Number of linear reservoir typically set to 3.0. This parameter can be “tweaked” during calibration to adjust hydrograph “peakness”.
	TP	<p>Time to peak (Tp) is calculated based on time of concentration (Tc). Tp can be “tweaked” during calibration to adjust the hydrograph timing. There are number of different methods used to calculate Tc and/or Tp, including the following:</p> <ul style="list-style-type: none"> • Upland’s Method • Bransby- Williams Method • Airport Method • Watt and Chow Method; and • HYMO Method <p>Typically, Tc is calculated first and then Tp is estimated based on $Tp=(N-1)/N*Tc$ or $Tp=0.67Tc$. Various methods are described in the literature and the VO2 reference manual. It is proposed, however, to use either the Airport method or the Bransby- Williams method. The Airport method is</p>

		to be used when $C < 0.4$ and the Bransby-Williams Method is to be used when $c > 0.4$ (Formula 8.15 and 8.16, 1997 MTO Drainage Manual). Typical c values are provided in table 1.2 in Attachment 1.
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STORM DATA FOR HYDROLOGIC MODEL (VO2)	
RETURN PERIOD RAINFALL DEPTH	Return period rainfall depths to be obtained from local AES climate stations for 2-yr, 5-yr, 10-yr, 25-yr, 50-yr, and 100-yr return periods. Although Lindsay Filtration Plant hydrometric station was discontinued during 1989-90 Environment Canada has maintained the old IDF curves for this station during 2012 updates. Technical committee agreed to maintain these curves to be consistent with City of Kawartha Lakes Technical Standard. An comparison with new Peterborough IDF curves showed a difference of 2-6% and was considered tolerable.
STORM DISTRIBUTION	Storm distributions used in southern Ontario typically consist of AES, SCS Type II and Chicago distributions. Chicago distributions are not generally suitable for subwatershed studies unless the area is very heavily developed. SCS distribution is OK for rural watershed with high rates of runoff generated by summer thunderstorms, but it is based on US conditions. The AES distribution was developed in Canada and is based on statistical analysis using local Canadian climate data. Could compare SCS Type II and AES and select critical distribution for each and/or all subwatersheds. – part of engineering analysis and based on each watershed
STORM DURATION	Depending on the storm distribution selected, storm duration typically ranges between 1 hr and 24 hrs. Could use 6-hr, 12 hr and 24 hr duration for this study and either select the critical duration for each subwatershed or report the highest peak flow for all durations. – part of engineering evaluation and based on each watershed

VO2 MODEL CALIBRATION
The following are some general notes regarding model calibration: <ul style="list-style-type: none"> • Calibration of computer model results in more accurate hydrograph simulation (uncalibrated model can be off by +/- 200%)

- Calibration is not always possible if historical flow and climate data are not available,
- Ideally should have many years of historical data.
- Typically it is only practical to calibrate models for large watershed with available WSC flow data and AES climate data.
- Calibration is not usually possible for small drainage areas (e.g. subdivisions).

The following procedure is proposed for model calibration (if suitable calibration data is available):

1. Obtain historical flow and climate data for selected stations for calibration period.
2. Separate baseflow from event flow data (flows in VO2 usually do not include base flow, unless baseflow constant is added).
3. Select parameter (i.e. CN*, Tp, etc.) values for model based on standard procedures
4. Run calibration events and plot simulate hydrograph with the actual hydrograph,
5. First match hydrograph volume by adjusting the CN* and note the factor by which CN* was adjusted.
6. Determine the Antecedent Precipitation Index (API) for the calibration events (e.g. 10-day API often used)
7. Plot CN* adjustment factor vs API for all calibration events.
8. Select the API corresponding to AMC II and apply this adjustment factor to the “calibrated” model
9. Next match the Tp of the hydrograph to the actual hydrograph for the calibration events.
10. Finally adjust the hydrograph shape and “peakness” by adjusting N (number of linear reservoirs).
11. Run verification events to test the model calibration
12. Using both calibration and verification events, try to establish uncertainty in simulated flows.

GENERAL WATERSHED MAPPING REQUIREMENTS

The following is a list of recommended general watershed mapping requirements:

1. Surficial soil mapping (including HSG)
2. Topography
3. Existing land use
4. Future land use
5. Aquatic and terrestrial natural features (not needed specifically for hydrology or water balance components)
6. Surficial geology

7. Bedrock subsurface

ATTACHMENT 1
PROPOSED CN AND C-VALUE TABLES

- TABLE 1.1 –RUNOFF CURVE NUMBERS FOR SELECTED LAND USES (AMC II)
- TABLE 1.2 –RUNOFF COEFFICIENTS FOR T_p CALCULATIONS

TABLE 1.1 **NOT USED – REFER INSTEAD TO CKL DESIGN GUIDELINES**

Curve Numbers CN (II) and Runoff Coefficients (C) for Various Land Uses

Land Use	CN Values							C Values						
	Hydrologic Soil Group													
	A	AB	B	BC	C	CD	D	A	AB	B	BC	C	CD	D
Commercial Residential	89	91	92	93	94	95	95	.9	.9	.9	.9	.9	.9	.9
High Density Residential	77	81	85	88	90	91	92	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Medium/Low Density Residential	59	67	74	78	82	85	87	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Estate	51	60	68	74	79	82	84	.25	.25	.25	0.25	0.25	0.25	0.25
Crop	64	70	75	79	82	84	85	0.22	0.35	0.40	0.45	0.50	0.55	0.55
Pasture	49	62	69	74	79	82	84	0.10	0.28	0.30	0.35	0.40	0.40	0.40
Woodlot	36	48	60	67	73	74	79	0.08	0.25	0.27	0.29	0.30	0.35	0.35
Open Space	49	59	69	74	79	80	80	.25	.25	.25	.25	.25	.25	.25

CN values AECOM (2010)

C values – CKL Engineering Technical Standards (2007)

Land Use Description	Hydrologic Soil Group (AMC II)						
	A	AB	B	BC	C	CD	D
Industrial Areas (72% Impervious)	81	85	88	90	91	92	
Paved parking lots, Roofs Driveways	98	98	98	98	98	98	98
Streets and Roads							
Paved with curb and storm sewer connection	98	98	98	98	98	98	98
Gravel	76	81	85	87	89	90	91

Adapted from U.S. Soil Conservation Service National Engineering Handbook (1972) and MTO Drainage Manuals.

Cover	<u>Hydrologic Soil Group</u>			
	A	B	C	D
Woods	36	60	73	79
Meadows	46	66	77	82
Cultivated	66	74	82	86
Lawns	56	71	81	85
Impervious areas	100	100	100	100
CVC Check List				

TABLE 1.2

RUNOFF COEFFICIENT FOR T_p CALCULATIONS

Topography and Land Use	SOIL TEXTURE		
	Open Sandy Loam	Loam and Silt Loam	Tight Clay loam and Clay
WOODLAND			
Flat ($\leq 5\%$ slope)	0.08	0.25	0.35
Rolling (5%-10% slope)	0.12	0.30	0.42
Hilly (10%-30% slope)	0.18	0.35	0.52
PASTURE			
Flat ($\leq 5\%$ slope)	0.10	0.28	0.40
Rolling (5%-10% slope)	0.15	0.35	0.45
Hilly (10%-30% slope)	0.22	0.40	0.55
CULTIVATED			
Flat ($\leq 5\%$ slope)	0.22	0.35	0.55
Rolling (5%-10% slope)	0.3	0.45	0.60
Hilly (10%-30% slope)	0.4	0.65	0.70
URBAN AREAS	30% TIMP	50% TIMP	70% TIMP
Flat ($\leq 5\%$ slope)	0.4	0.55	0.65
Rolling (5%-10% slope)	0.5	0.65	0.8

Adaptation from Determination of Runoff from Agricultural Areas (OMAF Publication 52) and MTC Drainage Manual Chapter B (1979).

Runoff coefficients are intended for 5-10 year storms.

TIMP refers to total impervious area.

GIS Portion of Hydrologic Model For Flood Plain Mapping Project

Preliminary Delineating of Catchment Areas within a watershed; (STANDHYD)

1. Obtain elevation data from LiDAR and develop a digital elevation model (DEM)
2. Delineate catchments, using Arc Hydro. A series of steps will be performed using the Terrain Pre Processing Tools;

a) DEM Manipulations - Fill Sinks

The fill sink function fills sinks in a grid. If a cell is surrounded by higher elevation cells, the water is trapped in that cell and cannot flow. The fill sinks function modifies the elevation value to eliminate these problems.

b) Flow Direction

Flow Direction function takes a grid as input, and computes the corresponding flow direction grid. The values of the cells of the flow direction grid indicate the steepest descent from that cell.

c) Flow Accumulations

The flow accumulation function computes the associated flow accumulation grid that contains the accumulated number of cells upstream of a cell, for each cell in the input grid.

d) Stream Definition

The stream definition function takes a flow accumulation grid as input and creates a stream grid for a user-defined threshold. This threshold is defined either as a number of cells or as a drainage area in square kilometres. In general the recommended size for stream threshold definition is 1% of the overall area. The size of the threshold may be increased to reduce the stream network and the number of catchment polygons. The resulting stream grid contains a value of "1" for all the cells in the input grid that have a value greater than the given threshold. All other cells in the stream grid contain no data.

e) *Stream Segmentation*

The stream segmentation function creates a grid of stream segments that have a unique identification. Either a segment may be a head segment, or it may be defined between two segment junctions. All the cells in a particular segment have the same grid code that is specific to that segment.

f) *Catchment Grid Delineation*

The Catchment Grid delineation function creates a grid in which each cell carries a value (grid code) indicating to which catchment the cell belongs. The value corresponds to the value carried by the stream segment that drains that area, defined in the input Link grid.

g) *Catchment Polygon Processing*

The catchment polygon processing function takes as input a catchment grid and converts it into a catchment polygon feature class. The adjacent cells in the grid that have the same grid code are combined in to a single area, whose boundary is then vectorized.

Final output will be one overall watershed polygon and individual catchment polygons that fall within the watershed.

Developing an Impervious Layer; (XIMP)

1. Using a variety of already existing datasets such as SWP Reports, Official Plans, Zoning By-Laws and air photos an impervious layer will be developed in a GIS. The following land use characteristics will be defined;
 - Estate Residential
 - Low Density Residential
 - Medium Density Residential
 - High Density Residential

- Institutional
- Industrial
- Commercial/Business
- Park

Developing a Land use and Hydrologic Soil Group (HSG) layers for CN Calculations;

1. Using a variety of already existing datasets such as ELC and impervious layer created in above step, create a land use layer that has the following land use characteristics defined;

- High Density Residential
- Medium Density Residential
- Low Density Residential
- Estate Residential
- Business/Commercial
- Institutional
- Industrial
- Agriculture - Crops
- Agricultural - Pasture, Shrubs
- Open Space, Lawn, Park, Golf Course, Cemetery
- Woodlot, Forest

- Meadow
- Swamp, Fen, Marsh
- Open Water
- Pits, Quarries
- Other

* Some digitizing might need to take place to define more specific land use characteristics.

2. Create a Hydrologic Soil Group layer through GIS by categorizing the soil groups into the following;

- A - Fine Sand
- AB
- B - Fine Sandy Loam
- BC
- C - Silt Loam
- CD - Clay Loam
- D - Clay

CN Values will then be calculated based on the following approach;

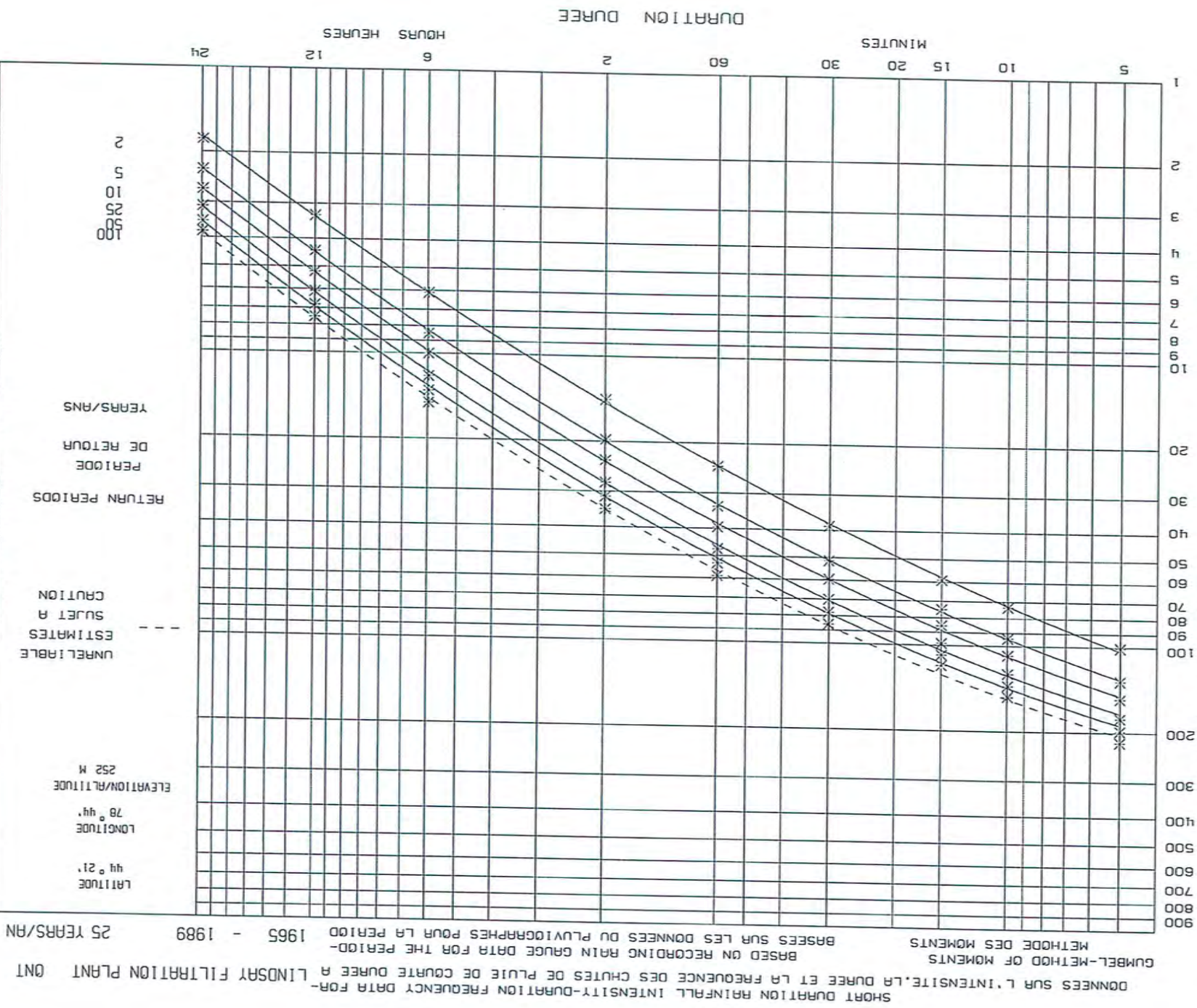
1. Area-weighted land use and soils data will be calculated using GIS. Soils information will be transformed to Hydrologic Soil Group (HSG) classification using soil texture.
2. CN Values will be calculated on area-weighted bases using **Table 1.1 and 1.2 in Attachment 1.**

Appendix B

Rainfall Data

ATMOSPHERIC ENVIRONMENT SERVICE - ENVIRONNEMENT CANADA
 SERVICE DE L'ENVIRONNEMENT ATMOSPHERIQUE - ENVIRONNEMENT CANADA

PREPARED BY - PRÉPARÉ PAR LE



2 5 10 25 50

6164432.txt
 ATMOSPHERIC ENVIRONMENT SERVICE
 SERVICE DE L'ENVIRONNEMENT ATMOSPHERIQUE
 RAINFALL INTENSITY-DURATION FREQUENCY VALUES
 INTENSITE, DUREE ET FREQUENCE DES PLUTES
 DATA INTEGRATION DIVISION
 LA DIVISION DU TRAITEMENT DES DONNEES

GUMBEL - METHOD OF MOMENTS/METHODE DES MOMENTS - 1990

 TABLE 1 LINDSAY FILTRATION PLANT ONT 6164432

LATITUDE	4421	LONGITUDE	7844	ELEVATION/ALTITUDE	252 M				
YEAR	5 MIN	10 MIN	15 MIN	30 MIN	1 H 2 H 6 H 12 H 24 H				
ANNEE									
1965	14.7	21.6	22.9	30.7	31.5	32.5	55.9	56.1	56.1
1966	5.8	6.6	8.9	13.5	20.1	30.2	30.5	30.5	30.5
1967	8.4	11.4	14.5	15.5	15.5	18.5	27.4	27.4	27.4
1968	7.1	14.2	17.3	24.4	41.9	55.1	67.3	67.3	67.3
1969	4.6	7.1	8.1	9.4	12.2	12.4	23.4	23.4	32.5
1970	13.0	17.8	19.8	22.9	25.7	30.0	39.1	39.1	50.5
1971	11.9	13.2	17.0	19.6	27.9	33.5	36.6	37.6	37.6
1972	4.6	6.6	8.9	11.9	11.9	15.0	30.5	33.0	33.0
1973	7.4	14.5	15.0	17.5	19.0	22.4	31.0	31.0	43.9
1974	8.1	12.7	15.5	22.6	35.1	45.5	49.0	56.1	56.1
1975	10.4	15.2	15.5	22.4	22.4	29.0	39.1	39.1	40.1
1976	6.3	9.1	10.2	13.7	23.9	23.9	34.0	38.1	38.1
1977	9.7	12.7	14.7	16.8	21.3	27.7	35.8	43.4	43.9
1978	7.6	13.2	19.8	21.6	25.3	27.7	27.9	34.4	32.8
1979	11.0	13.9	13.9	14.1	14.1	16.6	21.0	34.8	35.2
1980	13.3	15.8	20.2	28.3	51.8	53.9	69.8	70.4	82.8
1981	7.8	15.2	19.8	32.4	33.4	33.7	35.3	36.0	36.0
1982	10.0	16.2	19.0	23.4	36.2	41.8	45.6	45.6	45.6
1983	14.0	18.8	18.8	20.1	23.8	23.9	26.4	27.8	30.9
1984	10.7	12.8	19.2	36.8	44.4	57.6	84.3	84.6	84.7
1985	7.7	12.8	17.3	25.2	27.5	32.4	42.4	42.4	42.4
1986	5.8	6.9	7.1	10.5	13.6	26.8	41.1	42.1	42.1
1987	7.1	8.2	10.3	14.6	17.3	20.7	22.7	22.8	34.1
1988	6.6	12.1	18.2	24.4	24.9	24.9	25.2	25.2	40.0
1989	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	-99.9	48.6

NOTE:-99.9 INDICATES MSG DATA
 INDICATES MANQUANTES

# YRS. ANNEES	24	24	24	24	24	24	24	24	25
MEAN	8.9	12.9	15.5	20.5	25.9	30.4	39.2	42.3	46.0
STD. DEV.	2.9	3.9	4.5	7.1	10.5	12.4	16.1	15.2	14.4
ECART-TYPE	.49	.03	-.51	.45	.79	.90	1.41	1.28	1.58
DISSYMETRIE									
KURTOSIS	2.58	3.14	2.52	3.07	3.55	3.48	4.93	4.70	5.40

NOTE: -99.9 INDICATES LESS THAN 10 YEARS OF DATA AVAILABLE
 INDIQUE MOINS DE 10 ANNEES DE DONNEES DISPONIBLES
 ATMOSPHERIC ENVIRONMENT SERVICE
 SERVICE DE L'ENVIRONNEMENT ATMOSPHERIQUE

6164432.txt

RAINFALL INTENSITY-DURATION FREQUENCY VALUES
INTENSITE, DUREE ET FREQUENCE DES PLUIES

GUMBEL - METHOD OF MOMENTS/METHODE DES MOMENTS - 1990

TABLE 2 LINDSAY FILTRATION PLANT ONT 6164432

LATITUDE 4421 LONGITUDE 7844 ELEVATION/ALTITUDE 252 M

RETURN PERIOD RAINFALL AMOUNTS (MM)
PERIODE DE RETOUR QUANTITIES DE PLUIE (MM)

DURATION DUREE	2 YR/ANS	5 YR/ANS	10 YR/ANS	25 YR/ANS	50 YR/ANS	100 YR/ANS	# YEARS ANNEES
5 MIN	8.4	11.0	12.7	14.9	16.5	18.1	24
10 MIN	12.2	15.7	18.0	20.9	23.1	25.2	24
15 MIN	14.8	18.7	21.3	24.6	27.1	29.5	24
30 MIN	19.3	25.6	29.8	35.1	39.0	42.8	24
1 H	24.1	33.4	39.6	47.3	53.1	58.8	24
2 H	28.4	39.3	46.6	55.8	62.6	69.4	24
6 H	36.6	50.8	60.2	72.1	80.9	89.7	24
12 H	39.8	53.2	62.2	73.4	81.8	90.1	24
24 H	43.6	56.4	64.8	75.4	83.3	91.2	25

RETURN PERIOD RAINFALL RATES (MM/HR) -95% CONFIDENCE ' LIMITS
INTENSITE DE LA PLUIE PAR PERIODE DE RETOUR (MM/H) -LIMITES DE CONFIANCE DE 95%

DURATION DUREE	2 YR/ANS	5 YR/ANS	10 YR/ANS	25 YR/ANS	50 YR/ANS	100 YR/ANS	100 YR/ANS	# YEARS ANNEES
5 MIN	101.0	132.2	152.2	178.9	198.2	198.2	198.2	217.5
10 MIN	+/- 13.0	+/- 21.8	+/- 29.5	+/- 39.7	+/- 47.5	+/- 47.5	+/- 47.5	55.4
15 MIN	+/- 8.7	+/- 14.6	+/- 19.8	+/- 26.7	+/- 31.9	+/- 31.9	+/- 31.9	37.2
30 MIN	+/- 6.5	+/- 11.0	+/- 14.9	+/- 20.1	+/- 24.0	+/- 24.0	+/- 24.0	117.9
1 H	+/- 5.2	+/- 8.8	+/- 11.9	+/- 16.0	+/- 19.2	+/- 19.2	+/- 19.2	22.3
2 H	+/- 3.9	+/- 6.5	+/- 8.8	+/- 11.8	+/- 14.1	+/- 14.1	+/- 14.1	16.5
6 H	+/- 2.3	+/- 3.8	+/- 5.2	+/- 7.0	+/- 8.4	+/- 8.4	+/- 8.4	9.8
12 H	+/- 1.0	+/- 1.7	+/- 2.2	+/- 3.0	+/- 3.6	+/- 3.6	+/- 3.6	4.2
24 H	+/- 0.5	+/- 0.8	+/- 1.1	+/- 1.4	+/- 1.7	+/- 1.7	+/- 1.7	2.0
	+/- 0.2	+/- 0.4	+/- 0.5	+/- 0.7	+/- 0.8	+/- 0.8	+/- 0.8	0.9

ATMOSPHERIC ENVIRONMENT SERVICE
SERVICE DE L'ENVIRONNEMENT ATMOSPHERIQUE

RAINFALL INTENSITY-DURATION FREQUENCY VALUES
INTENSITE, DUREE ET FREQUENCE DES PLUIES

GUMBEL - METHOD OF MOMENTS/METHODE DES MOMENTS - 1990

TABLE 3 LINDSAY FILTRATION PLANT ONT 6164432

LATITUDE 4421 LONGITUDE 7844 ELEVATION/ALTITUDE 252 M

6164432.txt

INTERPOLATION EQUATION / EQUATION D'INTERPOLATION: R = A * T ** B
R = RAINFALL RATE / INTENSITE DE LA PLUIE (MM /HR)
T = TIME IN HOURS / TEMPS EN HEURES

STATISTICS STATISTIQUES	2 YR ANS	5 YR ANS	10 YR ANS	25 YR ANS	50 YR ANS	100 YR ANS
MEAN OF R MOYENNE DE R	35.7	46.7	54.0	63.2	70.1	76.9
STD. DEV. R	35.1	45.4	52.1	60.7	67.1	73.4
ECART-TYPE	9.4	12.4	14.5	17.1	19.0	21.0
STD. ERROR ERREUR STANDARD	20.9	27.8	32.3	38.0	42.3	46.5
COEFF. (A)	- .719	- .713	- .710	- .708	- .706	- .705
EXPONENT (B)	10.4	12.1	13.1	14.1	14.7	15.2
MEAN % ERROR						
% D'ERREUR						

TABLE D-4
TIMMINS - RAINFALL DEPTHS

Hour	Depth		Percent of 12 Hour
	(mm)	Inches	
1st	15	0.6	8
2nd	20	0.8	10
3rd	10	0.4	6
4th	3	0.1	1
5th	5	0.2	3
6th	20	0.8	10
7th	43	1.7	23
8th	20	0.8	10
9th	23	0.9	12
10th	13	0.5	6
11th	13	0.5	7
12th	8	0.3	4
TOTAL	193	7.6	

TABLE D-5
TIMMINS - AREAL REDUCTION

Area (km ²)	Reduction Factor Percentage
0 to 25	100 (no reduction)
26 to 50	97
51 to 75	94
76 to 100	90
101 to 150	87
151 to 200	84
201 to 250	82
251 to 375	79
376 to 500	76
501 to 750	74
751 to 1000	70
1001 to 1250	68
1251 to 1500	66
1501 to 1800	65
1801 to 2100	64
2101 to 2300	63
2301 to 2600	62
2601 to 3900	58
3901 to 5200	56
5201 to 6500	53
6501 to 8000	50

NOTE: Reduction factor to be multiplied by the rainfall.

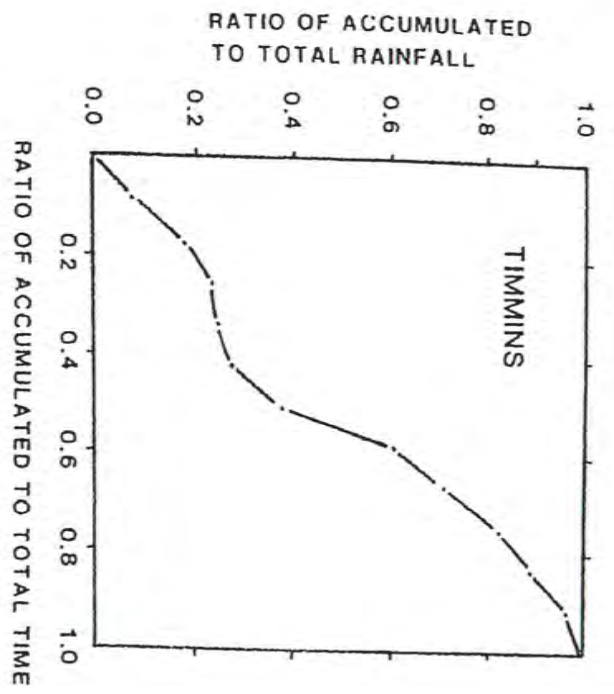
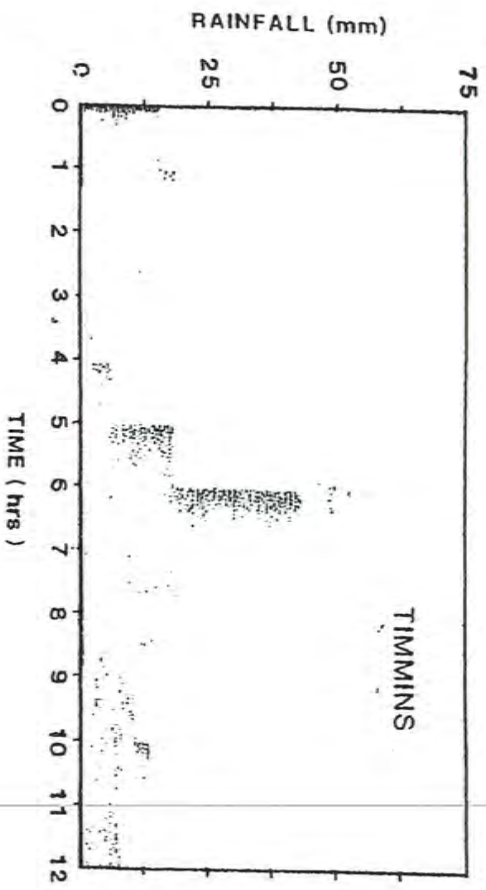


FIGURE D-4
 TIMMINS STORM HYETOGRAPH
 AND DIMENSIONLESS DISTRIBUTION

Design Chart 1.04: Timmins Storm

	Depth		Percent of 12 hour
	(mm)	(inches)	
1st hour	15	0.6	8
2nd hour	20	0.8	10
3rd hour	10	0.4	6
4th hour	3	0.1	1
5th hour	5	0.2	3
6th hour	20	0.8	10
7th hour	43	1.7	23
8th hour	20	0.8	10
9th hour	23	0.9	12
10th hour	13	0.5	6
11th hour	8	0.3	4
12th hour	193	7.6	100

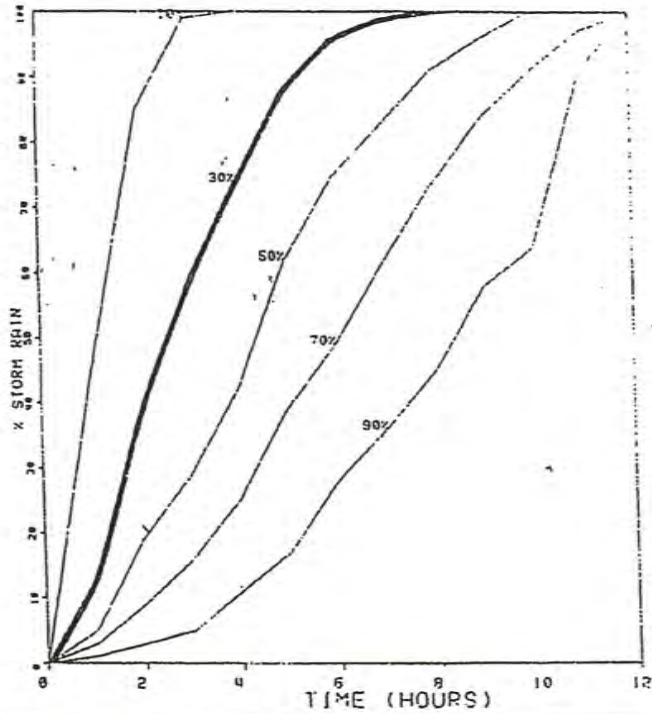
Drainage Area (km ²)	Percentage
0 to 25	100.0
26 to 50	97
51 to 75	94
76 to 100	90
101 to 150	87
151 to 200	84
201 to 250	82
251 to 375	79
376 to 500	76
501 to 750	74
751 to 1000	70
1001 to 1250	68
1251 to 1500	66
1501 to 1800	65
1801 to 2100	64
2101 to 2300	63
2301 to 2600	62
2601 to 3900	58
3901 to 5200	56
5201 to 6500	53
6501 to 8000	50

Source: Ministry of Transportation, MTO (1989)

12 HOUR STORM RAIN DISTRIBUTION
SOUTHERN ONTARIO

NO. OF EVENTS - 145 SELECTION CRITERIA: 6 HR 12 HR
 (MM = 10) ** 10

CURVES SHOW % OF EVENTS WITH ≥ STORM RAIN ≥ VALUES PLOTTED



12 HOUR STORM RAIN DISTRIBUTION
NORTHERN ONTARIO

NO. OF EVENTS - 173 SELECTION CRITERIA: 5 HR 12 HR
 (MM = 10) ** 35

CURVES SHOW % OF EVENTS WITH ≥ STORM RAIN ≥ VALUES PLOTTED

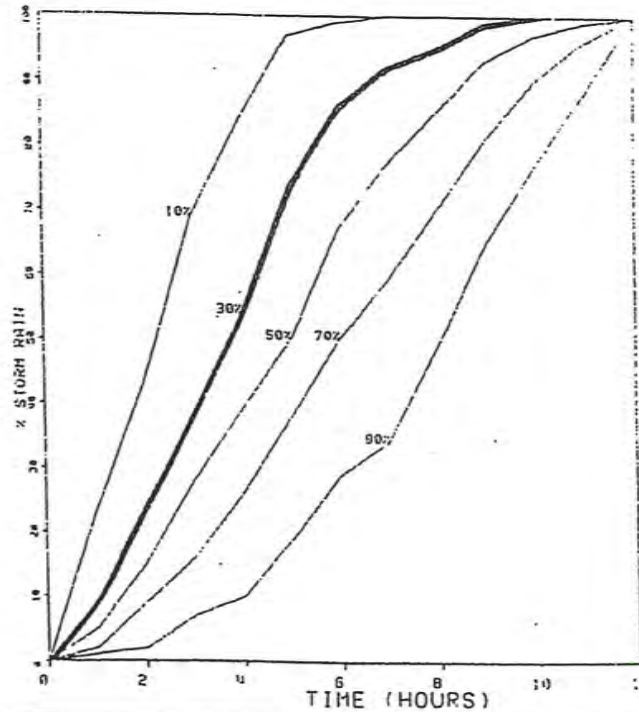


FIGURE D-7

12 - HOUR STORM DISTRIBUTION

TABLE D-8
RAINFALL DISTRIBUTIONS - PERCENT

Type	Reference	Storm Duration												Storm Duration
		1	2	3	4	5	6	7	8	9	10	11	12	HOURS
Probable Maximum Storm	Small Dams	8	9	11	11	49	15	8	-	-	-	-	-	-
HAZEL	Ministry of Natural Resources	3	2	3	6	8	6	11	6	6	25	18	6	
TIMMINS	Ministry of Natural Resources	8	10	6	1	3	10	23	10	12	6	7	4	
Return Period Storms	SCS II	2	3	3	4	6	48	16	6	4	3	3	2	
	AES, 30% Southern Ontario	15	25	22	14	12	8	8	3	1	0	0	0	
	AES, 30% Northern Ontario	8	17	15	14	18	14	6	3	3	1	1	0	

NOTE: A.E.S. distributions represent 70% of all storms for which the accumulated hourly rainfall was equal or less than shown. Consequently, only 30% of the storms had higher accumulated rainfall.
For other distribution see page D-16.

Christie Peacock

From: Jessica Mueller [jmueller@grca.on.ca]
Sent: January-07-14 1:41 PM
To: 'Mark'; 'Christina Sisson'; 'Peter Waring'
Cc: jburgess@kawarthaconservation.com; 'Christie Peacock'; pbuckley@kawarthaconservation.com
Subject: Increased/Decreased precipitation data
Attachments: ComparisonPPTvolume_increase_decrease_commercial/Area_zoom1N.docx

Dear Technical Committee,

As discussed at the last meeting at KC regarding the floodplain mapping study for the Ops Drain #1/Jennings Creek a precipitation sensitivity analyses was carried-out as per the peer reviewer's recommendation. Please find the results attached and kindly review the memo to indicate which rainfall data should be used to generate the floodlines.

In order to meet the timelines determined during the last meeting, direction to staff is required by Friday 17th, 2014.

Thank you,
Jessica

Jessica Mueller

GIS / Engineering Technician
Ganaraska Region Conservation Authority
2216 County Road 28
Port Hope, Ontario
Email: jmueller@grca.on.ca

27/06/2016

Memo regarding increased/decreased rainfall volumes by 10 % of the original values

As mentioned in the previous memo the Peterborough gauge experienced an increase in total rainfall volumes in the years following the decommissioning of the Lindsay station. As shown in the memo sent on Jan 7, 2014 this increase has an impact for the commercial area. Consequently KC staff ran a second analysis comparing rainfall data from the Peterborough station versus the Lindsay station.

The first figure shows a comparison of the resultant rainfall intensities using respective IDF values for the measured and calculated values from the Peterborough station and the measured, calculated and increased values from the Lindsay station. A significant difference of intensities among curves cannot be observed.

The table compares the future flows obtained from PCSWMM for the Chicago 100 yr storm events to evaluate the impact of the rainfall input adjustments. The results show that the flows with the Peterborough rainfall data are generally the same when compared to the original Lindsay gauge rainfall volumes and somewhat lower compared to the values where storm values were increased by 10 %.

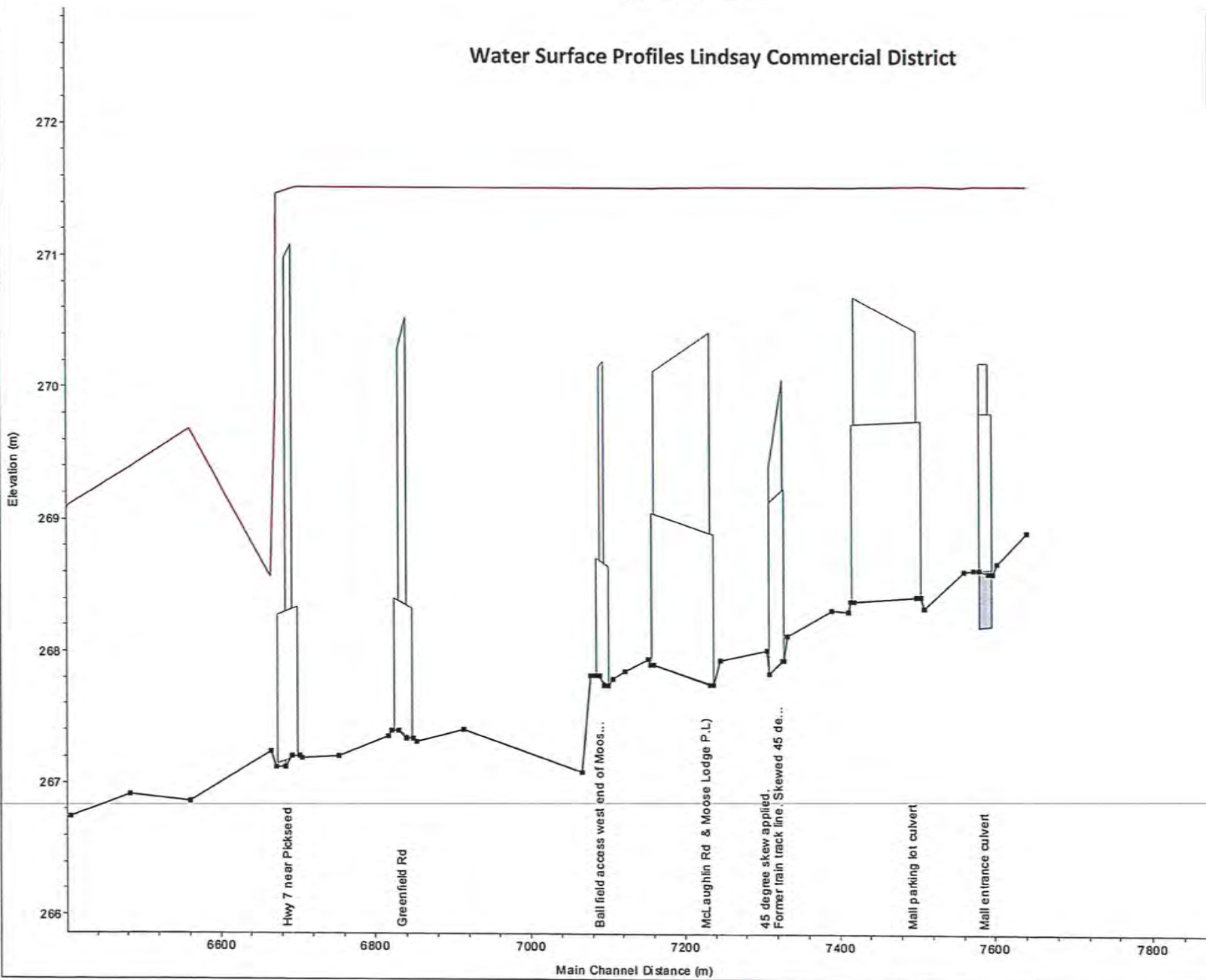
The HEC-Ras profiles compare the differences of water surface elevation generated by the original Lindsay station and the Peterborough station rainfall data, respectively. As can be seen the water surfaces of 271.54 m are identical.

Therefore, staff recommends continue using the original Lindsay station data for the final analyses and report.

1) Peer base 2) P1bo

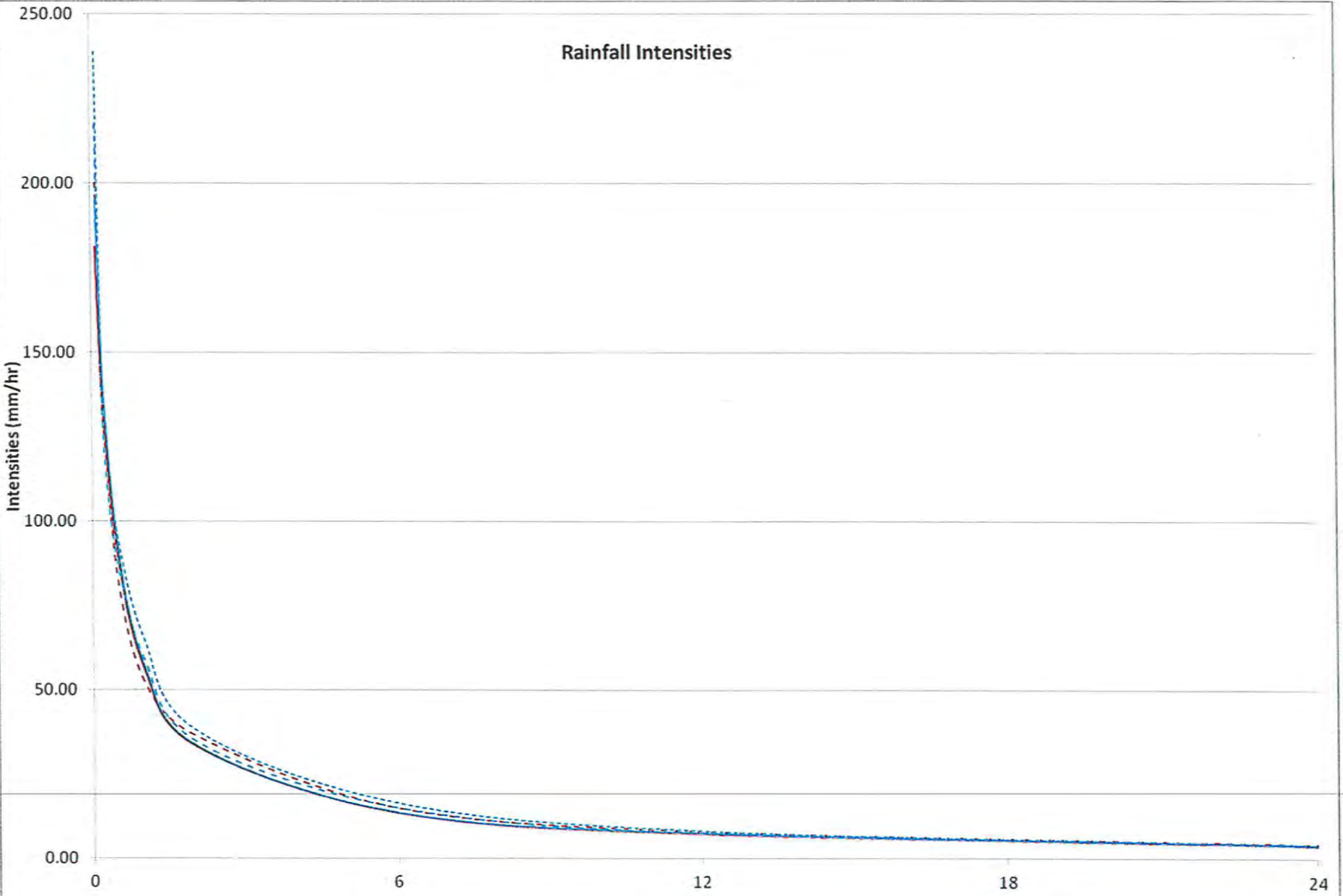
Water Surface Profiles Lindsay Commercial District

Legend	
—	WS 100yr future - Peer base
—	WS 100yr future - P1bo
●	Ground



Future Flows		100yr future		RS
	Ptbo			
7641.424	23.01	21.77	25.83	
7510.949	19.15	18.23	21.24	
7328.619	17.78	17.03	19.43	
7246.49	16.2	15.57	17.72	
7111.02	22.24	21.43	24.57	
6853.017	19.34	18.81	21.66	
6757.544	26.22	25.50	29.23	
6190.578	25.05	24.56	27.33	
5880.376	20.42	20.13	23.63	
5653.55	33.48	33.24	39.43	
5465.266	32.03	31.82	37.12	
4968.21	24.37	24.33	29.26	
4380.968	16.71	16.73	18.65	
3957.179	15.7	15.74	18.64	
3509.864	17.43	17.50	21.32	
3187.848	43.2	42.96	45.55	
2922.176	41.24	41.23	45.01	
1455.968	54.49	54.44	67.37	
273.7271	61.92	61.92	68.19	
154.6483	62.6	62.63	58.09	

Rainfall Intensities



— Calculated Intensities Ptbo - - - Measured Intensities Ptbo — Calculated Intensities Lindsay
- - - Measured Intensities Lindsay ····· Calculated Intensities Lindsay (110%)

Christie Peacock

From: Jessica Mueller [jmueller@grca.on.ca]
Sent: January-15-14 9:59 AM
To: 'Christina Sisson'; 'Mark'; 'Peter Waring'
Cc: jburgess@kawarthaconservation.com; 'Christie Peacock'; pbuckley@kawarthaconservation.com
Subject: Follow up regarding Lindsay/Peterborough station rainfall data
Attachments: MemoComparisonPtboLindsayPPTdata.docx

Greetings!

Please find attached a memo regarding the comparison of the Peterborough versus Lindsay station rainfall data in addition to the memo sent on Jan 7, 2014. This second analysis determines that there is no difference of water surface elevation generated for the area in question if rainfall data of the Lindsay station is compared to the rainfall data recorded at the Peterborough station.

Therefore, staff recommends continuing using the original Lindsay station data for the final report and analyses.

Please kindly discuss these findings and advise staff by Jan 17th, 2014 of your recommendation.

Thank you,

Jessica Mueller
GIS / Engineering Technician
Ganaraska Region Conservation Authority
2216 County Road 28
Port Hope, Ontario
Email: jmueller@grca.on.ca

Memo regarding the use of rainfall data from Lindsay Filtration Plant

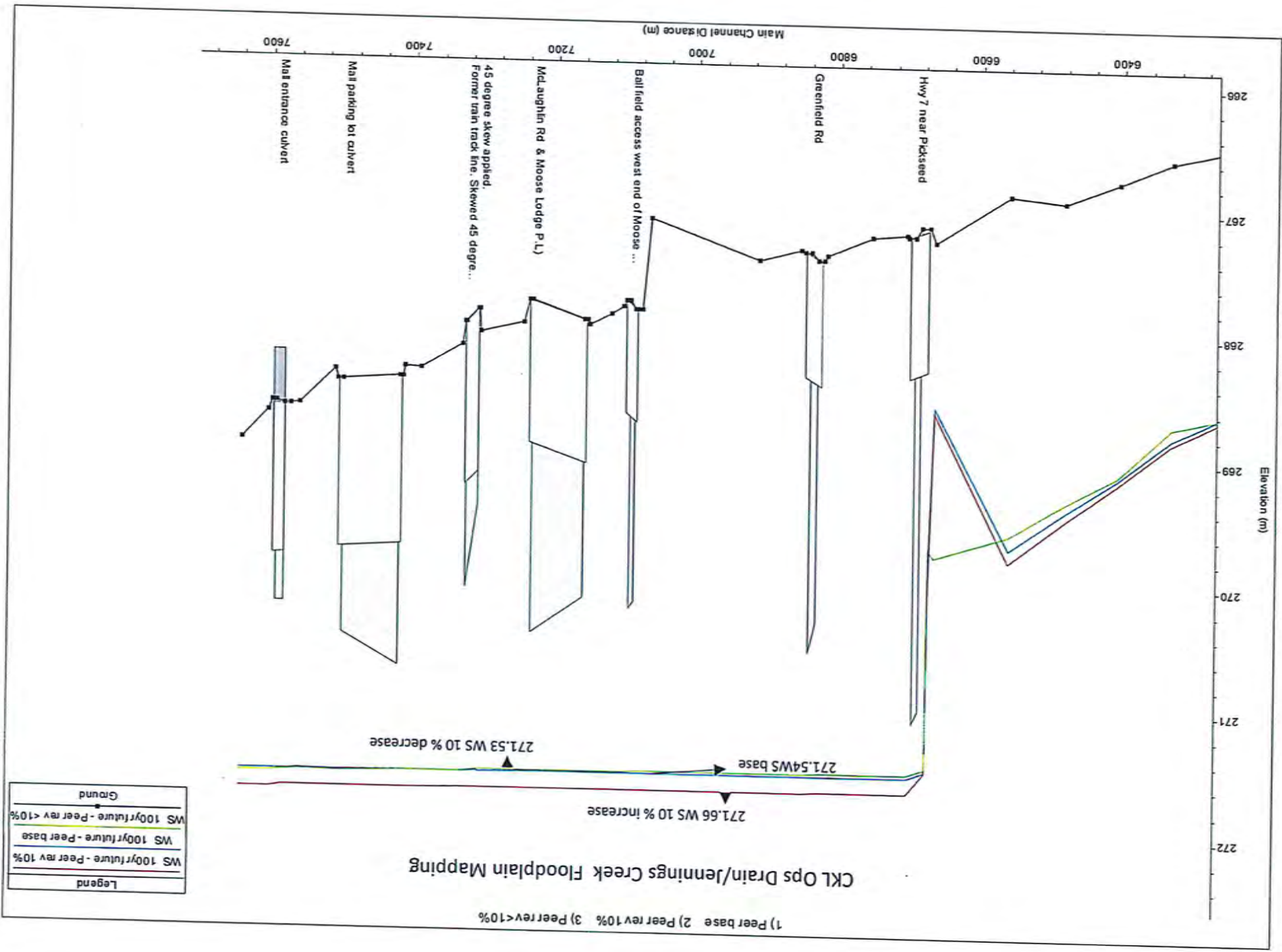
The hydrology peer review compared the Lindsay and Peterborough AES rain gauge data and determined that the Peterborough gauge experienced an increase in total rainfall volumes for the years following the abandonment of the Lindsay rain gauge. The technical committee for the Ops Drain #1/Jennings Creek floodplain model study directed staff to carry out a sensitivity analysis of the precipitation volumes, as per the peer reviewer's recommendation.

Rainfall volumes were reduced/increased by 10% of the original values and input into the PCSWMM hydrology model to determine the subsequent peak flows for the 12-hour Chicago storm. Resultant peak flows were then entered into the static HEC-RAS model. The figures above show a comparison of the calculated floodlines for the three separate scenarios:

- The pink line represents the floodline when storm volumes are increased 10%
- The blue line represents the original Lindsay gauge rainfall volumes
- The green line represents the floodline when storm volumes are decreased 10%

The results show that a difference in water surface elevations in two areas: upstream of Hwy 7, and between Angeline St and Hwy 35. Only the area upstream of Hwy 7 is of concern since at Angeline St. the Timmins storm is the event that determines the floodplain. The effect of the rainfall adjustment is therefore of consequence only for the commercial area. The second figure is a blow-up that indicates the differing water surface elevations: 271.66 m (10% increase), 271.54 m (original Lindsay data) to 271, 53 m (10% decrease).

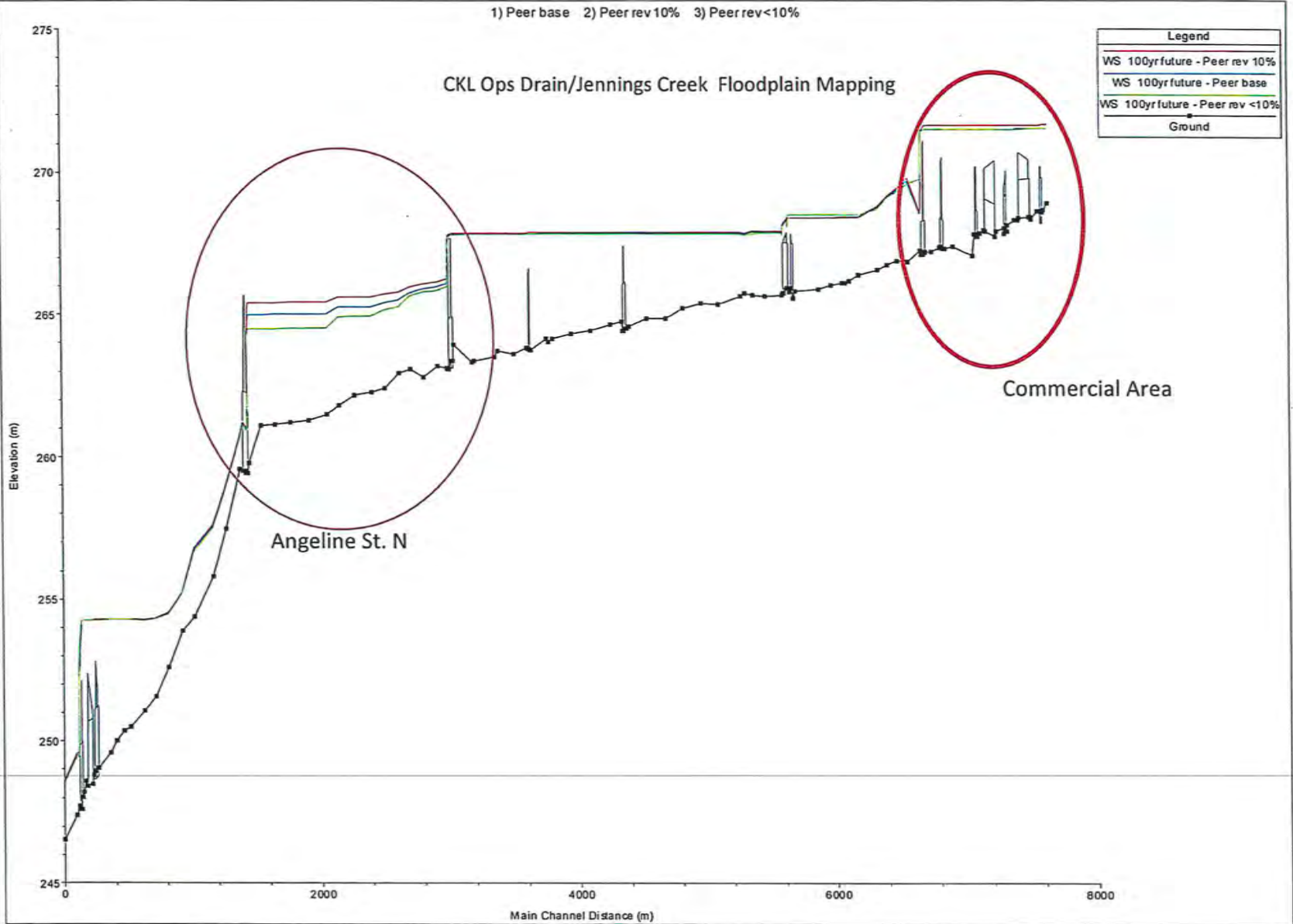
In order to complete the report and maps, staff require direction from the committee whether the base rain data or the 10% increase should be used in the final analyses.



1) Peer base 2) Peer rev 10% 3) Peer rev <10%

CKL Ops Drain/Jennings Creek Floodplain Mapping

Legend	
WS 100yr future - Peer rev 10%	(Red line)
WS 100yr future - Peer base	(Blue line)
WS 100yr future - Peer rev <10%	(Green line)
Ground	(Black line)



Angeline St. N

Commercial Area

Elevation (m)

Main Channel Distance (m)

Lindsay AES Data (comparing to Aecom report)

Intensity Values in AES 1965-1989

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	101.0	132.2	152.8	178.9	198.2	217.5
10	73.3	94.2	108.1	125.6	138.5	151.4
15	59.1	74.8	85.3	98.4	108.2	117.9
30	38.7	51.3	59.6	70.1	77.9	85.7
60	24.1	33.4	39.6	47.3	53.1	58.8
120	14.2	19.7	23.3	27.9	31.3	34.7
360	6.1	8.5	10.0	12.0	13.5	14.9
720	3.3	4.4	5.2	6.1	6.8	7.5
1440	1.8	2.3	2.7	3.1	3.5	3.8

Provided from AES

Return Period	2-year	5-year	10-year	25-year	50-year	100-year
a	20.9	27.8	32.3	38	42.3	46.5
b	-0.719	-0.713	-0.710	-0.708	-0.706	-0.705

Calculated Rainfall Intensities using a, b from AES rainfall

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	124.8	163.5	188.5	220.7	244.5	268.1
10	75.8	99.7	115.3	135.1	149.9	164.5
15	56.6	74.7	86.4	101.4	112.6	123.6
30	34.4	45.6	52.8	62.1	69.0	75.8
60	20.9	27.8	32.3	38.0	42.3	46.5
120	12.7	17.0	19.7	23.3	25.9	28.5
360	5.8	7.7	9.1	10.7	11.9	13.1
720	3.5	4.7	5.5	6.5	7.3	8.1
1440	2.1	2.9	3.4	4.0	4.5	4.9

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	124%	124%	123%	123%	123%	123%
10	103%	109%	107%	108%	108%	109%
15	96%	100%	101%	103%	104%	105%
30	89%	89%	89%	89%	89%	88%
60	87%	83%	82%	80%	80%	80%
120	89%	86%	85%	83%	83%	82%
360	94%	91%	89%	89%	88%	88%
720	106%	107%	106%	107%	108%	108%
1440	118%	125%	125%	129%	128%	130%

average = 101%
median = 96%
min = 87%
max = 124%

Calculated Rainfall Intensities using a, b, c from IDF-fit spreadsheet:

a = 808.299 1248.097 1486.792 1917.848 2142.007 2465.522
b = 7.413 9.760 10.44 11.842 12.182 12.897
c = 0.835 0.857 0.859605 0.872971 0.871993 0.879

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	98.7	124.2	141.8	163.0	179.4	195.2
10	74.4	96.7	111.4	129.9	143.6	157.2
15	60.2	79.7	92.4	108.5	120.3	132.1
30	39.3	53.1	62.0	73.7	82.0	90.5
60	24.0	32.8	38.5	45.9	51.3	56.8
120	14.1	19.3	22.7	27.0	30.3	33.5
360	5.8	7.9	9.3	10.9	12.3	13.5
720	3.3	4.4	5.2	6.1	6.8	7.5
1440	1.9	2.4	2.9	3.3	3.7	4.1

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	98%	94%	93%	91%	91%	90%
10	101%	103%	103%	103%	104%	104%
15	102%	107%	108%	110%	111%	112%
30	101%	104%	104%	105%	105%	105%
60	100%	98%	97%	97%	97%	97%
120	99%	98%	97%	97%	97%	97%
360	96%	92%	93%	91%	91%	91%
720	100%	100%	99%	99%	100%	100%
1440	103%	106%	106%	107%	107%	108%

average = 100%
median = 100%
min = 96%
max = 103%

Used in 2010 Aecom Report (CKL Engineering Standards)

Return Period	2-year	5-year	10-year	25-year	50-year	100-year
a	628.107	820.229	915.845	1041.821	1139.702	1230.783
b	5.3	6.0	6.0	6.0	6.0	6.0
c	0.78	0.768	0.757	0.748	0.743	0.738

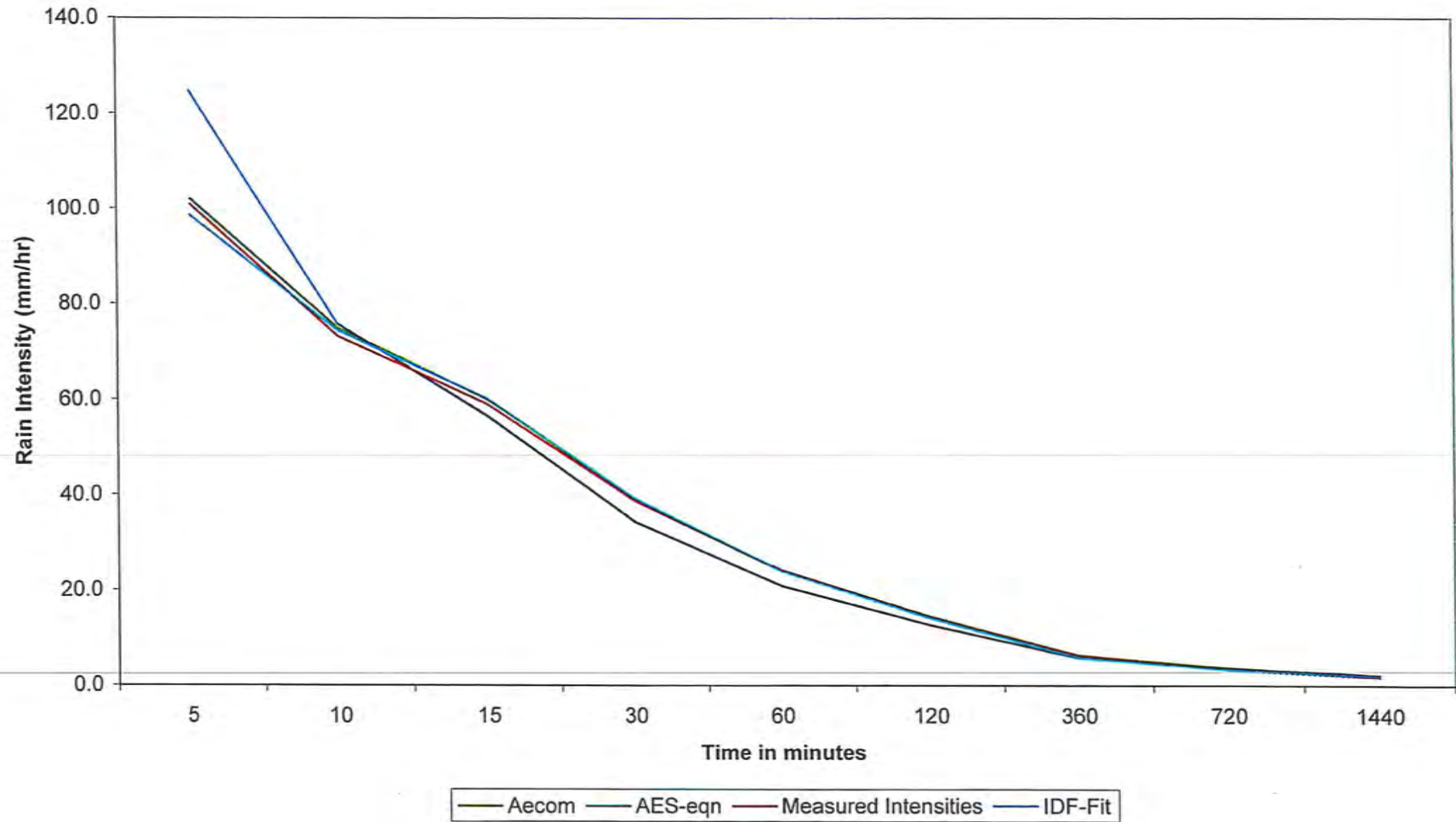
Calculated Rainfall Intensities using a, b, c from Aecom Report

Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	102.1	130.0	149.0	173.0	191.6	209.4
10	74.9	97.5	112.2	130.8	145.1	158.9
15	60.1	79.1	91.4	106.8	118.6	130.0
30	39.0	52.3	60.8	71.4	79.5	87.4
60	24.1	32.8	38.4	45.4	50.7	55.9
120	14.5	20.0	23.5	28.0	31.3	34.7
360	6.3	8.8	10.5	12.6	14.2	15.8
720	3.7	5.2	6.3	7.5	8.5	9.5
1440	2.2	3.1	3.7	4.5	5.1	5.7

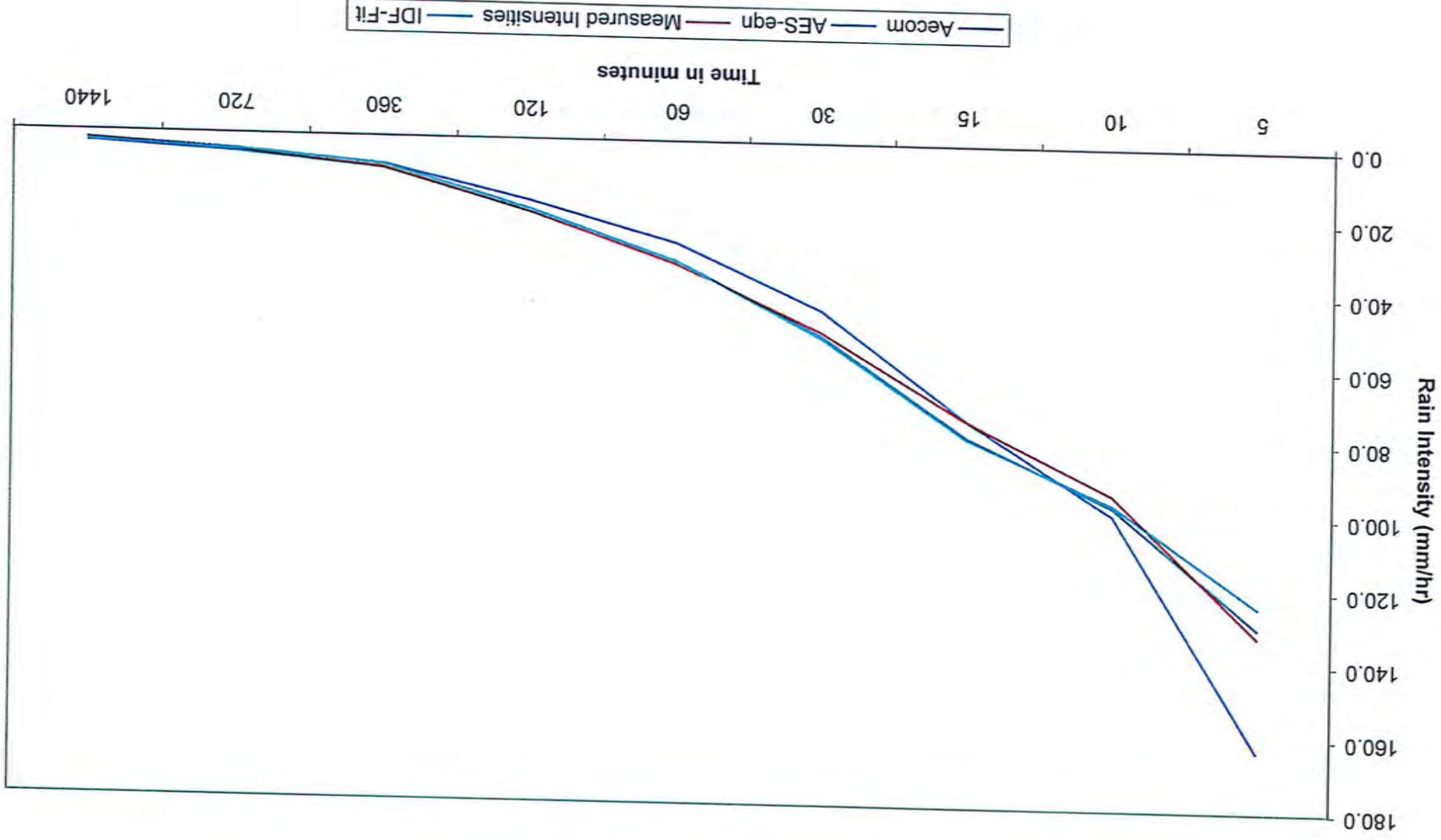
Minutes	Rainfall Intensity (mm/hr)					
	2-year	5-year	10-year	25-year	50-year	100-year
5	101%	98%	98%	97%	97%	96%
10	102%	103%	104%	104%	105%	105%
15	102%	106%	107%	108%	110%	110%
30	101%	102%	102%	102%	102%	102%
60	100%	98%	97%	96%	95%	95%
120	102%	101%	101%	100%	100%	100%
360	103%	104%	105%	105%	105%	106%
720	112%	118%	120%	124%	125%	127%
1440	120%	133%	137%	145%	146%	151%

average = 105%
median = 102%
min = 100%
max = 120%

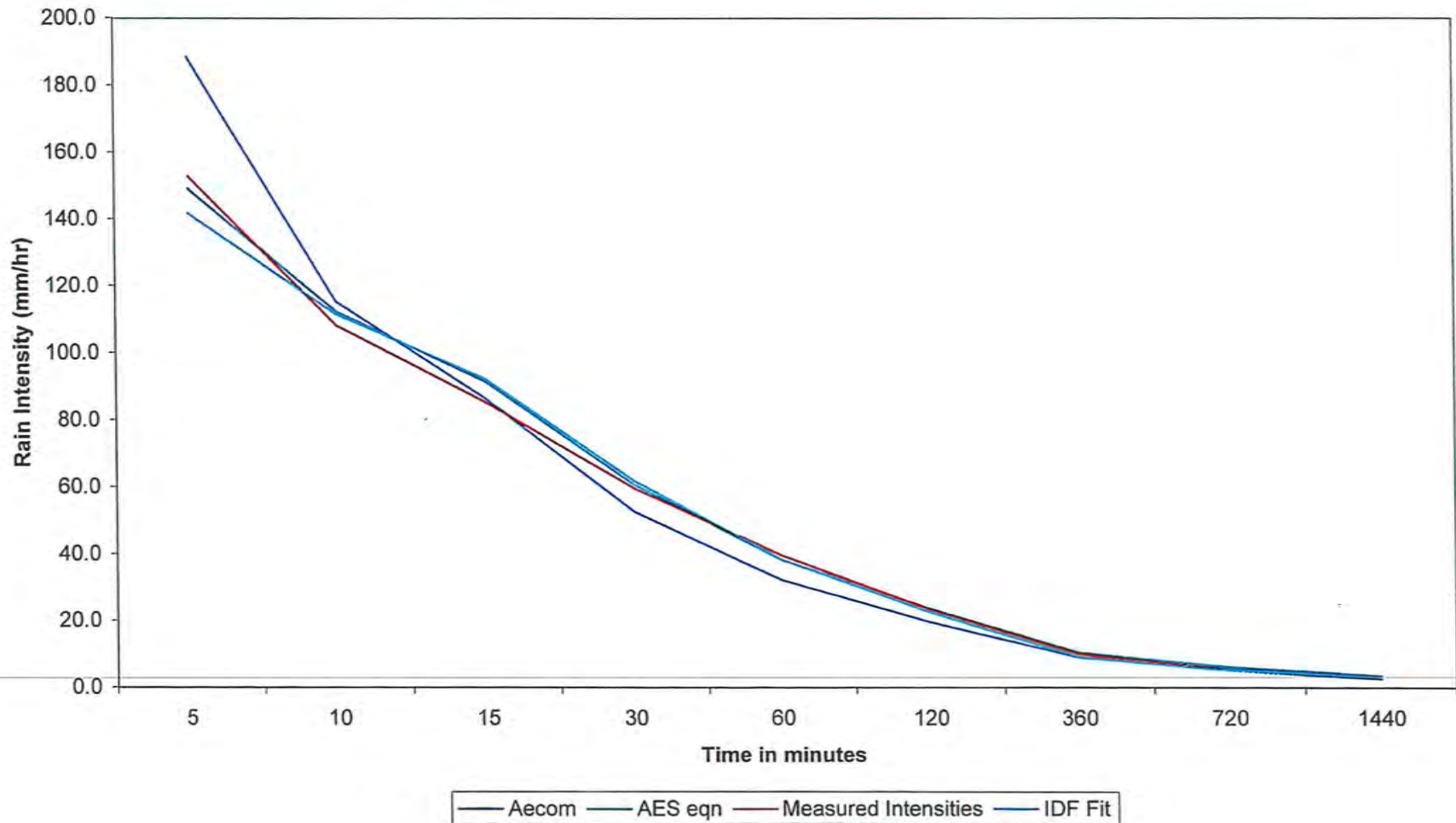
IDF Curve Comparison AES vs Aecom vs IDF-Fit
2-year Return Period
Lindsay Filtration Plant



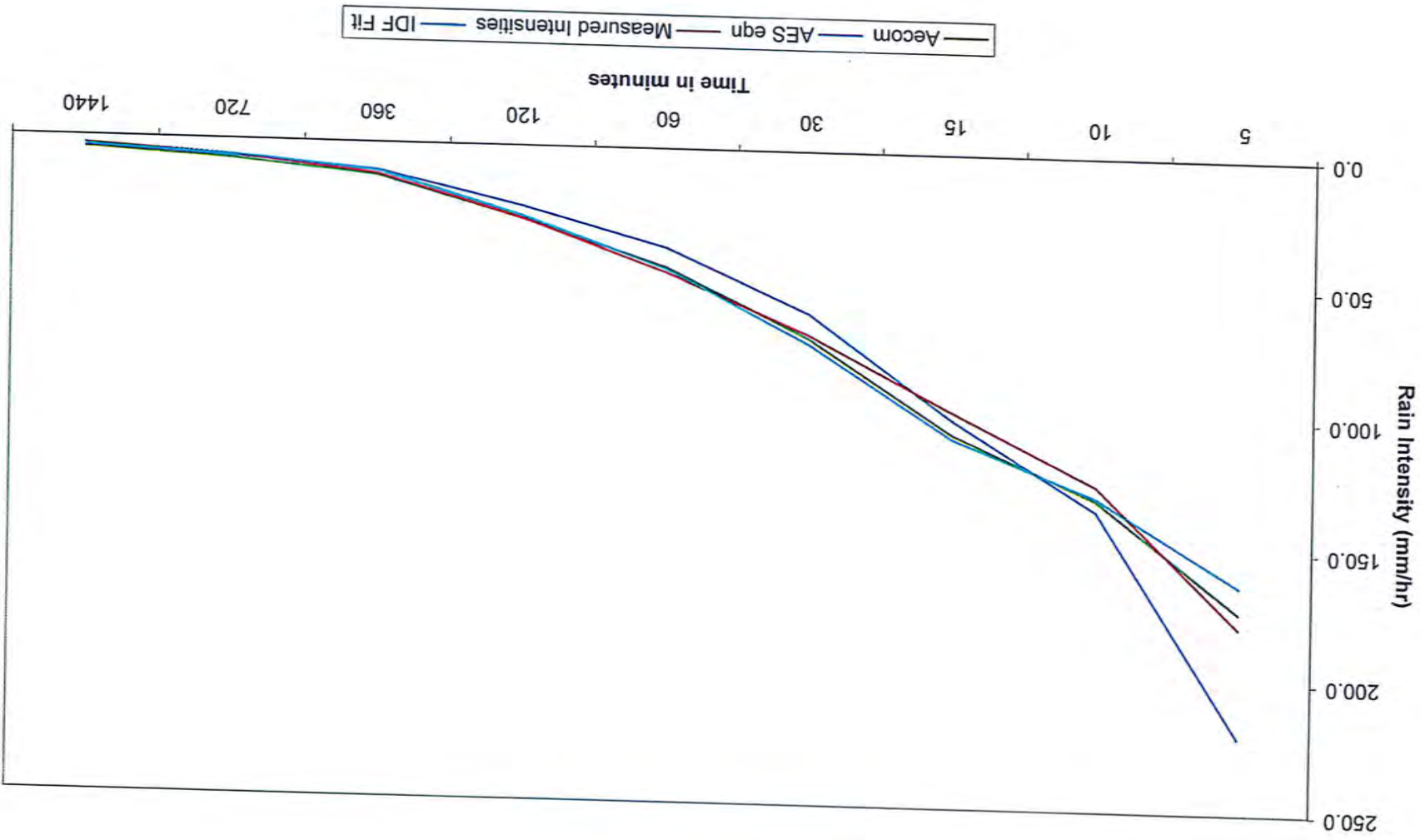
IDF Curve Comparison AES vs Aecom vs IDF-Fit
 5-year Return Period
 Lindsay Filtration Plant



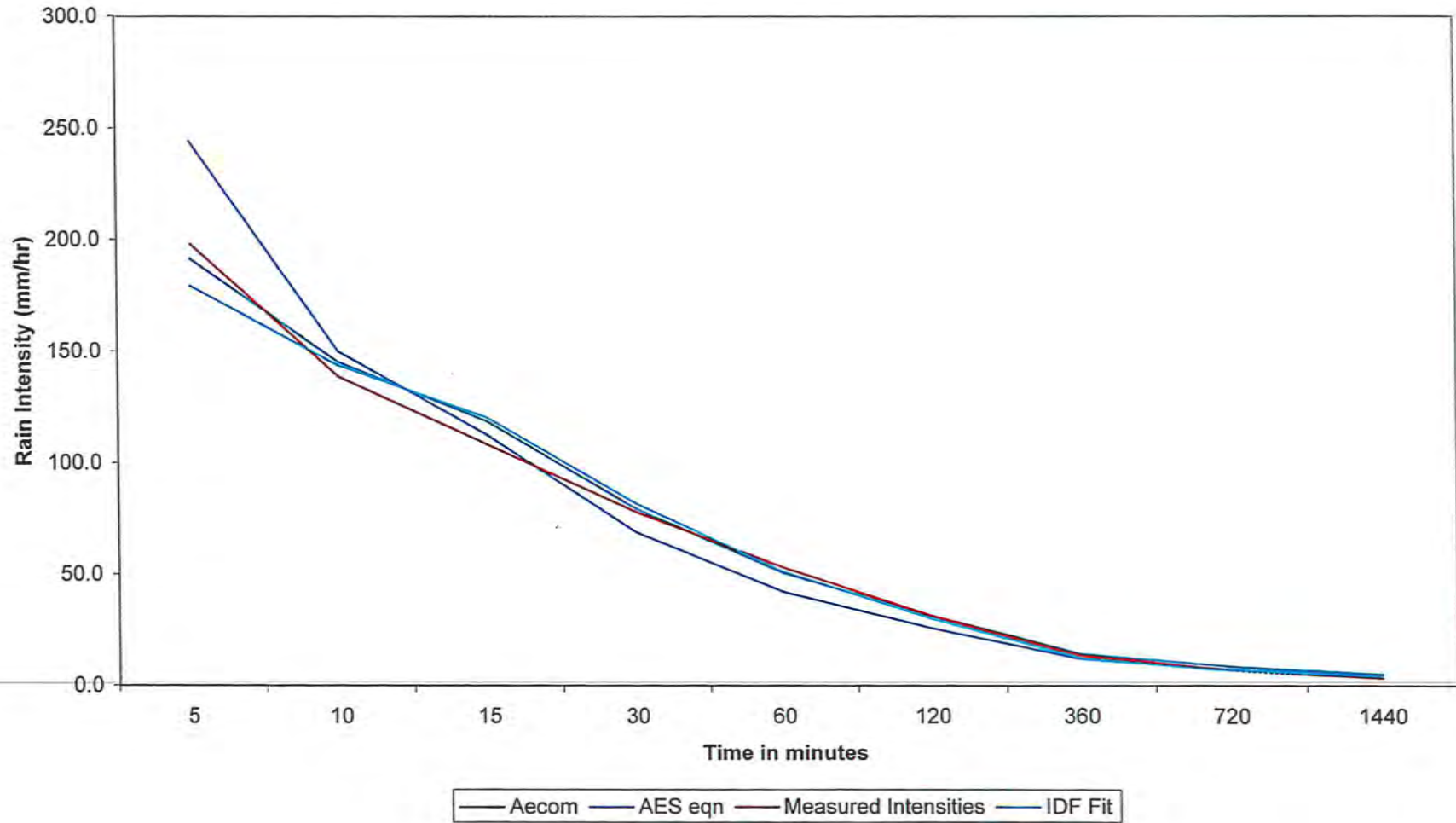
IDF Curve Comparison AES vs Aecom vs IDF-Fit
10-year Return Period
Lindsay Filtration Plant



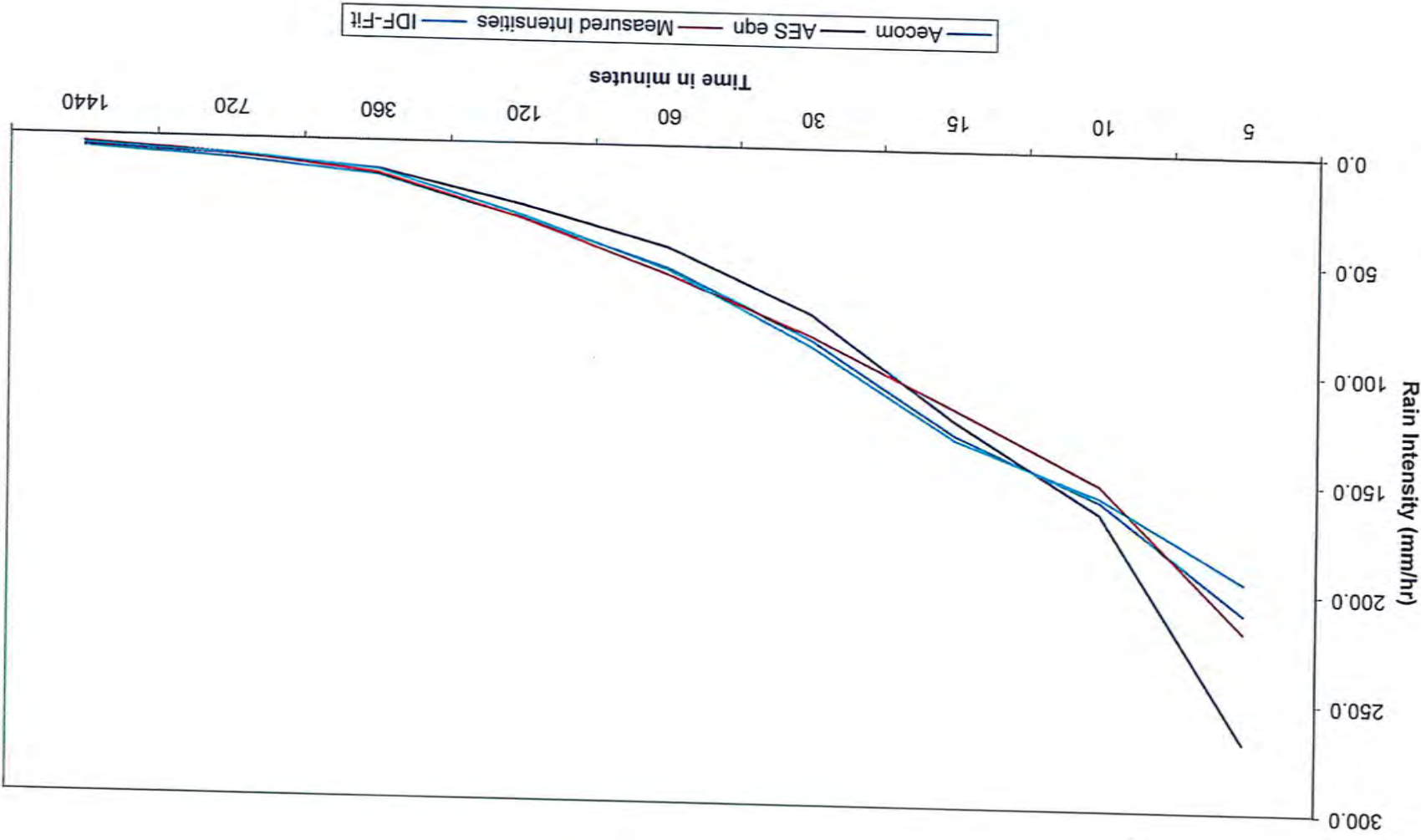
IDF Curve Comparison AES vs Aecom vs IDF-Fit
 25-year Return Period
 Lindsay Filtration Plant



IDF Curve Comparison AES vs Aecom vs IDF-Fit
50-year Return Period
Lindsay Filtration Plant



IDF Curve Comparison AES vs Aecom vs IDF-Fit
 100-year Return Period
 Lindsay Filtration Plant



Comparing Rainfall Volumes

6-hour Storm

Return Period Storm	Rainfall Volumes (mm)				
	Measured	Using CKL a, b, c	% Diff	Using new a, b, c	% Diff
2	36.6	37.8	103%	35.0	96%
5	50.8	52.9	104%	47.1	93%
10	60.2	63.0	105%	55.6	92%
25	72.1	75.6	105%	65.6	91%
50	80.9	85.2	105%	73.7	91%
100	89.7	94.7	106%	81.1	90%

12-hour Storm

Return Period Storm	Rainfall Volumes (mm)				
	Measured	Using CKL a, b, c	% Diff	Using new a, b, c	% Diff
2	39.8	44.3	111%	39.6	99%
5	53.2	62.5	117%	52.6	99%
10	62.2	75.0	121%	62.1	100%
25	73.4	90.6	123%	72.7	99%
50	81.8	102.4	125%	81.7	100%
100	90.1	114.3	127%	89.6	99%

24-hour Storm

Return Period Storm	Rainfall Volumes (mm)				
	Measured	Using CKL a, b, c	% Diff	Using new a, b, c	% Diff
2	43.6	51.7	119%	44.5	102%
5	56.4	73.6	131%	58.5	104%
10	64.8	89.1	137%	68.9	106%
25	75.4	108.2	143%	79.9	106%
50	83.3	122.7	147%	89.9	108%
100	91.2	137.5	151%	98.2	108%

Appendix C
Subcatchment Data

Route Channel	VO Node	To VO Node	GIS Node		Elevation		Base		RC+20	
			From	To	From	To	Length (m)	Slope m/m	Length (m)	Slope m/m
9	800	70	M'	OO	275.23	272.91	1419.19	0.163	1703.028	0.136
124	130	150	UU	QQ	248.59	248.05	409.38	0.132	491.256	0.110
10001	100	20	A*	NN	274.68	272.21	1070.89	0.231	1285.068	0.192
10003	200	20	B'	NN	273.92	272.21	2026.31	0.084	2431.572	0.070
10004	2300	10	MM	PP	274.38	272.68	2142.9	0.079	2571.48	0.066
10005	400	10	PP	FF*	272.68	272.48	230.96	0.087	277.152	0.072
10006	20	30	NN	GG	272.21	271.88	987.43	0.033	1184.916	0.028
10007	10	30	FF*	GG	272.48	271.88	455.747	0.132	546.8964	0.110
10008	30	125	GG	b	271.88	271.81	252.58	0.028	303.096	0.023
10009	125	40	b	y	271.81	271.71	477.76	0.021	573.312	0.017
10010	40	50	y	F	271.71	271.34	1841.33	0.020	2209.596	0.017
10011	70	60	OO	F	272.91	271.34	934.04	0.168	1120.848	0.140
10012	60	80	F	Z	271.34	271.01	825.863	0.040	991.0356	0.033
10013	80	90	Z	R	271.01	267.79	413.71	0.778	496.452	0.649
10014	90	101	R	JJ	267.79	256.91	1028.82	1.058	1234.584	0.881
10015	123	130	PP	UU	249.44	248.59	135.502	0.627	162.6024	0.523
10017	110	123	I'	PP	251.41	249.44	317.98	0.620	381.576	0.516
10130	101	121	JJ	T'	256.91	255.98	302.3	0.308	362.76	0.256
10140	1400	121	TT	T'	267.32	255.98	668.74	1.696	802.488	1.413
10160	121	110	T'	I'	255.98	251.41	260.9	1.752	313.08	1.460
10210	2000	160	HH	W	251.84	248.21	666.467	0.545	799.7604	0.454

RC-20	
Length (m)	Slope m/m
1135.352	0.204
327.504	0.165
856.712	0.288
1621.048	0.105
1714.32	0.099
184.768	0.108
789.944	0.042
364.5976	0.165
202.064	0.035
382.208	0.026
1473.064	0.025
747.232	0.210
660.6904	0.050
330.968	0.973
823.056	1.322
108.4016	0.784
254.384	0.774
241.84	0.385
534.992	2.120
208.72	2.190
533.1736	0.681

Catchment ID	Area (ha)	CN	Travel Length (m)	From	To	Elevation		Slope (%)	Runoff	ToC (min)	Tp (hr)
						Top	Bottom				
100	197.6	67	4031	A	A*	281.75	274.68	0.002	0.35	275.71	3.06
200	107.2	68	1447	Q	B*	290.52	273.93	0.011	0.33	91.28	1.01
300	315.5	54	4436	B	b	291.72	271.81	0.004	0.35	212.14	2.36
400	228.1	67	3401	B	PP	291.72	272.68	0.006	0.35	172.66	1.92
500	302.3	67	3018	D	FF*	300.87	272.66	0.009	0.35	137.34	1.53
600	299.6	63	3030	X	y	283.04	271.80	0.004	0.32	194.16	2.16
700	181.2	60	3720	EE	F*	286.56	271.34	0.004	0.36	197.61	2.20
800	183.2	68	3484	M	M'	302.92	275.23	0.008	0.33	159.82	1.78
900	236.7	64	4326	N	OO	294.93	272.91	0.005	0.33	206.31	2.29
1000	69.4	67	1532	W	F	280.70	271.34	0.006	0.36	111.12	1.23
1100	203.1	70	3108	J'	Z	282.85	271.01	0.004	0.37	182.43	2.03
1200	30.8	78	1343	G	R	278.93	267.79	0.008	0.4	88.94	0.99
1300	42.9	80	1600	H	JJ	277.21	256.91	0.013	0.42	59.70	0.66
1400	117.7	74	2232	O	TT	297.59	267.32	0.014	0.37	101.68	1.13
1500	37.3	74	1004	JJ*	T'	264.74	255.98	0.009	0.4	75.66	0.84
1600	8.9	74	436	AA	bb	253.68	252.70	0.002	0.37	81.26	0.90
1700	21.8	74	1544	I	P	271.44	249.44	0.014	0.35	85.50	0.95
1800	3.82	78	239	BB	UU	251.34	248.59	0.012	0.42	11.57	0.13
1900	10.25	80	745	L	QQ	252.45	248.05	0.006	0.53	37.40	0.42
2000	125	67	3272	DD*	HH	278.87	251.84	0.008	0.31	156.92	1.74
2100	34.3	80	906	RR	W	253.55	248.21	0.006	0.42	40.31	0.45
2200	9.7	78	563	CC	CC'	256.02	247.97	0.014	0.41	23.79	0.26
2300	308.8	64	3880	KK	MM	294.79	274.38	0.005	0.33	193.27	2.15

Catchment ID	Area (ha)	CN	Travel Length (m)	From	To	Elevation (m)		Slope (%)	Runoff Coeff	ToC (min)	Tp (hr)
						Top	Bottom				
100	197.6	67	2799	A	A*	281.75	274.68	0.003	0.35	203.71	2.26
200	107.2	68	1005	Q	B*	290.52	273.93	0.017	0.33	67.45	0.75
300	315.5	54	3081	B	b	291.72	271.81	0.006	0.35	156.74	1.74
400	228.1	67	2362	B	PP	291.72	272.68	0.008	0.35	127.57	1.42
500	302.3	67	2096	D	FF*	300.87	272.66	0.013	0.35	101.48	1.13
600	299.6	63	2104	X	y	283.04	271.80	0.005	0.32	143.46	1.59
700	181.2	60	2583	EE	F*	286.56	271.34	0.006	0.36	146.00	1.62
800	183.2	68	2419	M	M'	302.92	275.23	0.011	0.33	118.08	1.31
900	236.7	64	3004	N	OO	294.93	272.91	0.007	0.33	152.44	1.69
1000	69.4	67	1064	W	F	280.70	271.34	0.009	0.36	82.10	0.91
1100	203.1	70	2158	J'	Z	282.85	271.01	0.005	0.37	134.79	1.50
1200	30.8	78	933	G	R	278.93	267.79	0.012	0.4	65.71	0.73
1300	42.9	80	1111	H	JJ	277.21	256.91	0.018	0.42	38.54	0.43
1400	117.7	74	1550	O	TT	297.59	267.32	0.020	0.37	75.12	0.83
1500	37.3	74	698	JJ*	T'	264.74	255.98	0.013	0.4	55.90	0.62
1600	8.9	74	303	AA	bb	253.68	252.70	0.003	0.37	60.04	0.67
1700	21.8	74	1073	I	P	271.44	249.44	0.021	0.35	63.17	0.70
1800	3.82	78	166	BB	UU	251.34	248.59	0.017	0.42	7.47	0.08
1900	10.25	80	518	L	QQ	252.45	248.05	0.009	0.53	24.14	0.27
2000	125	67	2273	DD*	HH	278.87	251.84	0.012	0.31	115.94	1.29
2100	34.3	80	629	RR	W	253.55	248.21	0.008	0.42	26.02	0.29
2200	9.7	78	391	CC	CC'	256.02	247.97	0.021	0.41	15.36	0.17
2300	308.8	64	2694	KK	MM	294.79	274.38	0.008	0.33	142.79	1.59

Catchment ID	CN Base	CN +20%	CN -20%	IA Base	IA +50%	CN -20%
100	67	80.4	53.6	5	7.5	3.3
200	68	81.6	54.4	5	7.5	3.3
300	54	64.8	50	5	7.5	3.3
400	67	80.4	53.6	5	7.5	3.3
500	67	80.4	53.6	5	7.5	3.3
600	63	75.6	50.4	5	7.5	3.3
700	60	72	50	5	7.5	3.3
800	68	81.6	54.4	5	7.5	3.3
900	64	76.8	51.2	5	7.5	3.3
1000	67	80.4	53.6	5	7.5	3.3
1100	70	84	56	5	7.5	3.3
1200	78	93.6	62.4	5	7.5	3.3
1300	80	96	64	5	7.5	3.3
1400	74	88.8	59.2	5	7.5	3.3
1500	74	88.8	59.2	5	7.5	3.3
1600	74	88.8	59.2	5	7.5	3.3
1700	74	88.8	59.2	5	7.5	3.3
1800	78	93.6	62.4	5	7.5	3.3
1900	80	96	64	5	7.5	3.3
2000	67	80.4	53.6	5	7.5	3.3
2100	80	96	64	5	7.5	3.3
2200	78	93.6	62.4	5	7.5	3.3
2300	64	76.8	51.2	5	7.5	3.3
Route Channel	To VO Node	GIS Node		Elevation		Length (m)
		From	To	From	To	
10004	10	MM	PP	274.38	272.68	2142.9
10005	10	PP	FF*	272.68	272.48	230.96
10007	30	FF*	GG	272.48	271.88	455.747
10001	20	A*	NN	274.68	272.21	1070.89
10003	20	B'	NN	273.92	272.21	2026.31
10006	30	NN	GG	272.21	271.88	987.43
10008	125	GG	b	271.88	271.81	252.58
10009	40	b	y	271.81	271.71	477.76
10010	50	y	F	271.71	271.34	1841.33
9	70	M'	OO	275.23	272.91	1419.19
10011	60	OO	F	272.91	271.34	934.04
10012	80	F	Z	271.34	271.01	825.863
10013	90	Z	R	271.01	267.79	413.71
10014	101	R	JJ	267.79	256.91	1028.82
10130	121	JJ	T'	256.91	255.98	302.3
10160	110	T'	I'	255.98	251.41	260.9
10017	123	I'	PP	251.41	249.44	317.98
10015	130	PP	UU	249.44	248.59	135.502
124	150	UU	QQ	248.59	248.05	409.38

10210	160	HH	W	251.84	248.21	666.467
	121	TT	T'	267.32	255.98	668.74

HEC RAS ID	Location	Catchment	VO Flow Node	Regional	100 Year	50 Year	25 Year	10 Year	5 Year	2 year
3532	Top of System, US of Sturgeon	1100	90	64.73	19.01	15.64	12.19	7.92	5.30	2.32
2886	DS of Community Centre	1300	101	65.55	19.07	15.67	12.21	7.94	5.31	2.35
1815	DS of HWY 36 (W)	1500	121	69.77	20.51	16.88	13.22	8.73	5.96	2.95
1498	DS of Cedar Glen Road	1600	110	70.01	20.59	16.93	13.27	8.78	6.00	2.98
1186	DS of HWY 36 (E)	1700	123	70.55	20.78	17.10	13.42	8.92	6.12	3.05
883	DS of Herons Landing	1800	130	70.61	20.78	17.11	13.42	8.92	6.12	3.06
755	DS of Herons Landing 2	1900	150	70.76	20.71	16.67	13.31	8.89	6.10	3.07

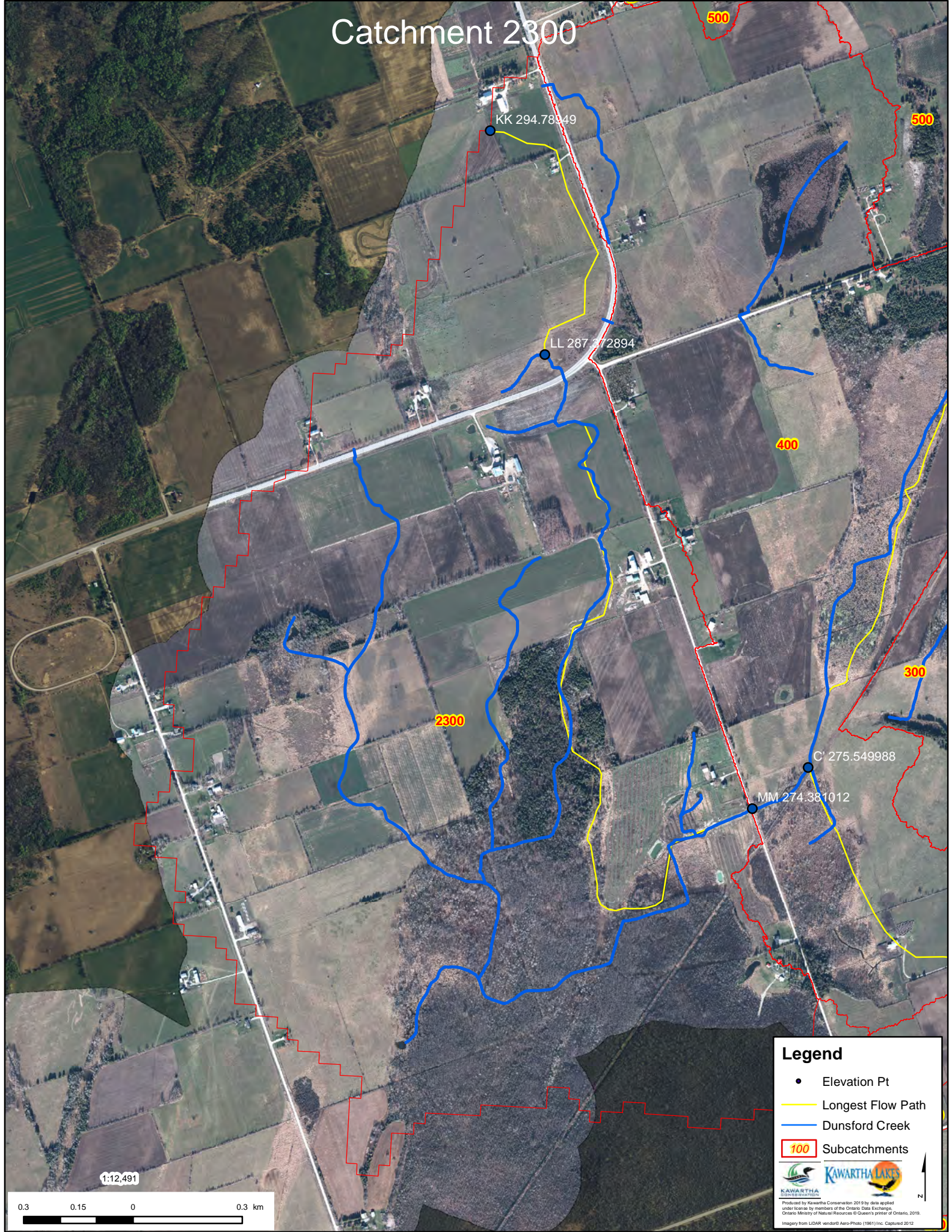
Comment
Included flows from Catchment 1200 for simplification (63.99 m ³ /s vs 64.73 m ² /s for regional event)

Location	Hydrologic Flow Node	Base	Curve Number		Initial Abstraction		Subcatchment Travel Length		Channel Routing			Time Step	
			CN+20%	CN-20%	IA+50%	IA-50%	TL+20%	TL-20%	No RC	RC+20%	RC-20%	DT+50%	DT-50%
Top of System, US of Sturgeon	90	65.6	83.7	50.1	64.5	66.3	63.7	67.0	114.0	57.3	74.8	65.6	65.6
DS of Community Centre	101	66.5	84.7	50.1	65.3	67.2	64.4	67.9	116.2	58.0	75.9	66.5	66.5
DS of HWY 36 (W)	121	71.0	90.0	54.1	69.5	71.6	68.6	72.4	124.2	62.0	80.5	70.9	70.9
DS of Cedar Glen Road	110	71.2	90.3	54.2	69.7	71.9	68.8	72.7	124.6	62.2	80.8	71.1	71.1
DS of HWY 36 (E)	123	71.8	91.0	54.7	70.3	71.4	69.3	73.3	125.7	62.8	81.4	71.7	71.7
DS of Herons Landing	130	71.8	91.0	54.7	70.3	72.5	69.3	73.4	125.8	62.8	81.5	71.8	71.8
DS of Herons Landing 2	150	71.8	91.1	54.8	70.5	72.6	69.5	73.5	126.3	62.7	81.3	71.9	71.9

Location	Hydrologic Flow Node	Curve Number		Initial Abstraction		Subcatchment Travel Length		Channel Routing			Time Step	
		CN+20%	CN-20%	IA+50%	IA-50%	TL+20%	TL-20%	No RC	RC+20	RC-20	DT+50%	DT-50%
Top of System, US of Sturgeon	90	27.6%	-23.6%	-1.6%	1.2%	-2.9%	2.1%	74%	-13%	14%	0%	0%
DS of Community Centre	101	27.3%	-24.7%	-1.8%	1.1%	-3.2%	2.1%	75%	-13%	14%	0%	0%
DS of HWY 36 (W)	121	26.8%	-23.8%	-2.1%	0.9%	-3.4%	2.1%	75%	-13%	14%	0%	0%
DS of Cedar Glen Road	110	26.8%	-23.8%	-2.1%	1.0%	-3.3%	2.1%	75%	-13%	14%	0%	0%
DS of HWY 36 (E)	123	26.8%	-23.8%	-2.0%	-0.4%	-3.4%	2.2%	75%	-13%	14%	0%	0%
DS of Herons Landing	130	26.8%	-23.8%	-2.0%	1.0%	-3.5%	2.2%	75%	-13%	13%	0%	0%
DS of Herons Landing 2	150	26.8%	-23.7%	-1.8%	1.0%	-3.3%	2.4%	76%	-13%	13%	0%	0%
	<i>Minimum =</i>	<i>26.8%</i>	<i>-24.7%</i>	<i>-2.1%</i>	<i>-0.4%</i>	<i>-3.5%</i>	<i>2.1%</i>	<i>73.8%</i>	<i>-12.7%</i>	<i>13.2%</i>	<i>-0.1%</i>	<i>-0.1%</i>
	<i>Average =</i>	<i>27.0%</i>	<i>-23.9%</i>	<i>-1.9%</i>	<i>0.8%</i>	<i>-3.3%</i>	<i>2.2%</i>	<i>75.0%</i>	<i>-12.6%</i>	<i>13.6%</i>	<i>0.0%</i>	<i>0.0%</i>
	<i>Maximum =</i>	<i>27.6%</i>	<i>-23.6%</i>	<i>-1.6%</i>	<i>1.2%</i>	<i>-2.9%</i>	<i>2.4%</i>	<i>75.8%</i>	<i>-12.5%</i>	<i>14.1%</i>	<i>0.0%</i>	<i>0.0%</i>

Appendix D
Subcatchment Maps

Catchment 2300



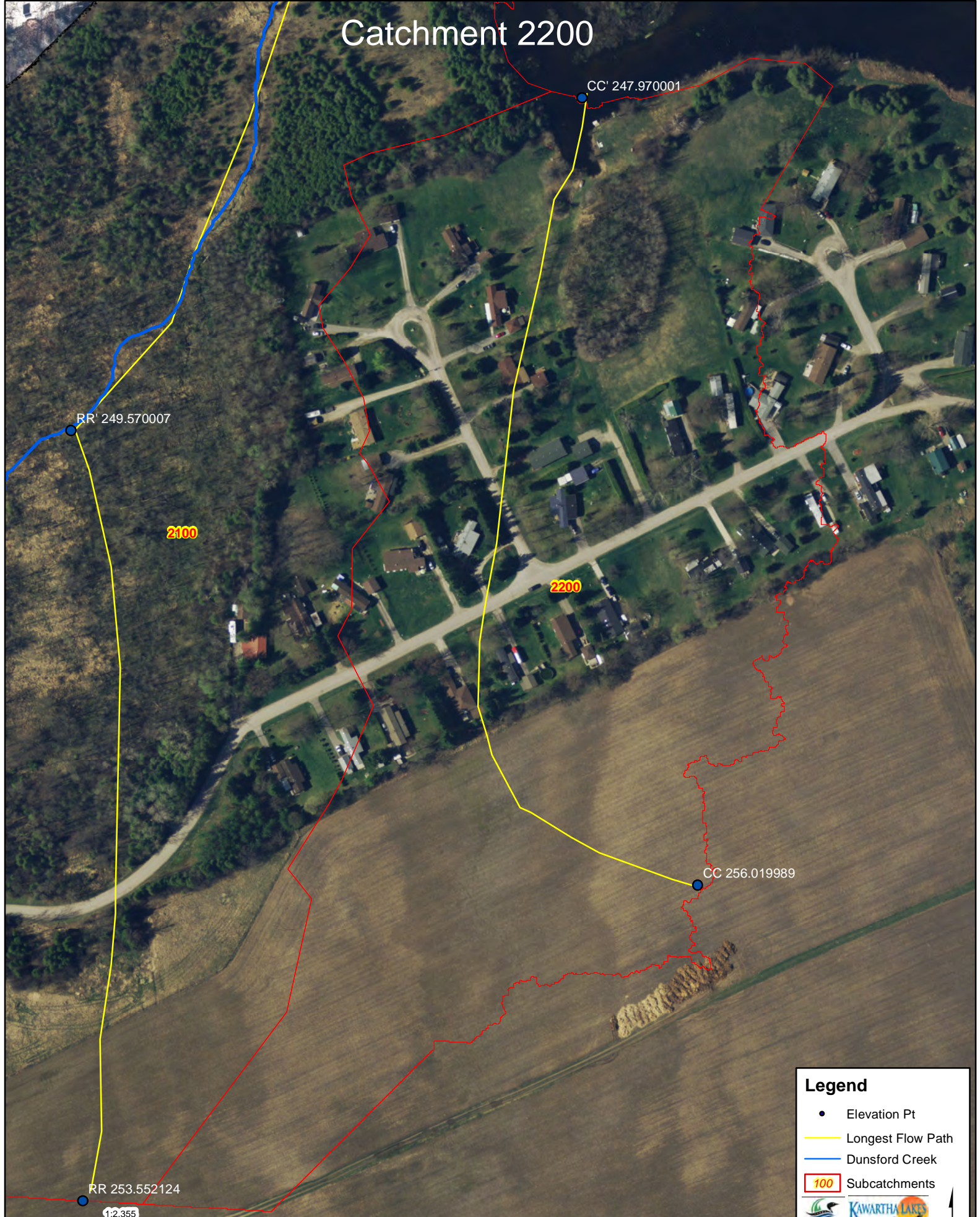
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 2200



Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments



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0.055 0.0275 0 0.055 km



Catchment 2100



1:3,832

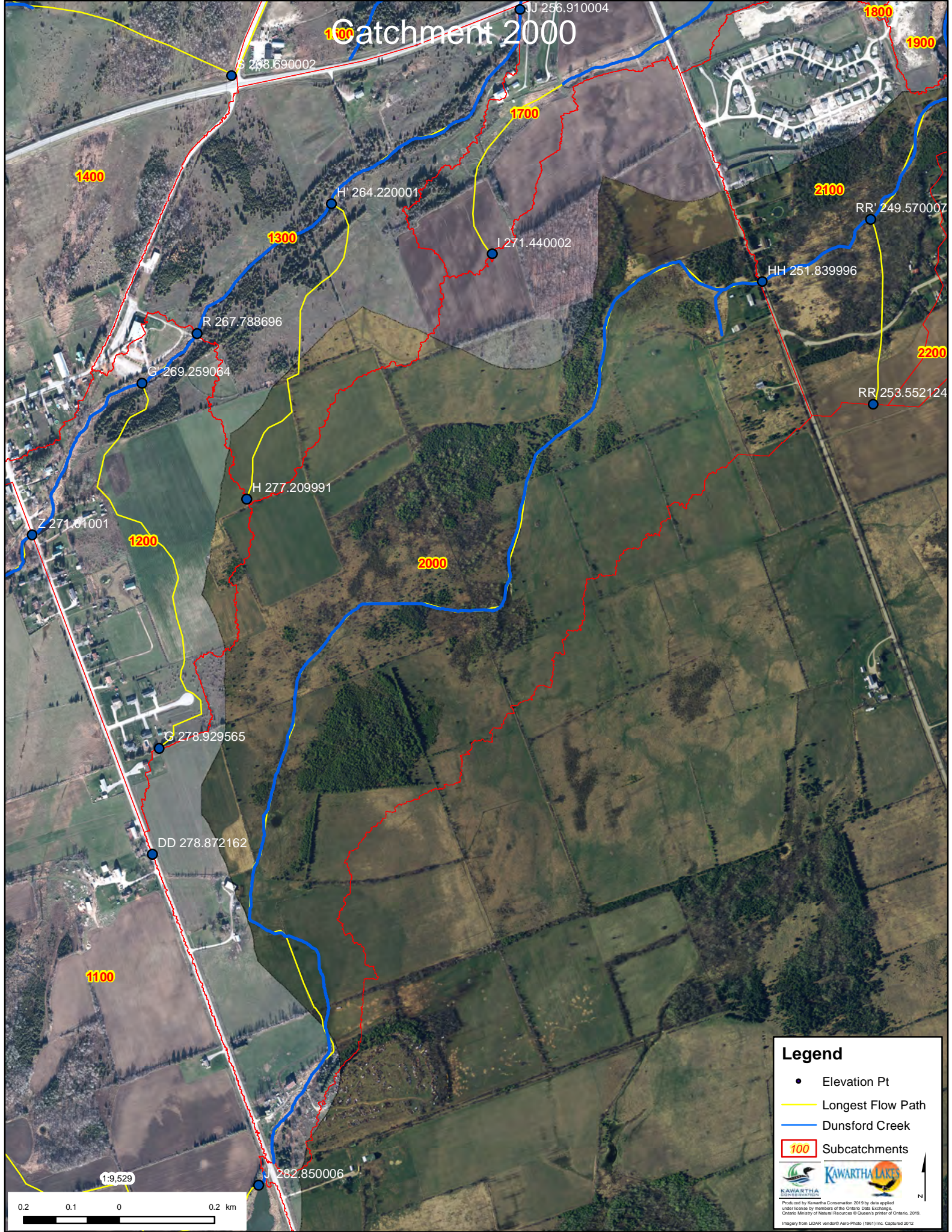


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments



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Catchment 2000



Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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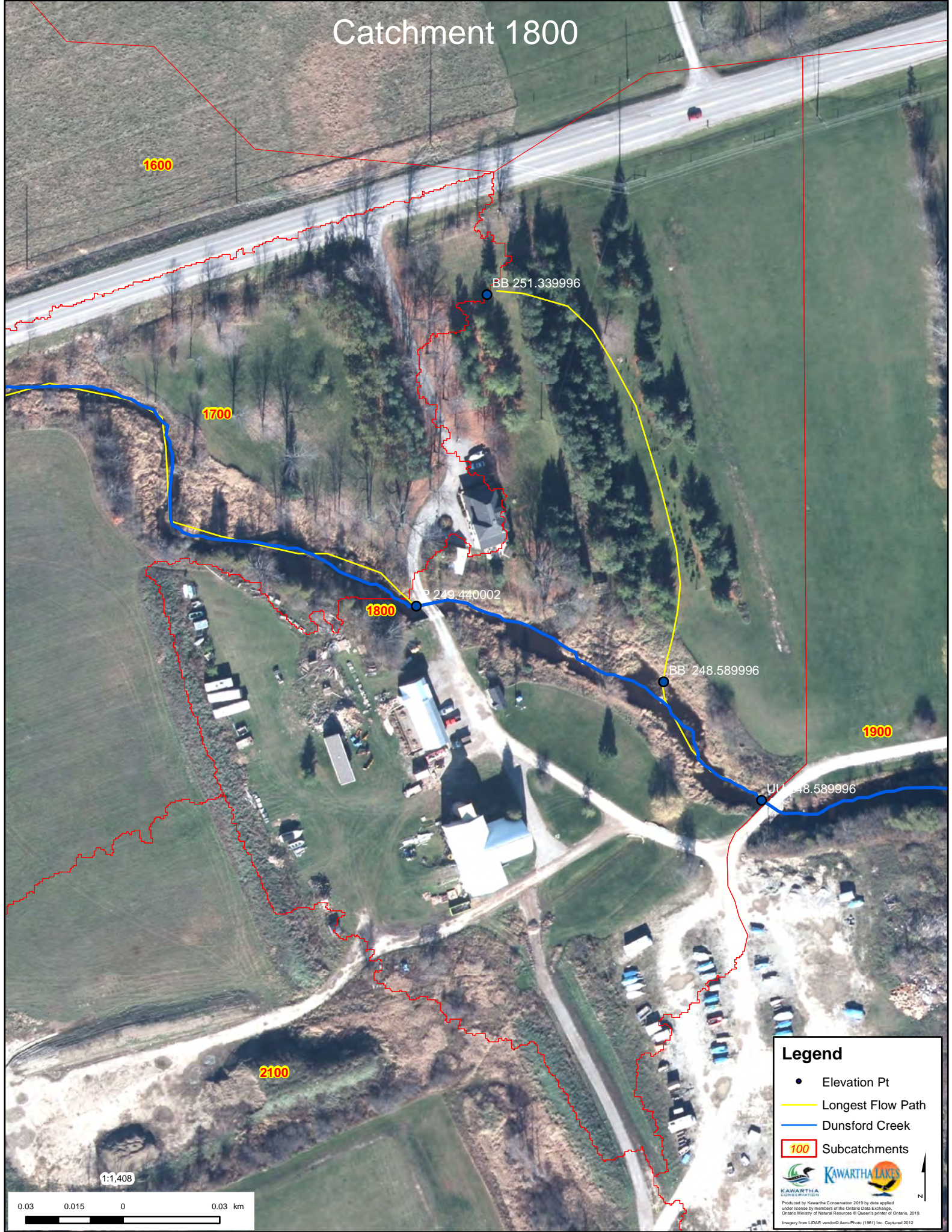
Catchment 1900



Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

Catchment 1800



1600

1700

1800

1900

2100

BB 251.339996

P 249.440002

BB' 248.589996

UU 248.589996

1:1,408

0.03 0.015 0 0.03 km

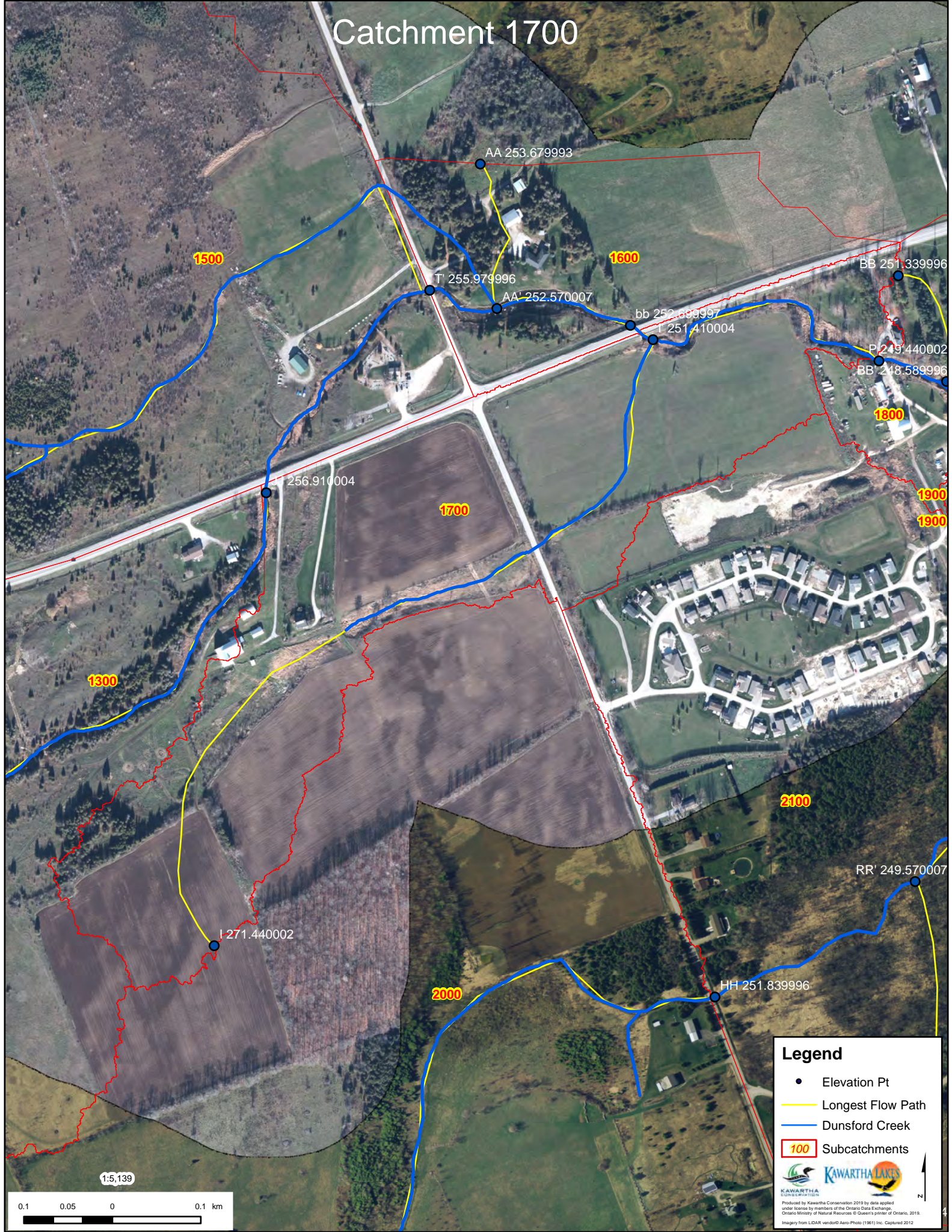
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 1700



1:5,139

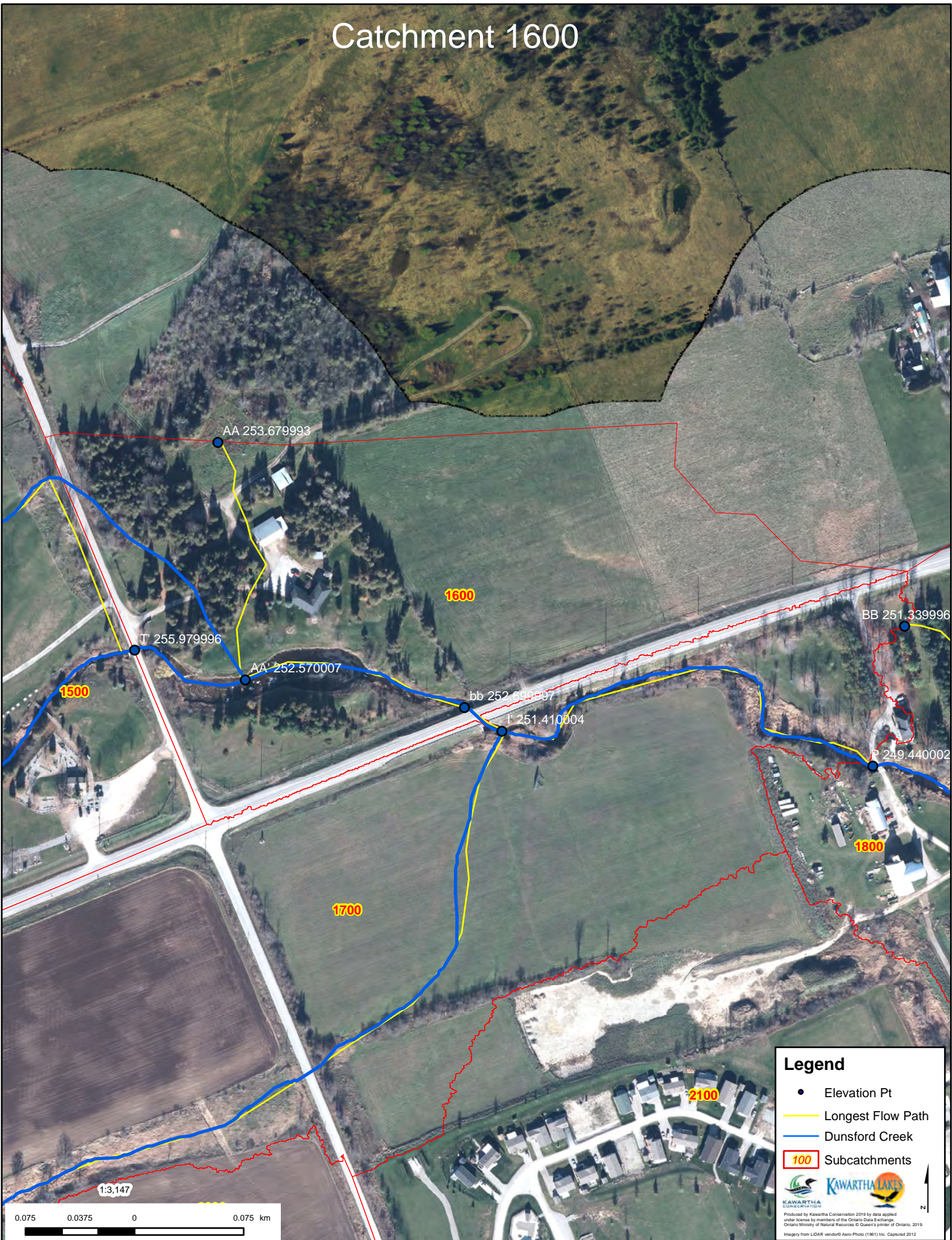


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 1600

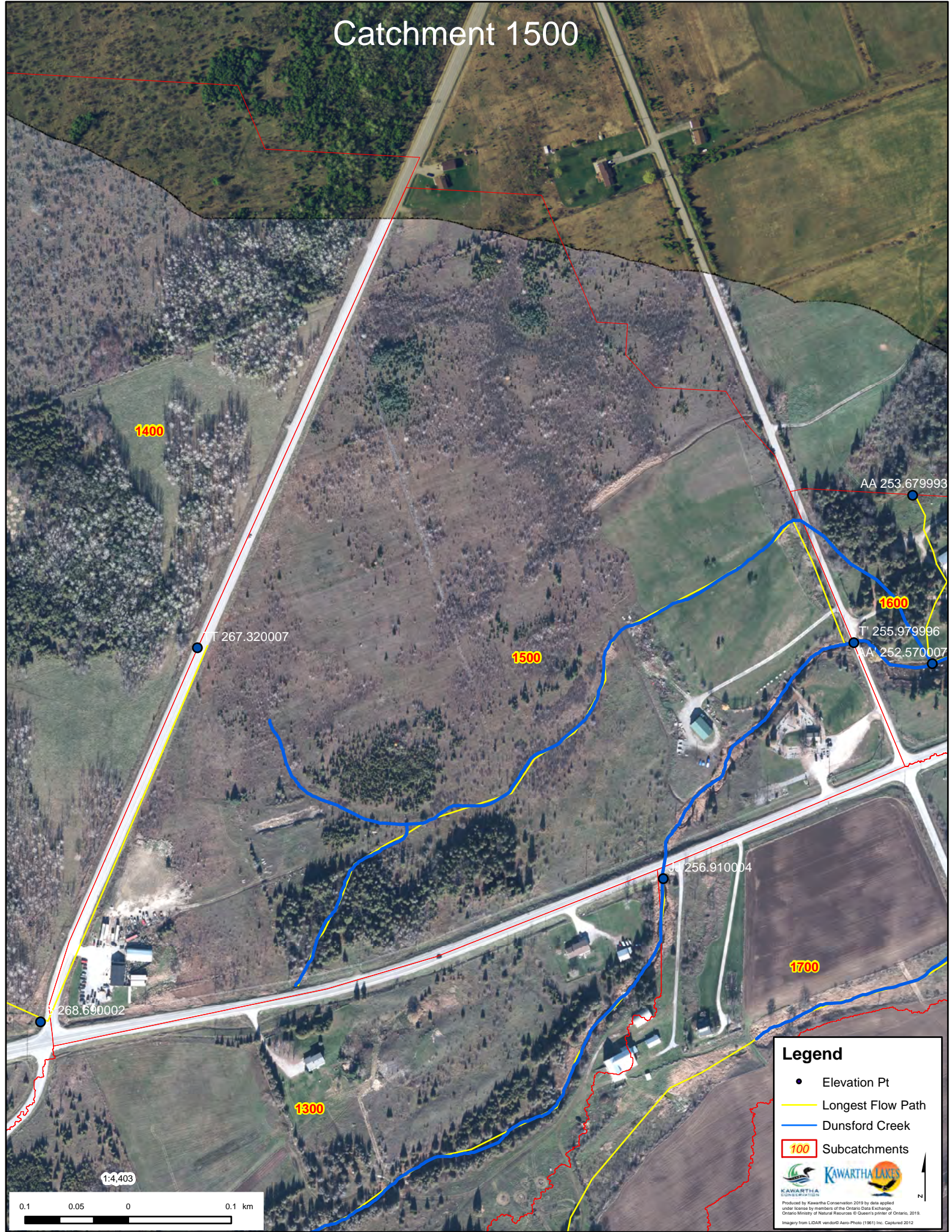


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments


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Imagery from LIDAR vendor: Aero-Photo (1961) Inc. Captured 2012.

Catchment 1500

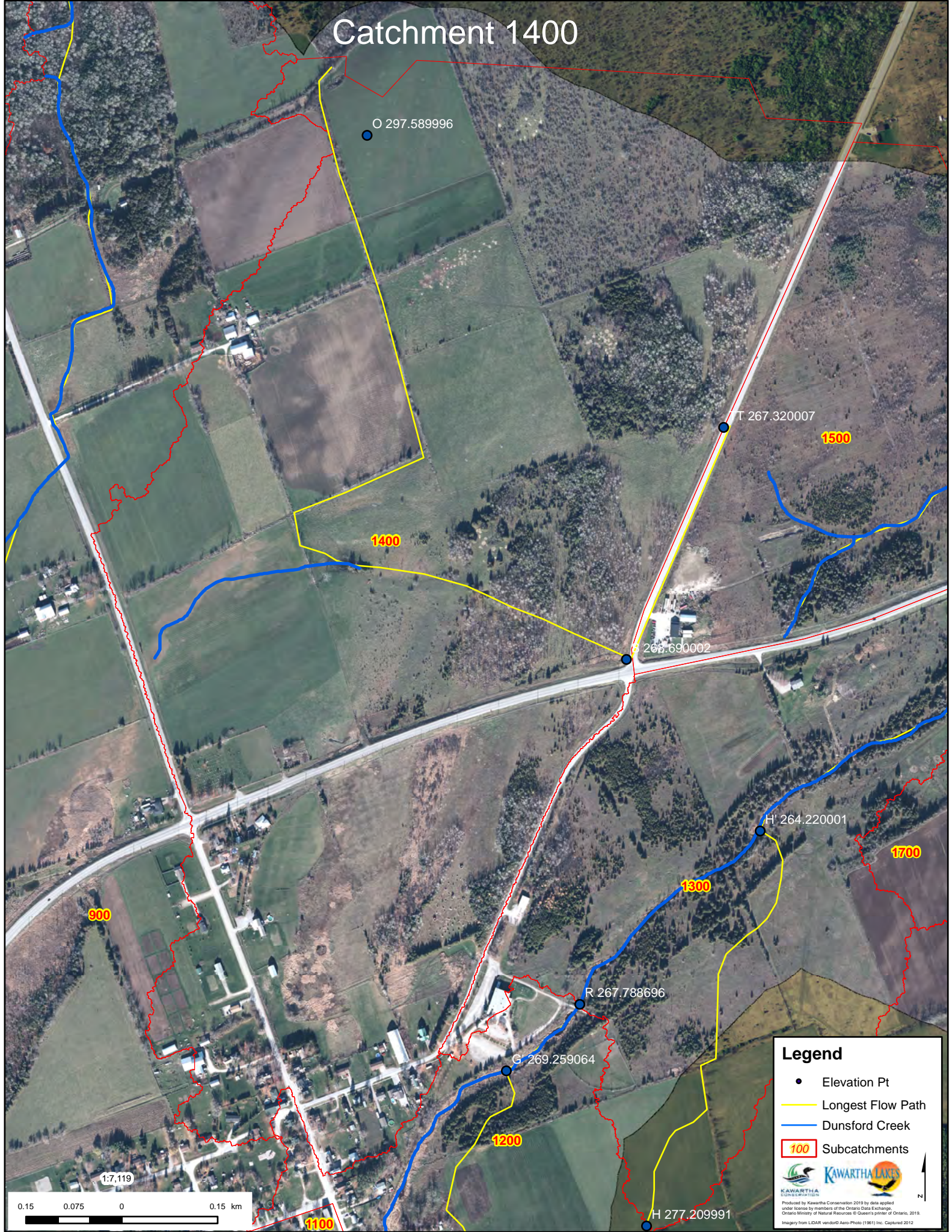


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

 
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Imagery from LIDAR vendor: Aero-Photo (1961) Inc. Captured 2012.

Catchment 1400



1:7,119

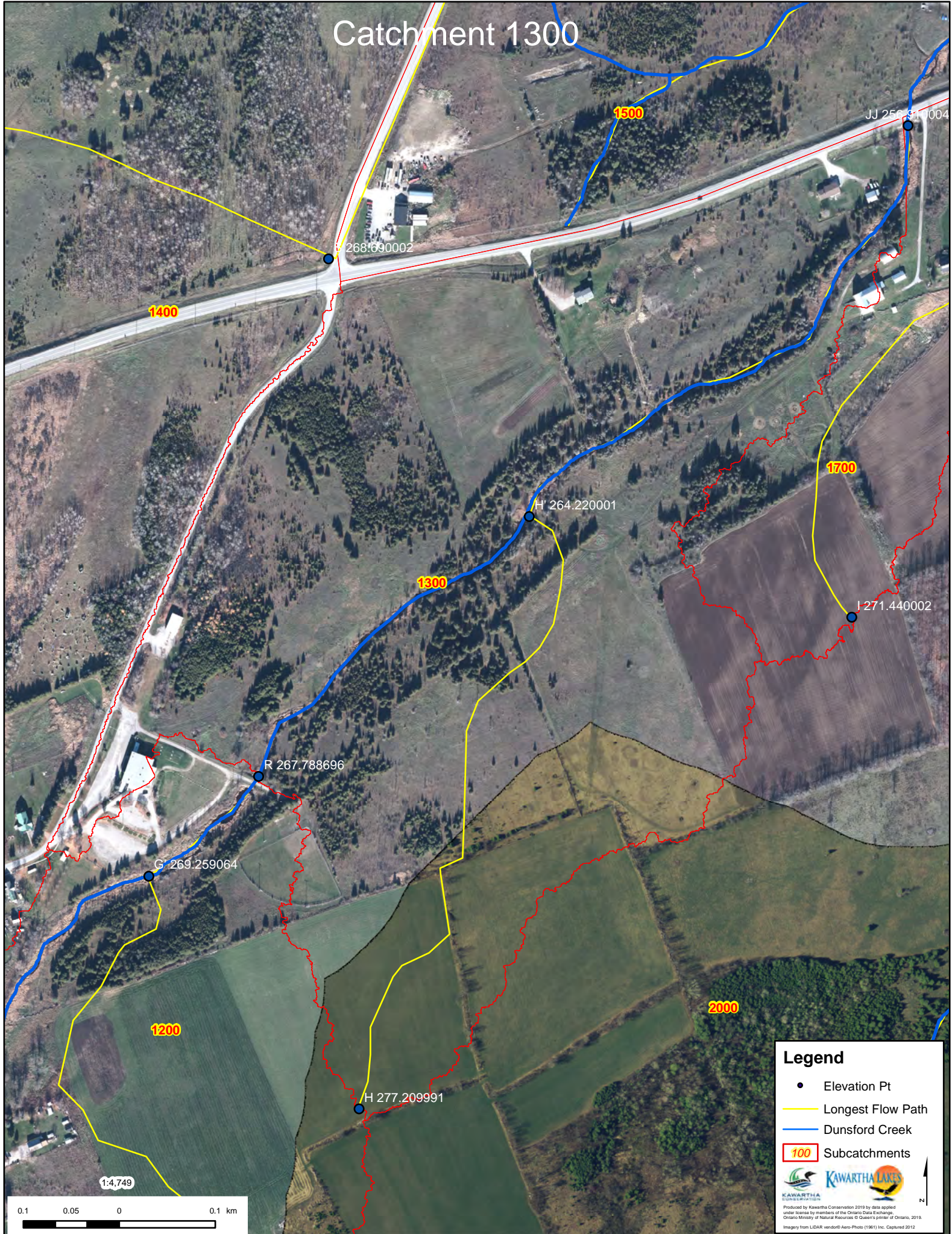
0.15 0.075 0 0.15 km

Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 1300

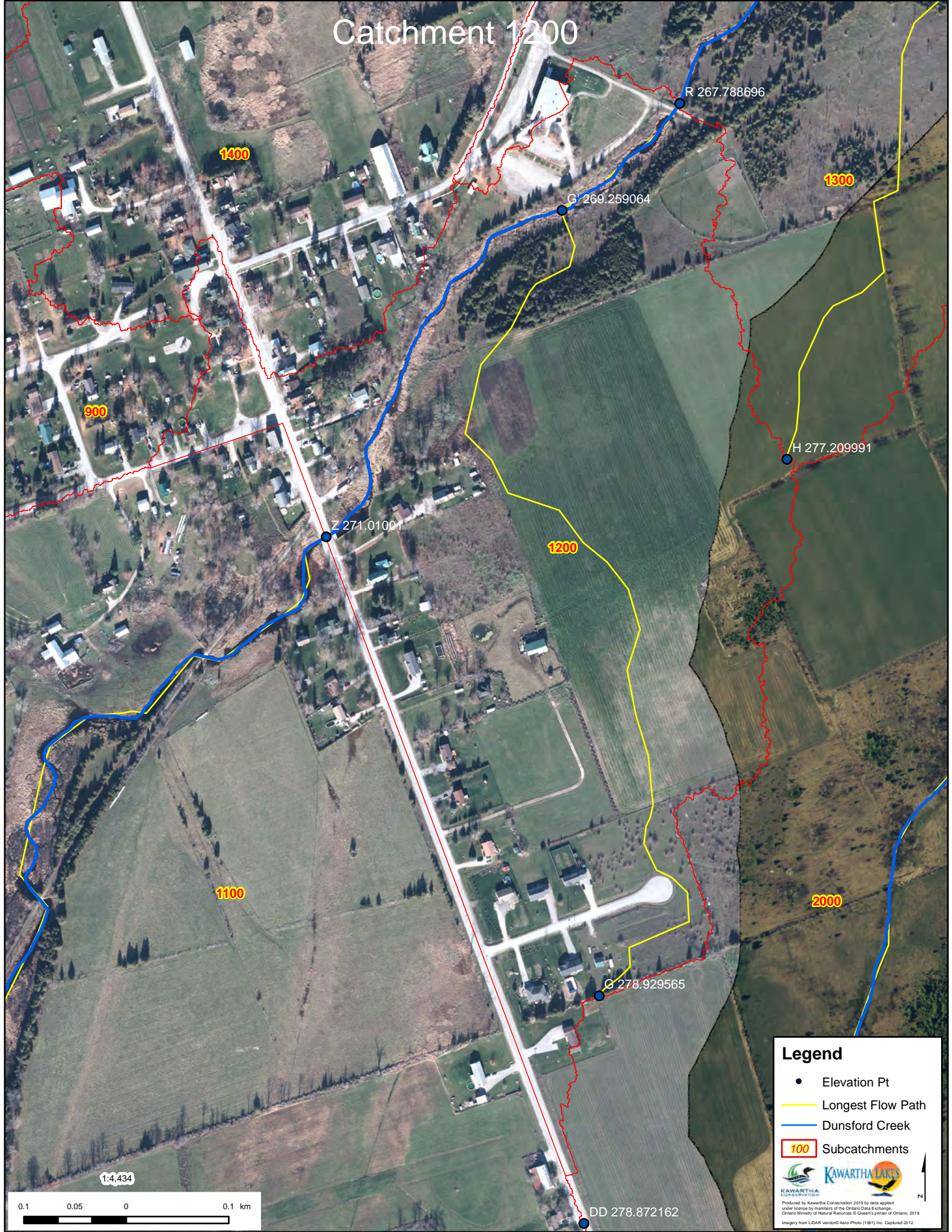


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments


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Imagery from LIDAR vendor: Aero-Photo (1961) Inc. Captured 2012.

Catchment 1200



1:4,434

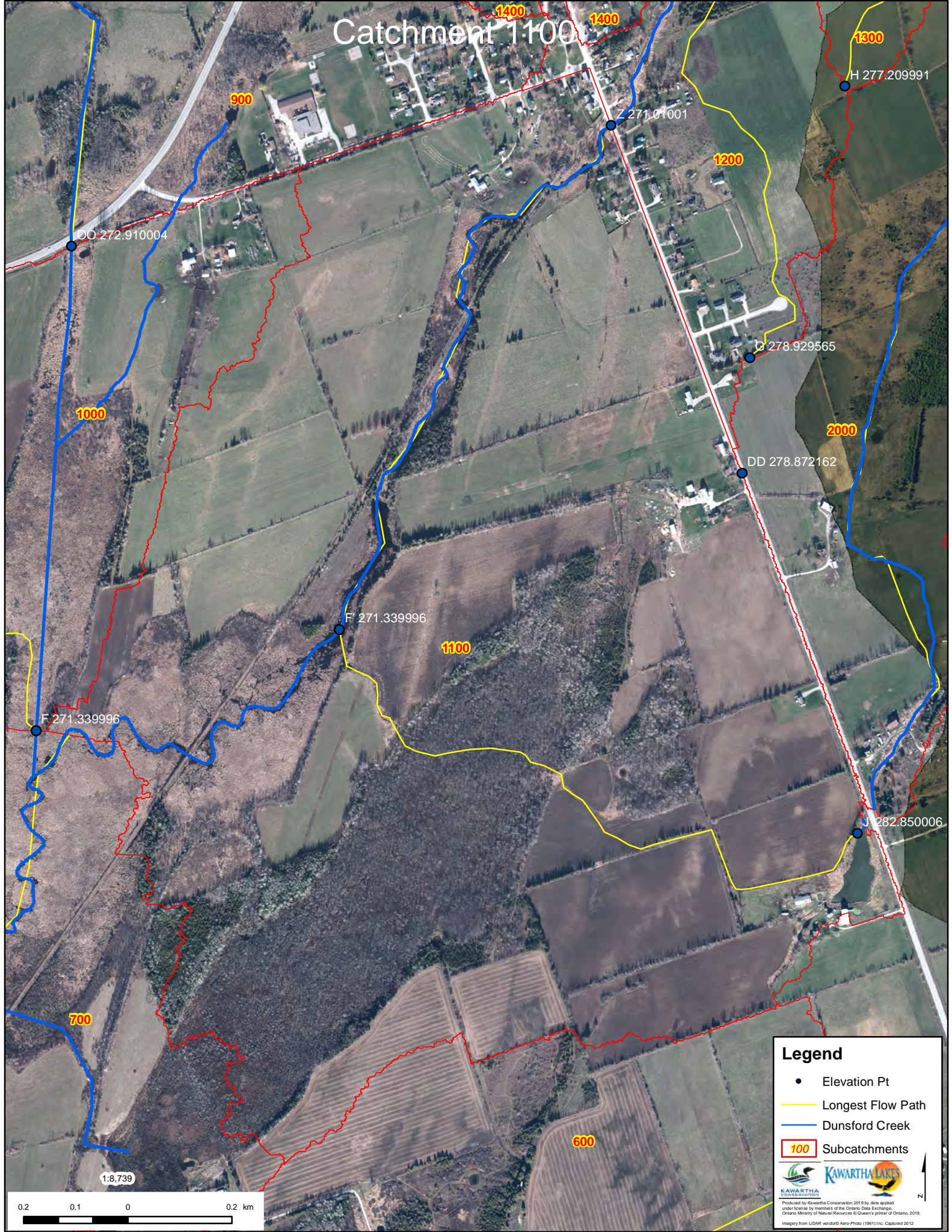


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments



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Catchment 1100



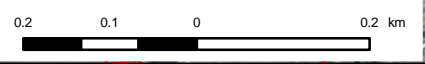
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

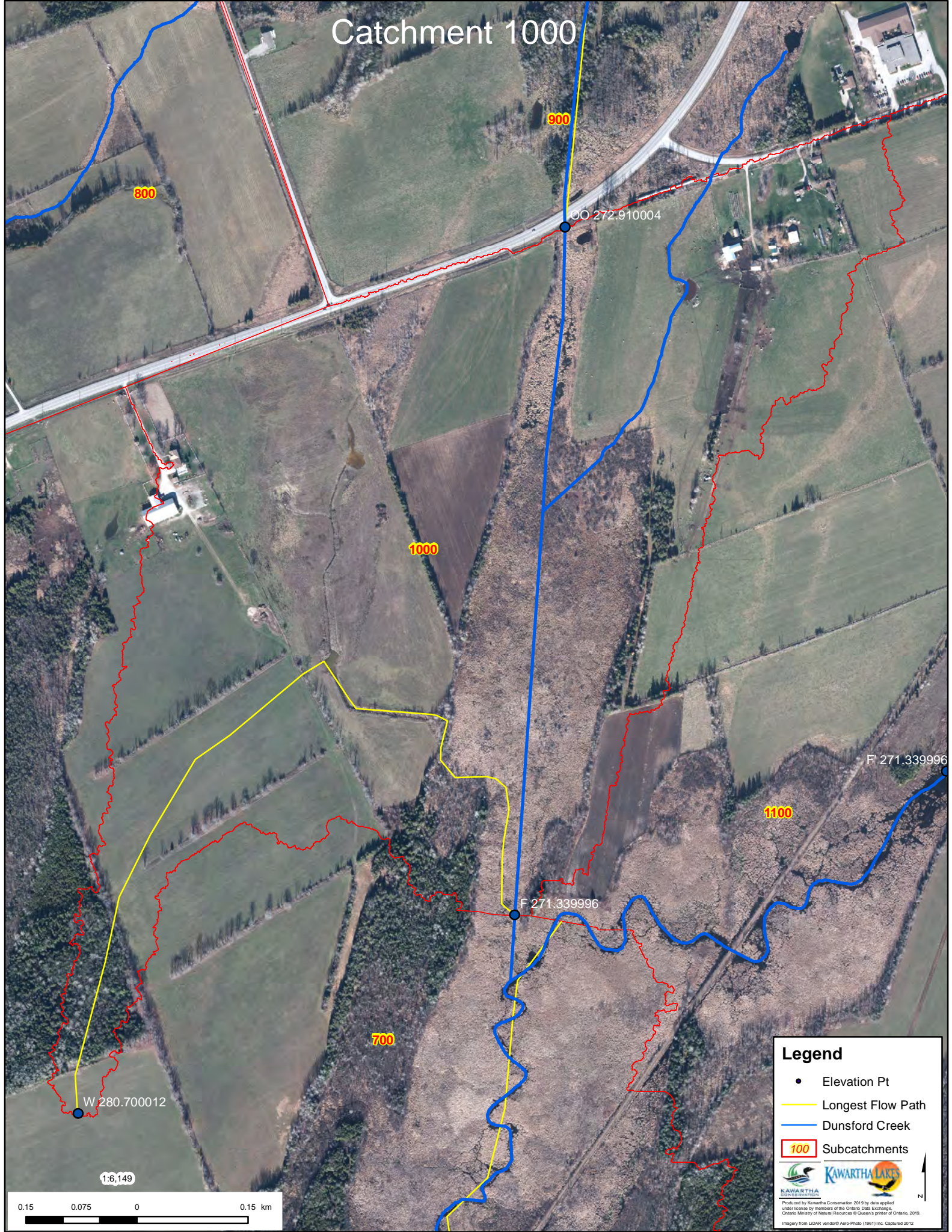
 

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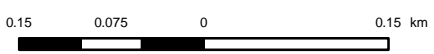
1:8,739



Catchment 1000





1:6,149



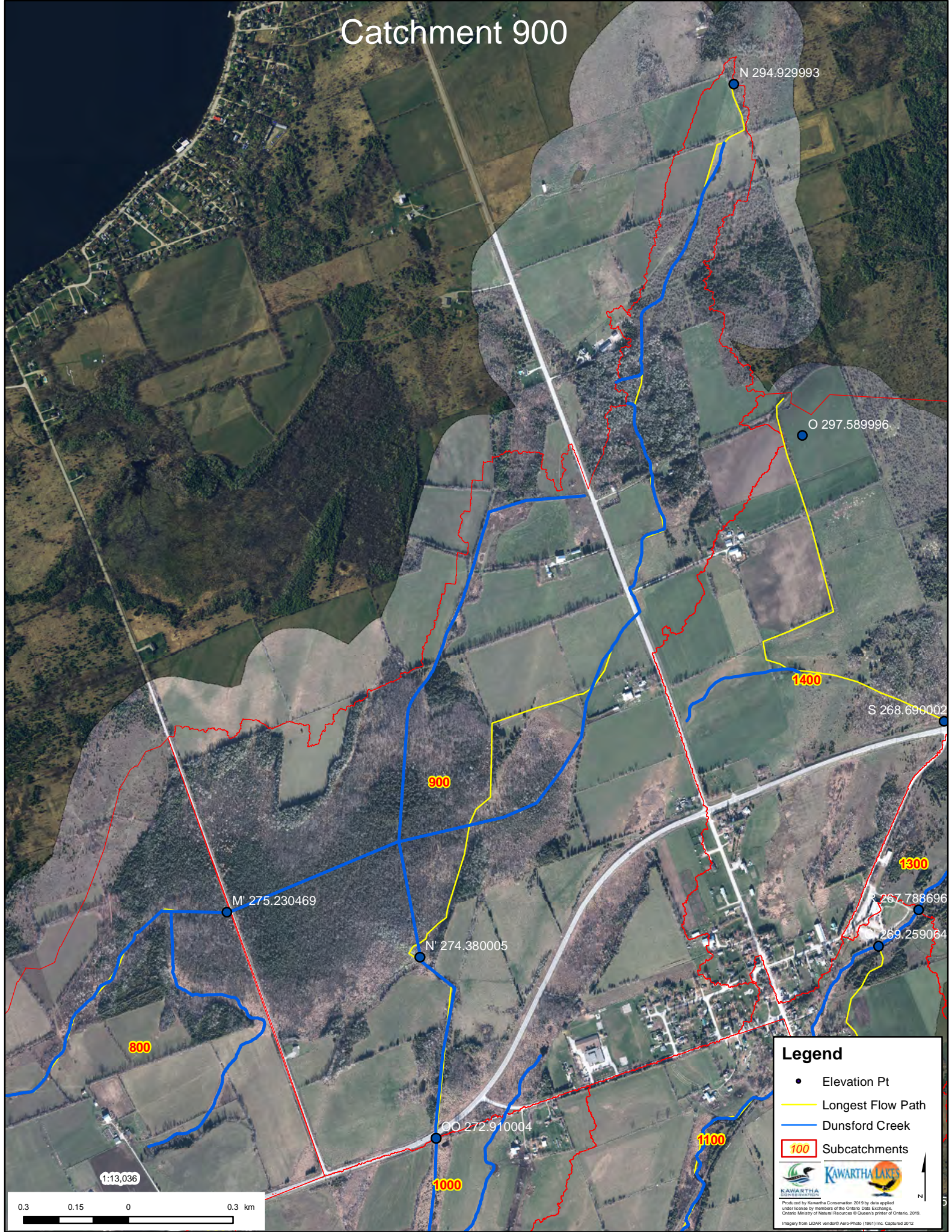
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments


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Catchment 900



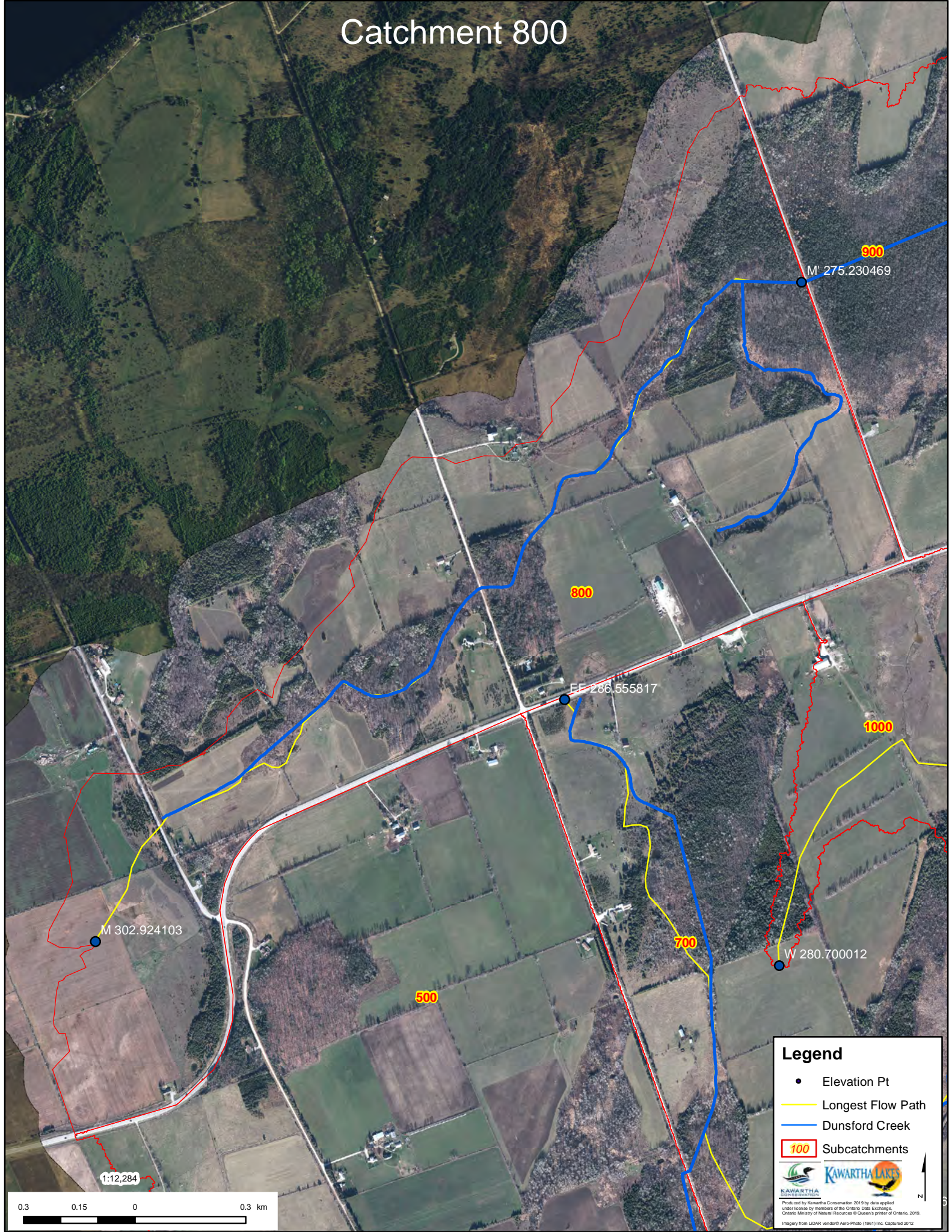
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments


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Imagery from LGAR veldor© Aero-Photo (1981) Inc. Captured 2012



Catchment 800



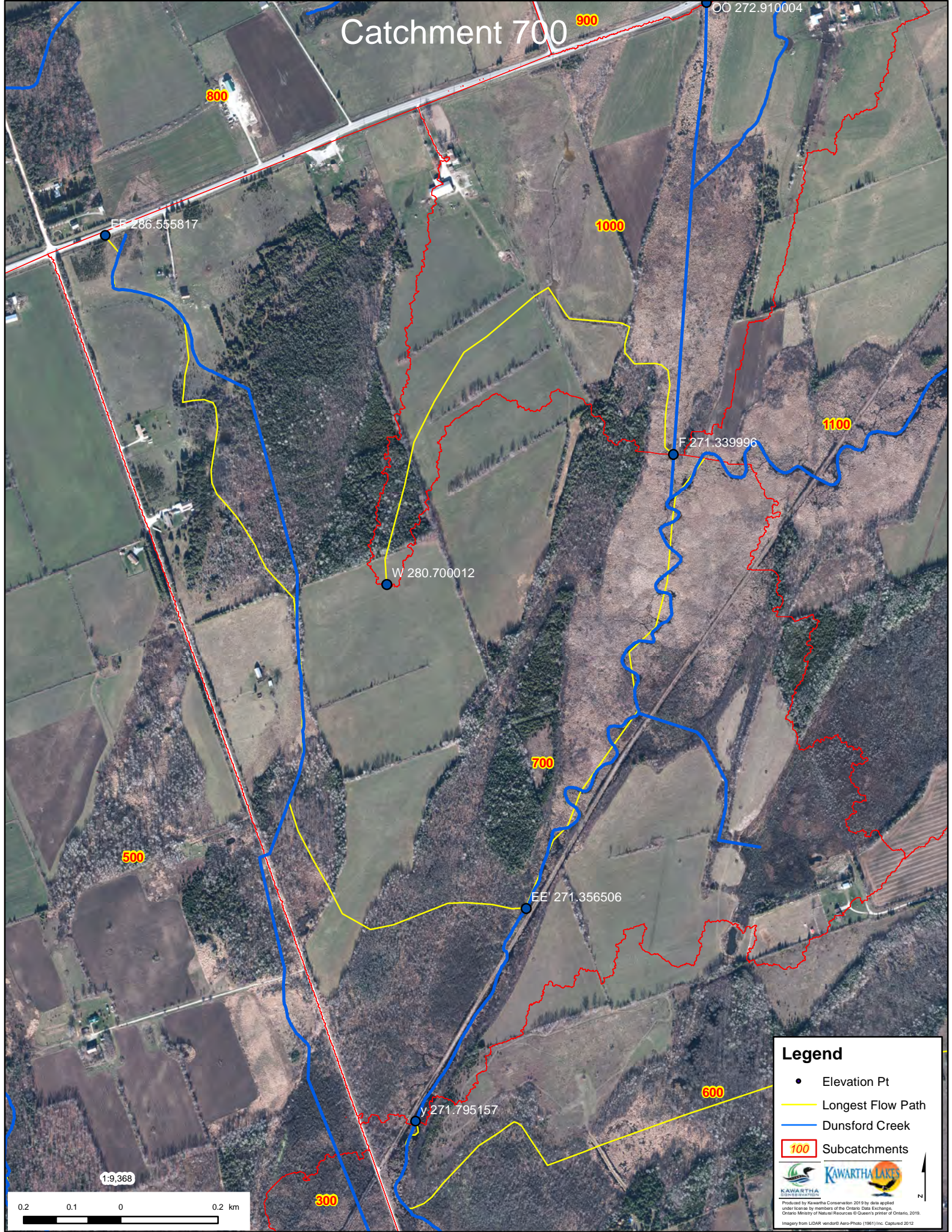
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

KAWARTHA LAKES CONSERVATION

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Catchment 700

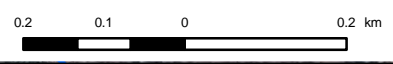


Legend

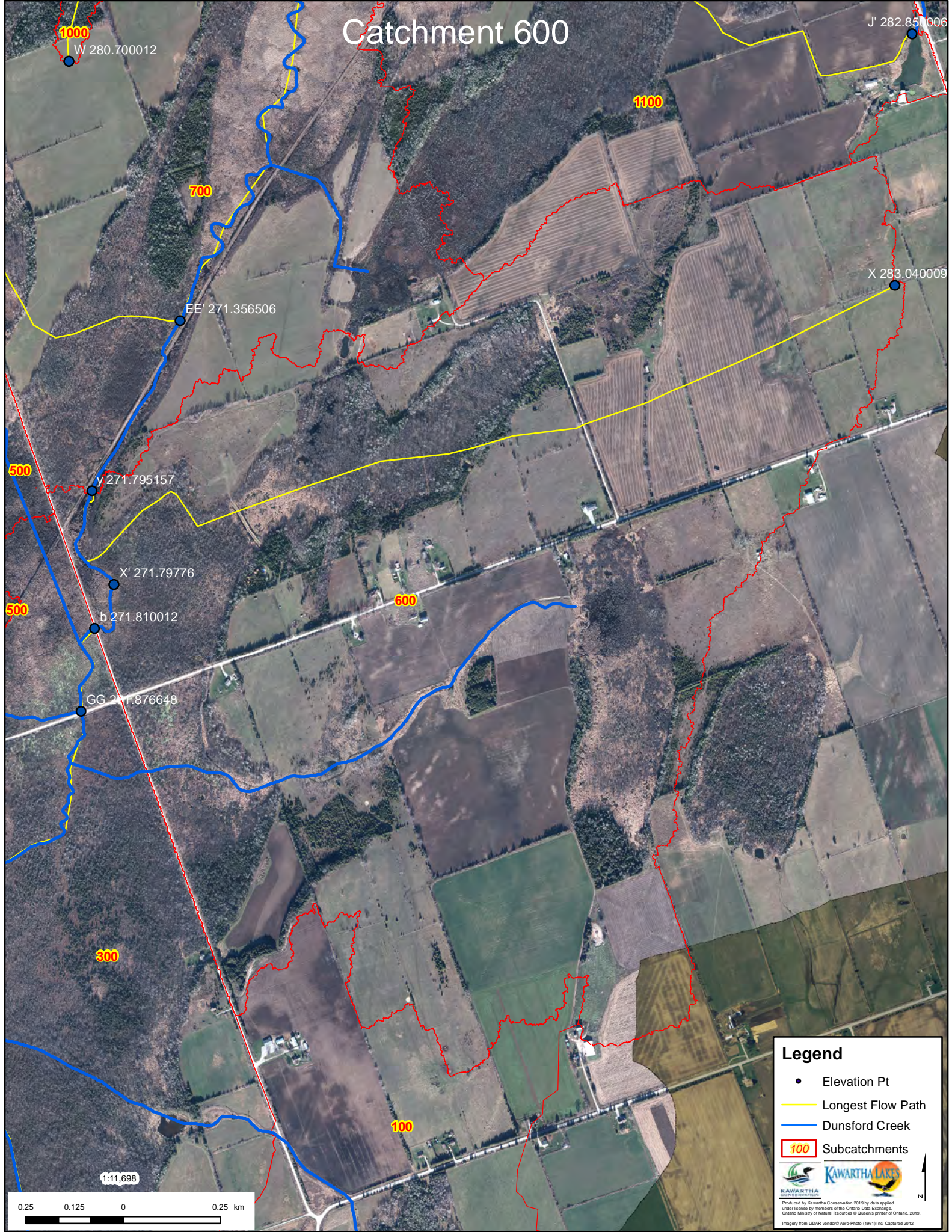
- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments


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Imagery from LGAR veldor® Aero-Photo (1981) Inc. Captured 2012

1:9,368





Catchment 600



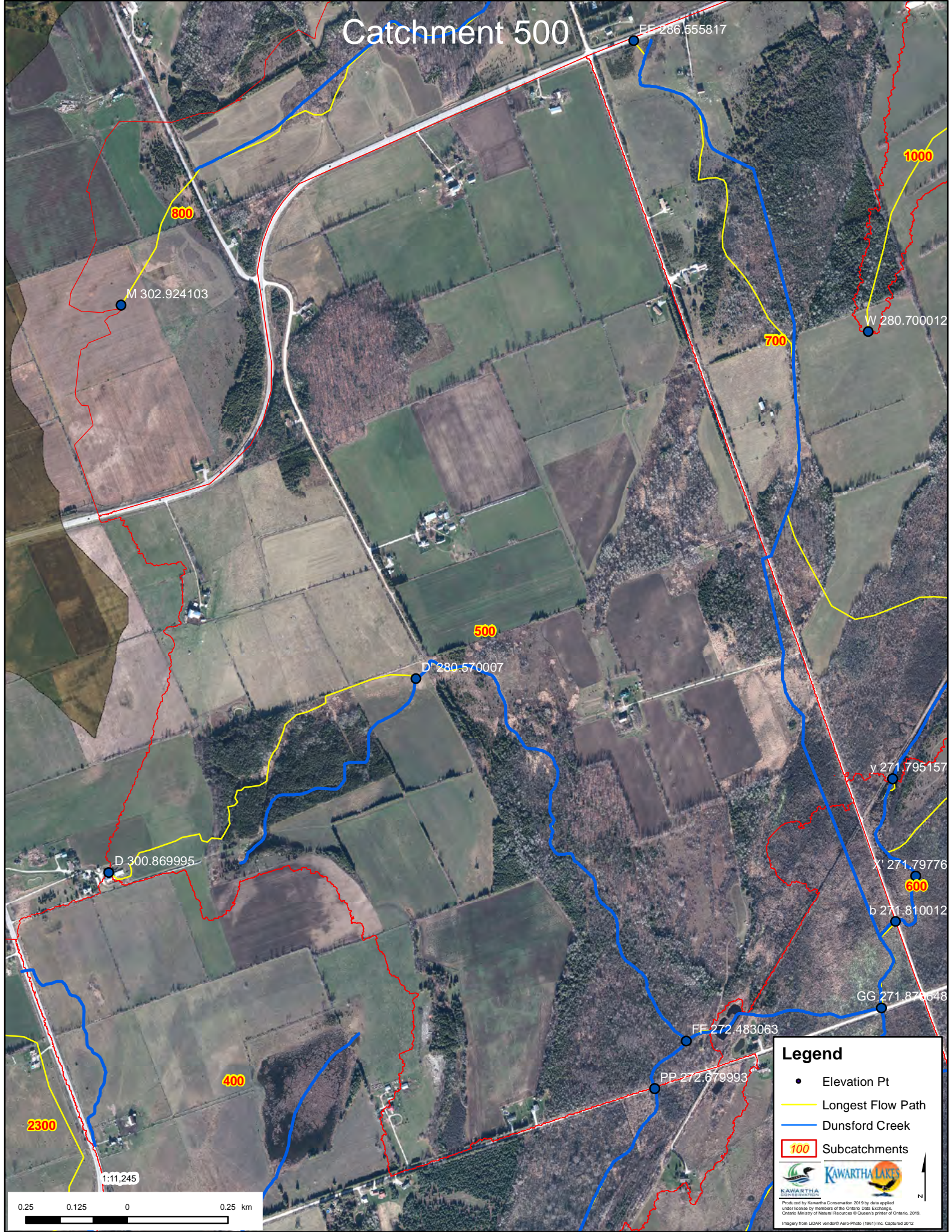
Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 500

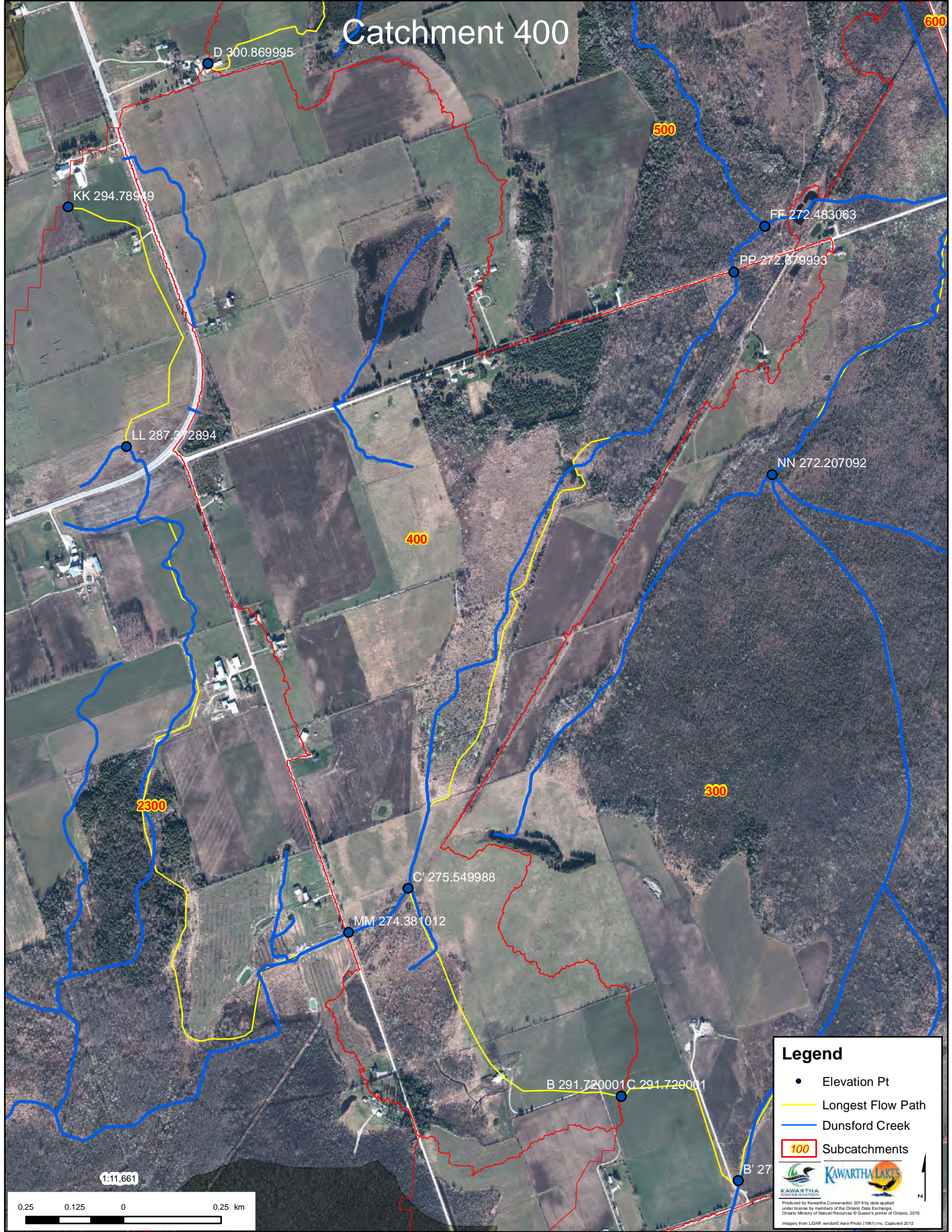


Legend

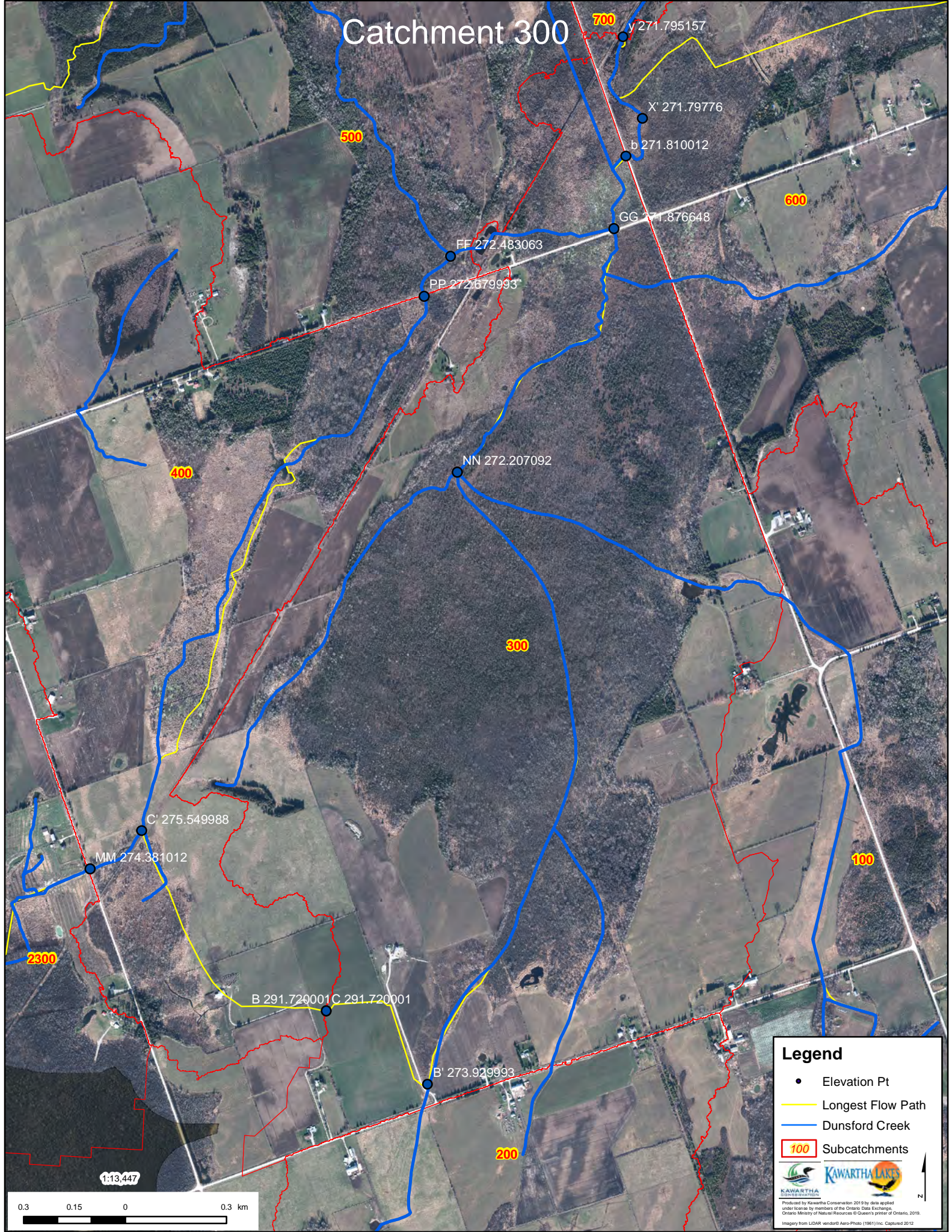
- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 400



Catchment 300



Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100** Subcatchments

 
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Imagery from LGAR vendor: Aero-Photo (1981) Inc. Captured 2012

Catchment 200

400

300

100

200

B 291.720001 C 291.720001

B' 273.929993

Q' 276.059998

Q 290.519989

1:8,111

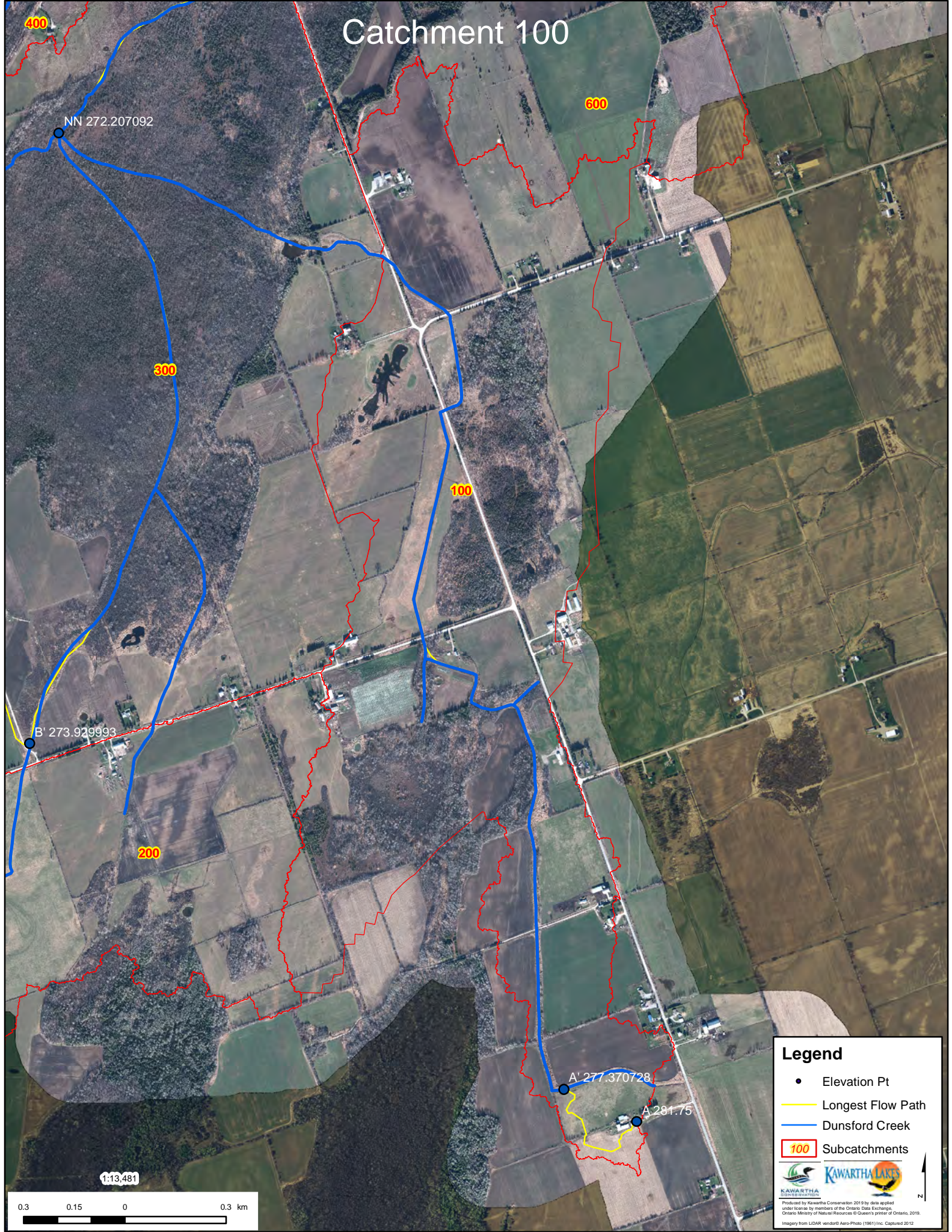


Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

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Catchment 100



Legend

- Elevation Pt
- Longest Flow Path
- Dunsford Creek
- 100 Subcatchments

 
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Imagery from LGAR vendor: Aero-Photo (1981) Inc. Captured 2012

Appendix E
VH Suite Output

100YearSCS6hour Results.txt

```

=====
V   V   I   SSSSS  U   U   A   L
V   V   I   SS    U   U   A A  L
V   V   I   SS    U   U   AAAAA L
V   V   I   SS    U   U   A   A  L
VV    I   SSSSS  UUUUU  A   A  LLLLL

  000  TTTTT  TTTTT  H   H  Y   Y  M   M  000  TM
  0   0   T   T   H   H  Y Y  MM MM  0   0
  0   0   T   T   H   H  Y   M   M  0   0
  000  T   T   H   H  Y   M   M  000

```

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\VO suite 3.0\VO2\voin.dat

Output filename: C:\Users\GAL - Kevin\AppData\Local\Temp\bec36a0b-9f64-4d7f-a130-73c3067dc7e8\Scenario.out

Summary filename: C:\Users\GAL - Kevin\AppData\Local\Temp\bec36a0b-9f64-4d7f-a130-73c3067dc7e8\Scenario.sum

DATE: 04/01/2019

TIME: 02:49:31

USER:

COMMENTS: _____

```

*****
** SIMULATION NUMBER: 0 **
*****

```

```

-----
| READ STORM | Filename: C:\Users\GAL - Kevin\AppData\Local\Temp\bec36a0b-9f64-4d7f-a130-73c3067dc7e8\486ab9ab
| Ptotal= 89.80 mm | Comments: 100 year SCS 6hour storm mm/hr
-----

```

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.17	0.00	1.83	7.20	3.50	28.70	5.17	5.40
0.33	3.60	2.00	7.20	3.67	28.70	5.33	5.40
0.50	3.60	2.17	7.20	3.83	10.80	5.50	5.40
0.67	3.60	2.33	10.80	4.00	10.80	5.67	5.40
0.83	5.40	2.50	10.80	4.17	10.80	5.83	3.60
1.00	5.40	2.67	10.80	4.33	7.20	6.00	3.60
1.17	5.40	2.83	86.10	4.50	7.20	6.17	3.60
1.33	5.40	3.00	86.10	4.67	7.20		

100YearSCS6hour Results.txt

1.50 5.40 | 3.17 86.10 | 4.83 5.40 |
 1.67 5.40 | 3.33 28.70 | 5.00 5.40 |

CALIB
 NASHYD (0100)
 ID= 1 DT=10.0 min

Area (ha)= 197.60 Curve Number (CN)= 67.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 2.63

Unit Hyd Qpeak (cms)= 2.870
 PEAK FLOW (cms)= 3.421 (i)
 TIME TO PEAK (hrs)= 6.333
 RUNOFF VOLUME (mm)= 34.259
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.381

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	277.27	0.1000	
332.34	275.59	0.1000 /0.0500	Main Channel
352.82	273.81	0.0500	Main Channel
365.19	273.82	0.0500	Main Channel
387.54	274.15	0.0500	Main Channel
399.23	275.75	0.0500 /0.1000	Main Channel
500.73	277.20	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.18	273.99	.351E+04	0.8	0.24	73.47
0.36	274.17	.976E+04	3.3	0.37	48.89
0.53	274.34	.175E+05	8.3	0.51	35.01
0.71	274.52	.259E+05	15.2	0.63	28.39
0.89	274.70	.349E+05	23.9	0.73	24.39
1.07	274.88	.446E+05	34.3	0.82	21.66
1.25	275.06	.548E+05	46.5	0.91	19.66
1.42	275.23	.658E+05	60.5	0.99	18.11
1.60	275.41	.774E+05	76.4	1.06	16.86
1.78	275.59	.896E+05	94.2	1.13	15.84
1.96	275.77	.106E+06	116.5	1.18	15.12
2.14	275.95	.130E+06	143.5	1.18	15.11
2.32	276.13	.164E+06	175.1	1.15	15.58
2.50	276.31	.207E+06	212.2	1.10	16.22
2.67	276.48	.258E+06	255.6	1.06	16.86
2.85	276.66	.320E+06	305.9	1.02	17.42
3.03	276.84	.390E+06	363.8	1.00	17.87
3.21	277.02	.469E+06	429.9	0.98	18.20
3.39	277.20	.558E+06	504.8	0.97	18.43

		<---- hydrograph ---->			<-pipe / channel->	
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
INFLOW : ID= 2 (0100)	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
	197.60	3.42	6.33	34.26	0.36	0.37

100YearSCS6hour Results.txt
 OUTFLOW: ID= 1 (****) 197.60 3.27 6.83 34.26 0.35 0.36

CALIB NASHYD (0200) ID= 1 DT=10.0 min	Area (ha)= 107.20 Ia (mm)= 5.00 U.H. Tp(hrs)= 0.87	Curve Number (CN)= 68.0 # of Linear Res.(N)= 3.00
---	--	--

Unit Hyd Qpeak (cms)= 4.706
 PEAK FLOW (cms)= 4.295 (i)
 TIME TO PEAK (hrs)= 4.000
 RUNOFF VOLUME (mm)= 35.190
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.392

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****) IN= 2---> OUT= 1	Routing time step (min)'= 10.00
--------------------------------------	---------------------------------

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	279.83	0.1000	
204.39	277.60	0.0500	Main Channel
296.57	273.96	0.0500	Main Channel
461.97	273.75	0.0500	Main Channel
485.91	272.71	0.0500 /0.1000	Main Channel
798.40	272.85	0.1000	
877.72	273.64	0.1000	
1006.81	276.74	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.21	272.92	.916E+05	3.6	0.08	429.52
0.42	273.13	.237E+06	16.5	0.14	238.88
0.64	273.35	.393E+06	36.9	0.19	177.74
0.85	273.56	.561E+06	64.0	0.23	145.94
1.06	273.77	.739E+06	97.5	0.27	126.27
1.27	273.98	.964E+06	140.8	0.30	114.14
1.48	274.19	.122E+07	202.9	0.34	100.49
1.70	274.41	.149E+07	277.8	0.38	89.31
1.91	274.62	.176E+07	364.6	0.42	80.46
2.12	274.83	.204E+07	462.6	0.46	73.42
2.33	275.04	.232E+07	571.4	0.50	67.71
2.55	275.26	.261E+07	690.7	0.54	63.00
2.76	275.47	.291E+07	820.5	0.57	59.05
2.97	275.68	.321E+07	960.4	0.61	55.69
3.18	275.89	.352E+07	1110.4	0.64	52.79
3.39	276.10	.383E+07	1270.5	0.67	50.26
3.61	276.32	.415E+07	1440.5	0.70	48.03
3.82	276.53	.448E+07	1620.5	0.73	46.05
4.03	276.74	.481E+07	1810.4	0.76	44.28

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel-->	
INFLOW : ID= 2 (0200)	107.20	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
		4.30	4.00	35.19	0.22	0.08

100YearSCS6hour Results.txt
 OUTFLOW: ID= 1 (****) 107.20 1.01 6.50 35.17 0.06 0.08

ADD HYD (0020)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (****):	197.60	3.270	6.83	34.26
+ ID2= 2 (****):	107.20	1.015	6.50	35.17
===== ID = 3 (0020):	304.80	4.277	6.83	34.58

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1 Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	273.19	0.1000	
89.61	271.91	0.1000 /0.0500	Main Channel
138.71	271.70	0.0500	Main Channel
184.80	271.75	0.0500 /0.1000	Main Channel
266.32	271.80	0.1000	
367.88	271.93	0.1000	
520.40	272.09	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.02	271.72	.159E+03	0.0	0.01	*****
0.03	271.73	.634E+03	0.0	0.02	694.13
0.05	271.75	.143E+04	0.0	0.03	529.62
0.07	271.77	.306E+04	0.1	0.04	405.42
0.09	271.79	.551E+04	0.3	0.04	365.74
0.11	271.81	.873E+04	0.4	0.05	336.92
0.13	271.83	.124E+05	0.7	0.05	310.09
0.16	271.86	.166E+05	1.0	0.06	288.06
0.18	271.88	.211E+05	1.3	0.06	269.92
0.20	271.90	.262E+05	1.7	0.06	254.75
0.22	271.92	.317E+05	2.2	0.07	239.31
0.24	271.94	.376E+05	2.8	0.07	224.81
0.26	271.96	.439E+05	3.4	0.08	213.43
0.28	271.98	.507E+05	4.1	0.08	203.95
0.30	272.00	.579E+05	4.9	0.08	195.88
0.33	272.03	.656E+05	5.8	0.09	188.88
0.35	272.05	.738E+05	6.7	0.09	182.73
0.37	272.07	.824E+05	7.7	0.09	177.27
0.39	272.09	.915E+05	8.8	0.10	172.36

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0020)	304.80	4.28	6.83	34.58	0.29	0.08
OUTFLOW: ID= 1 (****)	304.80	2.59	8.83	34.56	0.23	0.07

100YearSCS6hour Results.txt

CALIB
NASHYD (0400)
ID= 1 DT=10.0 min

Area (ha)= 228.10 Curve Number (CN)= 67.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.65

Unit Hyd Qpeak (cms)= 5.280
PEAK FLOW (cms)= 5.620 (i)
TIME TO PEAK (hrs)= 5.000
RUNOFF VOLUME (mm)= 34.258
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.381

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->
Distance Elevation Manning
0.00 276.00 0.1000
91.20 274.69 0.1000
174.02 274.10 0.1000
210.03 273.92 0.1000
333.58 273.80 0.1000 /0.0500 Main Channel
368.08 273.64 0.0500 Main Channel
385.33 273.85 0.0500 /0.1000 Main Channel
462.42 275.22 0.1000
531.42 275.33 0.1000

<----- TRAVEL TIME TABLE ----->
DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
(m) (m) (cu.m.) (cms) (m/s) (min)
0.08 273.72 .220E+03 0.1 0.07 54.86
0.16 273.80 .880E+03 0.4 0.11 34.56
0.25 273.89 .291E+04 1.6 0.13 29.37
0.34 273.98 .663E+04 4.2 0.15 26.31
0.43 274.07 .109E+05 8.0 0.17 22.70
0.52 274.16 .157E+05 13.0 0.19 20.01
0.61 274.25 .208E+05 19.2 0.21 18.01
0.70 274.34 .263E+05 26.5 0.23 16.50
0.79 274.43 .321E+05 34.9 0.25 15.32
0.88 274.52 .383E+05 44.5 0.27 14.36
0.97 274.61 .449E+05 55.2 0.28 13.57
1.06 274.70 .519E+05 67.1 0.30 12.88
1.15 274.79 .591E+05 80.7 0.32 12.21
1.24 274.88 .666E+05 95.5 0.33 11.62
1.33 274.97 .743E+05 111.4 0.35 11.11
1.42 275.06 .822E+05 128.5 0.36 10.66
1.51 275.15 .904E+05 146.8 0.38 10.26
1.60 275.24 .989E+05 165.2 0.39 9.97
1.69 275.33 .108E+06 183.2 0.39 9.85

<---- hydrograph ----> <-pipe / channel->
AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
(ha) (cms) (hrs) (mm) (m) (m/s)
INFLOW : ID= 2 (0400) 228.10 5.62 5.00 34.26 0.37 0.15
OUTFLOW: ID= 1 (****) 228.10 5.32 5.50 34.26 0.37 0.15

100YearsSCS6hour Results.txt

```

-----
| CALIB                               |
| NASHYD      (0500)                 |
| ID= 1 DT=10.0 min                 |
|-----|-----|-----|-----|
| Area      (ha)= 302.30             |
| Ia        (mm)= 5.00               |
| U.H. Tp(hrs)= 1.31                |
| Curve Number (CN)= 67.0           |
| # of Linear Res.(N)= 3.00         |

```

```

Unit Hyd Qpeak (cms)= 8.814

PEAK FLOW      (cms)= 8.831 (i)
TIME TO PEAK   (hrs)= 4.667
RUNOFF VOLUME  (mm)= 34.258
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.381

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| CALIB                               |
| NASHYD      (2300)                 |
| ID= 1 DT=10.0 min                 |
|-----|-----|-----|-----|
| Area      (ha)= 308.80             |
| Ia        (mm)= 5.00               |
| U.H. Tp(hrs)= 1.85                |
| Curve Number (CN)= 64.0           |
| # of Linear Res.(N)= 3.00         |

```

```

Unit Hyd Qpeak (cms)= 6.375

PEAK FLOW      (cms)= 6.419 (i)
TIME TO PEAK   (hrs)= 5.333
RUNOFF VOLUME  (mm)= 31.585
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.352

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ROUTE CHN (****)                   |
| IN= 2---> OUT= 1                   |
|-----|-----|-----|-----|
| Routing time step (min)'= 10.00    |

```

```

<----- DATA FOR SECTION ( 1.1) ----->
Distance      Elevation      Manning
  0.00         274.69         0.1000
  82.82         274.10         0.1000
 118.83         273.92         0.1000
 242.38         273.80         0.1000 /0.0500 Main Channel
 276.88         273.64         0.0500 Main Channel
 294.13         273.85         0.0500 /0.1000 Main Channel
 371.22         275.22         0.1000
 440.22         275.33         0.1000

```

```

<----- TRAVEL TIME TABLE ----->
DEPTH      ELEV      VOLUME      FLOW RATE      VELOCITY      TRAV.TIME
(m)        (m)        (cu.m.)     (cms)          (m/s)        (min)
0.05      273.69     .907E+03     0.0            0.05         711.92
0.11      273.75     .363E+04     0.1            0.08         448.48
0.16      273.80     .816E+04     0.4            0.10         342.25
0.22      273.86     .175E+05     1.0            0.12         298.74
0.27      273.91     .342E+05     2.0            0.12         287.79
0.33      273.97     .560E+05     3.5            0.13         266.60
0.38      274.02     .797E+05     5.5            0.15         242.26
0.44      274.08     .105E+06     7.9            0.16         222.10
0.49      274.13     .132E+06     10.7           0.17         205.22
0.55      274.19     .160E+06     14.0           0.19         191.05
0.60      274.24     .190E+06     17.7           0.20         179.33

```

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0.66	274.30	.221E+06	21.7	0.21	169.47
0.72	274.36	.253E+06	26.2	0.22	161.07
0.77	274.41	.287E+06	31.1	0.23	153.82
0.83	274.47	.321E+06	36.3	0.24	147.48
0.88	274.52	.358E+06	42.0	0.25	141.88
0.94	274.58	.395E+06	48.1	0.26	136.90
0.99	274.63	.434E+06	54.6	0.27	132.43
1.05	274.69	.474E+06	61.5	0.28	128.38

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (2300)	308.80	6.42	5.33	31.58	0.40	0.15
OUTFLOW: ID= 1 (****)	308.80	3.08	7.50	31.57	0.31	0.13

ADD HYD (0010)					
1 + 2 = 3					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 1 (****):	308.80	3.083	7.50	31.57	
+ ID2= 2 (****):	228.10	5.325	5.50	34.26	
=====					
ID = 3 (0010):	536.90	7.602	6.00	32.71	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0010)					
3 + 2 = 1					
	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	
ID1= 3 (0010):	536.90	7.602	6.00	32.71	
+ ID2= 2 (0500):	302.30	8.831	4.67	34.26	
=====					
ID = 1 (0010):	839.20	15.057	5.17	33.27	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)		Routing time step (min)'= 10.00
IN= 2	OUT= 1	

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
0.00	272.10	0.1000	
34.80	271.88	0.0500	Main Channel
68.44	271.83	0.0500	Main Channel
76.43	271.69	0.0500	Main Channel
82.05	271.69	0.0500	Main Channel
110.40	271.81	0.0500 /0.1000	Main Channel
127.77	271.89	0.1000	
150.00	272.05	0.1000	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.02	271.71	.635E+02	0.0	0.05	165.35
0.03	271.72	.166E+03	0.0	0.07	112.65

100YearSCS6hour Results.txt

0.05	271.74	.308E+03	0.1	0.08	89.85
0.07	271.76	.490E+03	0.1	0.10	76.31
0.09	271.78	.710E+03	0.2	0.11	67.08
0.10	271.79	.970E+03	0.3	0.13	60.27
0.12	271.81	.127E+04	0.4	0.14	55.00
0.14	271.83	.161E+04	0.6	0.16	48.44
0.16	271.85	.209E+04	0.7	0.15	49.64
0.18	271.87	.273E+04	0.9	0.15	50.05
0.20	271.89	.353E+04	1.2	0.16	47.38
0.22	271.91	.441E+04	1.7	0.18	42.48
0.24	271.93	.534E+04	2.3	0.20	38.91
0.26	271.95	.633E+04	2.9	0.21	36.19
0.28	271.97	.737E+04	3.6	0.22	34.02
0.30	271.99	.847E+04	4.4	0.24	32.26
0.32	272.01	.962E+04	5.2	0.25	30.78
0.34	272.03	.108E+05	6.1	0.26	29.53
0.36	272.05	.121E+05	7.1	0.27	28.45

**** WARNING: TRAVEL TIME TABLE EXCEEDED

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0010)	839.20	15.06	5.17	33.27	0.35	0.26
OUTFLOW: ID= 1 (****)	839.20	14.19	5.67	33.27	0.36	0.27

ADD HYD (0030)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	304.80	2.593	8.83	34.56
+ ID2= 2 (****):	839.20	14.187	5.67	33.27
=====				
ID = 3 (0030):	1144.00	15.288	6.00	33.61

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 5.00

Distance	Elevation	Manning	
0.00	273.19	0.1000	
89.61	271.91	0.1000 / 0.0500	Main Channel
138.71	271.70	0.0500	Main Channel
184.80	271.75	0.0500 / 0.1000	Main Channel
266.32	271.80	0.1000	
367.88	271.93	0.1000	
520.40	272.09	0.1000	
714.30	273.40	0.1000	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.05	271.75	.365E+03	0.0	0.03	147.14
0.13	271.83	.275E+04	0.5	0.05	89.17
0.20	271.90	.688E+04	1.6	0.06	70.23
0.28	271.98	.124E+05	3.6	0.07	57.38
0.35	272.05	.195E+05	6.4	0.08	50.32

100YearsSCS6hour Results.txt

0.43	272.13	.278E+05	10.4	0.09	44.57
0.50	272.20	.366E+05	15.5	0.11	39.50
0.58	272.28	.457E+05	21.4	0.12	35.69
0.66	272.36	.552E+05	28.1	0.13	32.73
0.73	272.43	.649E+05	35.6	0.14	30.37
0.81	272.51	.750E+05	44.0	0.15	28.43
0.88	272.58	.854E+05	53.1	0.16	26.81
0.96	272.66	.961E+05	63.0	0.17	25.43
1.04	272.74	.107E+06	73.7	0.17	24.24
1.11	272.81	.118E+06	85.1	0.18	23.21
1.19	272.89	.130E+06	97.3	0.19	22.29
1.26	272.96	.142E+06	110.3	0.20	21.48
1.34	273.04	.154E+06	124.0	0.20	20.75
1.41	273.11	.167E+06	138.6	0.21	20.09

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel-->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0030)	1144.00	15.29	6.00	33.61	0.50	0.11
OUTFLOW:	ID= 1 (****)	1144.00	13.96	6.50	33.61	0.48	0.10

```

CALIB
NASHYD (0300)
ID= 1 DT=10.0 min
    
```

```

Area (ha)= 315.50      Curve Number (CN)= 54.0
Ia (mm)= 5.00         # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 2.03
    
```

Unit Hyd Qpeak (cms)= 5.936

```

PEAK FLOW (cms)= 4.599 (i)
TIME TO PEAK (hrs)= 5.500
RUNOFF VOLUME (mm)= 23.877
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.266
    
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

ADD HYD (0125)
1 + 2 = 3
    
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	1144.00	13.963	6.50	33.61
+ ID2= 2 (0300):	315.50	4.599	5.50	23.88
===== ID = 3 (0125):	1459.50	18.224	6.25	31.51

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

ROUTE CHN (****)
IN= 2----> OUT= 1
    
```

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
133.75	272.89	0.1000	
157.66	271.71	0.0500 /0.1000	Main Channel
506.36	271.74	0.1000	
524.97	272.90	0.1000	

100YearSCS6hour Results.txt

----- TRAVEL TIME TABLE -----					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.06	271.77	.787E+04	0.6	0.04	211.05
0.12	271.83	.183E+05	2.5	0.07	120.74
0.19	271.90	.288E+05	5.4	0.09	89.62
0.25	271.96	.394E+05	9.0	0.11	73.08
0.31	272.02	.500E+05	13.3	0.13	62.58
0.37	272.08	.607E+05	18.3	0.14	55.23
0.43	272.14	.715E+05	23.9	0.16	49.74
0.50	272.21	.823E+05	30.2	0.18	45.47
0.56	272.27	.932E+05	37.0	0.19	42.03
0.62	272.33	.104E+06	44.3	0.20	39.19
0.68	272.39	.115E+06	52.2	0.22	36.80
0.75	272.46	.126E+06	60.6	0.23	34.76
0.81	272.52	.137E+06	69.5	0.24	32.98
0.87	272.58	.149E+06	78.8	0.25	31.43
0.93	272.64	.160E+06	88.7	0.26	30.06
0.99	272.70	.171E+06	99.1	0.28	28.83
1.06	272.77	.183E+06	109.9	0.29	27.73
1.12	272.83	.194E+06	121.1	0.30	26.73
1.18	272.89	.206E+06	132.8	0.31	25.83

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel-->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0125)	1459.50	18.22	6.25	31.51	0.37	0.14
OUTFLOW: ID= 1 (****)	1459.50	16.06	6.83	31.51	0.34	0.14

CALIB		Area (ha)= 299.60		Curve Number (CN)= 63.0	
NASHYD (0600)	ID= 1 DT=10.0 min	Ia (mm)= 5.00	U.H. Tp(hrs)= 1.85	# of Linear Res.(N)= 3.00	

Unit Hyd Qpeak (cms)= 6.186

PEAK FLOW (cms)= 6.056 (i)
 TIME TO PEAK (hrs)= 5.333
 RUNOFF VOLUME (mm)= 30.734
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.342

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0040)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (****)	:	1459.50	16.060	6.83	31.51
+ ID2= 2 (0600)	:	299.60	6.056	5.33	30.73
=====		=====			
ID = 3 (0040)	:	1759.10	20.955	6.50	31.37

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

100yearSCS6hour Results.txt

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	280.66	0.1000	
230.75	272.35	0.0500 /0.1000	Main Channel
454.64	271.34	0.1000	
776.25	271.91	0.1000	
796.25	273.69	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.12	271.46	.111E+05	0.2	0.03	*****
0.25	271.59	.443E+05	1.1	0.05	681.82
0.37	271.71	.996E+05	3.2	0.06	520.33
0.49	271.83	.177E+06	6.9	0.07	429.52
0.62	271.96	.275E+06	12.8	0.09	359.68
0.74	272.08	.383E+06	21.2	0.10	301.05
0.87	272.21	.498E+06	31.8	0.12	261.00
0.99	272.33	.619E+06	44.5	0.13	231.74
1.11	272.45	.744E+06	60.8	0.15	204.11
1.24	272.58	.871E+06	79.5	0.17	182.72
1.36	272.70	.999E+06	100.2	0.18	166.24
1.48	272.82	.113E+07	122.8	0.20	153.09
1.61	272.95	.126E+07	147.3	0.22	142.33
1.73	273.07	.139E+07	173.7	0.23	133.33
1.86	273.20	.152E+07	201.8	0.24	125.68
1.98	273.32	.166E+07	231.7	0.26	119.08
2.10	273.44	.179E+07	263.2	0.27	113.32
2.23	273.57	.193E+07	296.4	0.28	108.24
2.35	273.69	.206E+07	331.3	0.30	103.73

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0040)	1759.10	20.96	6.50	31.37	0.74	0.10
OUTFLOW: ID= 1 (****)	1759.10	9.68	8.42	31.37	0.55	0.08

CALIB
NASHYD (0700)
ID= 1 DT=10.0 min

Area (ha)= 181.20 Curve Number (CN)= 60.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.89

Unit Hyd Qpeak (cms)= 3.662
PEAK FLOW (cms)= 3.313 (i)
TIME TO PEAK (hrs)= 5.333
RUNOFF VOLUME (mm)= 28.296
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.315

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB
NASHYD (1000)
ID= 1 DT=10.0 min

Area (ha)= 69.40 Curve Number (CN)= 67.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

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U.H. Tp(hrs)= 1.06

Unit Hyd Qpeak (cms)= 2.501
 PEAK FLOW (cms)= 2.364 (i)
 TIME TO PEAK (hrs)= 4.333
 RUNOFF VOLUME (mm)= 34.257
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.381

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0050)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (1000):	69.40	2.364	4.33	34.26
+ ID2= 2 (****):	1759.10	9.683	8.42	31.37
=====				
ID = 3 (0050):	1828.50	9.809	8.33	31.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0050)
 3 + 2 = 1

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0050):	1828.50	9.809	8.33	31.48
+ ID2= 2 (0700):	181.20	3.313	5.33	28.30
=====				
ID = 1 (0050):	2009.70	11.308	7.58	31.19

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
 NASHYD (0800)
 ID= 1 DT=10.0 min

Area (ha)= 183.20 Curve Number (CN)= 68.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.53

Unit Hyd Qpeak (cms)= 4.573
 PEAK FLOW (cms)= 4.910 (i)
 TIME TO PEAK (hrs)= 4.833
 RUNOFF VOLUME (mm)= 35.193
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.392

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0009)
 IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 8.00 272.30 0.1000

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35.00	271.80	0.1000 /0.0500	Main Channel
50.00	271.50	0.0500	Main Channel
80.00	271.80	0.0500 /0.1000	Main Channel
142.00	272.20	0.1000	
150.00	272.10	0.1000	
228.00	273.20	0.1000	
288.00	275.23	0.1000	

----- TRAVEL TIME TABLE -----

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.04	271.54	.150E+03	0.0	0.06	415.02
0.08	271.58	.599E+03	0.0	0.09	261.44
0.11	271.61	.135E+04	0.1	0.12	199.52
0.15	271.65	.240E+04	0.2	0.14	164.70
0.19	271.69	.374E+04	0.4	0.17	141.93
0.23	271.73	.539E+04	0.7	0.19	125.69
0.26	271.76	.734E+04	1.1	0.21	113.41
0.30	271.80	.958E+04	1.5	0.23	103.74
0.35	271.85	.128E+05	2.4	0.27	88.84
0.39	271.89	.166E+05	3.4	0.29	80.63
0.44	271.94	.210E+05	4.7	0.31	75.41
0.48	271.98	.261E+05	6.1	0.33	71.76
0.53	272.03	.318E+05	7.7	0.34	69.01
0.57	272.07	.380E+05	9.5	0.35	66.83
0.62	272.12	.450E+05	11.5	0.36	65.24
0.66	272.16	.528E+05	13.7	0.37	64.35
0.71	272.21	.618E+05	16.2	0.37	63.59
0.75	272.25	.713E+05	19.1	0.38	62.29
0.80	272.30	.812E+05	22.2	0.39	60.90

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0800)	183.20	4.91	4.83	35.19	0.44	0.32
OUTFLOW: ID= 1 (0009)	183.20	3.81	6.00	35.18	0.40	0.30

 | CALIB
 | NASHYD (0900)
 | ID= 1 DT=10.0 min |

Area (ha)= 236.70 Curve Number (CN)= 64.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.97

Unit Hyd Qpeak (cms)= 4.589
 PEAK FLOW (cms)= 4.693 (i)
 TIME TO PEAK (hrs)= 5.500
 RUNOFF VOLUME (mm)= 31.585
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.352

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 | ADD HYD (0070)
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0009):	183.20	3.811	6.00	35.18
+ ID2= 2 (0900):	236.70	4.693	5.50	31.58

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=====
 ID = 3 (0070): 419.90 8.430 5.67 33.15
 =====

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 | ROUTE CHN (****) |
 | IN= 2----> OUT= 1 |

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 16.00 272.32 0.1000
 55.00 271.60 0.1000 /0.0500 Main Channel
 64.00 270.90 0.0500 Main Channel
 129.00 271.30 0.0500 /0.1000 Main Channel
 151.00 271.51 0.1000
 193.00 271.75 0.1000
 296.00 272.52 0.1000

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.07	270.97	.364E+03	0.0	0.08	183.39
0.13	271.03	.146E+04	0.2	0.13	115.51
0.20	271.10	.328E+04	0.6	0.18	88.15
0.27	271.17	.582E+04	1.3	0.21	72.77
0.33	271.23	.910E+04	2.4	0.25	62.71
0.40	271.30	.131E+05	3.9	0.28	55.53
0.48	271.38	.186E+05	6.8	0.34	45.54
0.56	271.46	.247E+05	10.3	0.39	39.89
0.64	271.54	.316E+05	14.5	0.43	36.24
0.71	271.61	.394E+05	19.4	0.46	33.82
0.79	271.69	.485E+05	25.2	0.49	32.05
0.87	271.77	.589E+05	31.9	0.51	30.81
0.95	271.85	.705E+05	39.4	0.52	29.81
1.03	271.93	.831E+05	47.8	0.54	28.98
1.11	272.01	.968E+05	57.1	0.55	28.26
1.18	272.08	.112E+06	67.3	0.56	27.63
1.26	272.16	.127E+06	78.4	0.58	27.07
1.34	272.24	.144E+06	90.6	0.59	26.56
1.42	272.32	.162E+06	103.7	0.60	26.09

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	419.90	8.43	5.67	33.15	0.51	0.36
OUTFLOW: ID= 1 (****)	419.90	7.87	6.33	33.15	0.50	0.35

 | ADD HYD (0060) |
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	419.90	7.874	6.33	33.15
+ ID2= 2 (0050):	2009.70	11.308	7.58	31.19
===== ID = 3 (0060):	2429.60	18.624	6.83	31.53

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ROUTE CHN (****) |
 IN= 2---> OUT= 1 | Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->
 Distance Elevation Manning
 90.00 276.61 0.1000
 140.00 273.00 0.1000
 152.00 271.10 0.1000 /0.0500 Main Channel
 160.00 271.10 0.0500 /0.1000 Main Channel
 168.00 271.51 0.1000
 230.00 271.51 0.1000
 252.00 274.18 0.1000
 280.00 276.18 0.1000

<----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME
 (m) (m) (cu.m.) (cms) (m/s) (min)
 0.27 271.37 .253E+04 0.4 0.13 104.52
 0.53 271.63 .129E+05 1.8 0.11 120.57
 0.80 271.90 .315E+05 5.7 0.15 92.29
 1.07 272.17 .510E+05 11.5 0.19 73.61
 1.34 272.44 .714E+05 19.1 0.22 62.18
 1.60 272.70 .926E+05 28.3 0.25 54.48
 1.87 272.97 .115E+06 39.1 0.28 48.92
 2.14 273.24 .138E+06 51.1 0.31 44.89
 2.41 273.51 .162E+06 64.8 0.33 41.71
 2.67 273.77 .188E+06 80.0 0.35 39.11
 2.94 274.04 .215E+06 96.9 0.37 36.95
 3.21 274.31 .243E+06 115.0 0.39 35.25
 3.48 274.58 .273E+06 134.3 0.41 33.89
 3.74 274.84 .305E+06 155.4 0.42 32.68
 4.01 275.11 .338E+06 178.3 0.44 31.60
 4.28 275.38 .373E+06 203.0 0.45 30.62
 4.55 275.65 .409E+06 229.5 0.46 29.72
 4.81 275.91 .448E+06 258.1 0.48 28.90
 5.08 276.18 .487E+06 288.6 0.49 28.14

<---- hydrograph ----> <-pipe / channel->
 AREA QPEAK TPEAK R.V. MAX DEPTH MAX VEL
 (ha) (cms) (hrs) (mm) (m) (m/s)
 INFLOW : ID= 2 (0060) 2429.60 18.62 6.83 31.53 1.32 0.22
 OUTFLOW: ID= 1 (****) 2429.60 16.43 7.42 31.53 1.24 0.21

CALIB
 NASHYD (1100) Area (ha)= 203.07 Curve Number (CN)= 70.0
 ID= 1 DT=10.0 min Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.74

Unit Hyd Qpeak (cms)= 4.458
 PEAK FLOW (cms)= 5.222 (i)
 TIME TO PEAK (hrs)= 5.167
 RUNOFF VOLUME (mm)= 37.133
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.414

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100YearSCS6hour Results.txt

ADD HYD (0080)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2429.60	16.427	7.42	31.53
+ ID2= 2 (1100):	203.07	5.222	5.17	37.13
=====				
ID = 3 (0080):	2632.67	19.548	6.92	31.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
44.00	272.20	0.0700	
75.00	270.40	0.0700	
76.00	268.80	0.0700 /0.0500	Main Channel
80.00	268.70	0.0500	Main Channel
84.00	268.10	0.0500	Main Channel
88.00	269.90	0.0500 /0.0700	Main Channel
135.00	271.98	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.17	268.27	.563E+02	0.0	0.34	20.26
0.35	268.45	.225E+03	0.3	0.54	12.76
0.52	268.62	.507E+03	0.9	0.71	9.74
0.70	268.80	.970E+03	1.6	0.68	10.11
0.91	269.01	.183E+04	4.4	1.00	6.87
1.12	269.22	.275E+04	8.4	1.26	5.46
1.34	269.44	.372E+04	13.4	1.49	4.64
1.55	269.65	.475E+04	19.3	1.68	4.10
1.76	269.86	.582E+04	26.2	1.86	3.71
1.97	270.07	.708E+04	34.7	2.03	3.40
2.18	270.28	.876E+04	44.9	2.12	3.25
2.40	270.50	.109E+05	56.8	2.16	3.20
2.61	270.71	.137E+05	71.3	2.15	3.21
2.82	270.92	.173E+05	88.8	2.12	3.25
3.03	271.13	.216E+05	109.9	2.10	3.28
3.24	271.34	.267E+05	135.0	2.09	3.30
3.46	271.56	.325E+05	164.4	2.09	3.29
3.67	271.77	.390E+05	198.6	2.11	3.27
3.88	271.98	.463E+05	238.0	2.13	3.24

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0080)	2632.67	19.55	6.92	31.96	1.56	1.69
OUTFLOW: ID= 1 (****)	2632.67	19.55	7.00	31.96	1.55	1.69

CALIB
NASHYD (1200)
ID= 1 DT=10.0 min

Area (ha)= 30.80 Curve Number (CN)= 78.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00

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U.H. Tp(hrs)= 0.85

Unit Hyd Qpeak (cms)= 1.384

PEAK FLOW (cms)= 1.672 (i)
 TIME TO PEAK (hrs)= 4.000
 RUNOFF VOLUME (mm)= 45.962
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.512

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0090)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2632.67	19.545	7.00	31.96
+ ID2= 2 (1200):	30.80	1.672	4.00	45.96
=====				
ID = 3 (0090):	2663.47	19.774	7.00	32.12

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
18.00	268.20	0.0700	
29.00	266.80	0.0700	
50.50	266.10	0.0700	
57.00	264.70	0.0700 /0.0500	Main channel
60.50	264.60	0.0500	Main channel
66.00	264.72	0.0500 /0.0700	Main channel
77.80	267.30	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	264.70	.416E+03	0.1	0.28	61.42
0.24	264.84	.175E+04	1.1	0.64	26.84
0.37	264.97	.327E+04	2.9	0.90	19.08
0.51	265.11	.497E+04	5.3	1.11	15.51
0.65	265.25	.685E+04	8.5	1.28	13.40
0.78	265.38	.890E+04	12.4	1.43	11.98
0.92	265.52	.111E+05	16.9	1.57	10.95
1.06	265.66	.135E+05	22.2	1.69	10.16
1.19	265.79	.161E+05	28.2	1.80	9.53
1.33	265.93	.189E+05	34.9	1.90	9.01
1.47	266.07	.218E+05	42.4	2.00	8.58
1.61	266.21	.251E+05	49.7	2.04	8.42
1.74	266.34	.290E+05	58.3	2.07	8.30
1.88	266.48	.336E+05	68.3	2.09	8.21
2.02	266.62	.389E+05	79.9	2.11	8.13
2.15	266.75	.449E+05	93.0	2.13	8.05
2.29	266.89	.515E+05	108.5	2.17	7.91
2.43	267.03	.583E+05	126.0	2.22	7.71
2.56	267.16	.654E+05	145.1	2.28	7.51

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		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0090)	2663.47	19.77	7.00	32.12	0.99	1.63
OUTFLOW:	ID= 1 (****)	2663.47	19.73	7.08	32.12	0.99	1.63

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD (1300)	42.90	80.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.53	

unit Hyd Qpeak (cms)= 3.092

PEAK FLOW (cms)= 3.294 (i)

TIME TO PEAK (hrs)= 3.667

RUNOFF VOLUME (mm)= 48.459

TOTAL RAINFALL (mm)= 89.800

RUNOFF COEFFICIENT = 0.540

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0101)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (****):	2663.47	19.731	7.08	32.12
+ ID2= 2 (1300):	42.90	3.294	3.67	48.46
=====				
ID = 3 (0101):	2706.37	19.843	7.08	32.38

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)	Routing time step (min)'
IN= 2---> OUT= 1	= 10.00

Distance	Elevation	Manning	
0.00	259.27	0.0700	
224.90	256.32	0.0500 / 0.0700	Main Channel
234.22	255.44	0.0700	
241.28	255.24	0.0700	
245.63	256.44	0.0700	
278.81	257.64	0.0700	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	255.34	.588E+02	0.0	0.11	46.94
0.20	255.44	.235E+03	0.1	0.17	29.57
0.33	255.57	.576E+03	0.5	0.28	17.82
0.46	255.70	.988E+03	1.2	0.37	13.64
0.59	255.83	.147E+04	2.2	0.44	11.35
0.72	255.96	.203E+04	3.4	0.51	9.86
0.85	256.09	.266E+04	5.0	0.57	8.80
0.98	256.22	.336E+04	7.0	0.63	7.99
1.11	256.35	.414E+04	9.4	0.69	7.32

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1.24	256.48	.522E+04	12.2	0.71	7.12
1.36	256.60	.679E+04	15.2	0.68	7.45
1.49	256.73	.890E+04	19.6	0.67	7.57
1.62	256.86	.115E+05	25.5	0.67	7.55
1.75	256.99	.147E+05	33.0	0.68	7.42
1.88	257.12	.184E+05	42.3	0.70	7.23
2.01	257.25	.226E+05	53.6	0.72	7.01
2.14	257.38	.273E+05	67.0	0.74	6.79
2.27	257.51	.325E+05	82.7	0.77	6.56
2.40	257.64	.383E+05	100.8	0.80	6.34

		<---- hydrograph ---->				<-pipe / channel-->	
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0101)	2706.37	19.84	7.08	32.38	1.50	0.67
OUTFLOW:	ID= 1 (****)	2706.37	19.79	7.17	32.38	1.50	0.67

```

CALIB
NASHYD (1400)
ID= 1 DT=10.0 min
    
```

```

Area (ha)= 117.70 Curve Number (CN)= 74.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.97
    
```

Unit Hyd Qpeak (cms)= 4.635

```

PEAK FLOW (cms)= 5.203 (i)
TIME TO PEAK (hrs)= 4.167
RUNOFF VOLUME (mm)= 41.315
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.460
    
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

ROUTE CHN (****)
IN= 2---> OUT= 1
    
```

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	259.27	0.0700	
224.90	256.32	0.0500 /0.0700	Main Channel
234.22	255.44	0.0700	
241.28	255.24	0.0700	
245.63	256.44	0.0700	
278.81	257.64	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	255.34	.130E+03	0.0	0.25	44.25
0.20	255.44	.521E+03	0.3	0.40	27.88
0.33	255.57	.127E+04	1.3	0.66	16.80
0.46	255.70	.219E+04	2.8	0.87	12.86
0.59	255.83	.326E+04	5.1	1.04	10.70
0.72	255.96	.449E+04	8.0	1.20	9.30
0.85	256.09	.588E+04	11.8	1.34	8.30
0.98	256.22	.743E+04	16.4	1.48	7.53
1.11	256.35	.915E+04	22.1	1.61	6.90
1.24	256.48	.115E+05	28.7	1.66	6.71
1.36	256.60	.150E+05	35.7	1.59	7.02

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1.49	256.73	.197E+05	45.9	1.56	7.14
1.62	256.86	.255E+05	59.7	1.57	7.11
1.75	256.99	.325E+05	77.4	1.59	6.99
1.88	257.12	.406E+05	99.3	1.64	6.82
2.01	257.25	.499E+05	125.8	1.69	6.61
2.14	257.38	.604E+05	157.3	1.74	6.40
2.27	257.51	.720E+05	194.1	1.80	6.18
2.40	257.64	.848E+05	236.6	1.87	5.97

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel-->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (1400)	117.70	5.20	4.17	41.32	0.59	1.05
OUTFLOW:	ID= 1 (****)	117.70	5.17	4.33	41.31	0.59	1.05

```

CALIB
NASHYD (1500)
ID= 1 DT=10.0 min
    
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```

Area (ha)= 37.27      Curve Number (CN)= 74.0
Ia (mm)= 5.00        # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.72
    
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```

Unit Hyd Qpeak (cms)= 1.977

PEAK FLOW (cms)= 2.012 (i)
TIME TO PEAK (hrs)= 3.833
RUNOFF VOLUME (mm)= 41.310
TOTAL RAINFALL (mm)= 89.800
RUNOFF COEFFICIENT = 0.460
    
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

ADD HYD (0121)
1 + 2 = 3
    
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2706.37	19.793	7.17	32.38
+ ID2= 2 (****):	117.70	5.173	4.33	41.31
=====				
ID = 3 (0121):	2824.07	20.979	6.92	32.75

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

ADD HYD (0121)
3 + 2 = 1
    
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0121):	2824.07	20.979	6.92	32.75
+ ID2= 2 (1500):	37.27	2.012	3.83	41.31
=====				
ID = 1 (0121):	2861.34	21.227	6.75	32.87

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

ROUTE CHN (****)
IN= 2----> OUT= 1
    
```

Routing time step (min)'= 10.00
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----->

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	253.10	0.0700	
17.00	252.40	0.0500	Main Channel
29.00	251.60	0.0500	Main Channel
31.00	250.80	0.0500	Main Channel
35.00	251.00	0.0500	Main Channel
39.50	250.90	0.0500 / 0.0700	Main Channel
44.00	251.50	0.0700	
56.00	252.50	0.0700	
61.00	253.20	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	250.90	.294E+02	0.0	0.36	12.18
0.22	251.02	.226E+03	0.4	0.52	8.41
0.33	251.13	.543E+03	1.8	0.86	5.05
0.45	251.25	.895E+03	3.8	1.12	3.88
0.56	251.36	.128E+04	6.6	1.34	3.25
0.68	251.48	.170E+04	9.9	1.52	2.86
0.79	251.59	.217E+04	13.9	1.68	2.59
0.91	251.71	.270E+04	17.6	1.70	2.55
1.03	251.83	.333E+04	22.2	1.75	2.49
1.14	251.94	.405E+04	27.9	1.80	2.42
1.26	252.06	.486E+04	34.7	1.86	2.33
1.37	252.17	.577E+04	42.8	1.93	2.25
1.49	252.29	.678E+04	52.2	2.01	2.17
1.61	252.41	.788E+04	63.0	2.09	2.08
1.72	252.52	.909E+04	77.8	2.23	1.95
1.84	252.64	.104E+05	94.4	2.37	1.84
1.95	252.75	.119E+05	112.7	2.48	1.75
2.07	252.87	.134E+05	132.8	2.59	1.68
2.18	252.98	.151E+05	154.7	2.68	1.62

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0121)	2861.34	21.23	6.75	32.87	1.00	1.74
OUTFLOW: ID= 1 (****)	2861.34	21.23	6.75	32.87	1.00	1.74

CALIB			
NASHYD (1600)	Area (ha)=	8.90	Curve Number (CN)= 74.0
ID= 1 DT=10.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.78	

Unit Hyd Qpeak (cms)= 0.436

PEAK FLOW (cms)= 0.455 (i)

TIME TO PEAK (hrs)= 4.000

RUNOFF VOLUME (mm)= 41.312

TOTAL RAINFALL (mm)= 89.800

RUNOFF COEFFICIENT = 0.460

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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ADD HYD (0110)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2861.34	21.226	6.75	32.87
+ ID2= 2 (1600):	8.90	0.455	4.00	41.31
=====				
ID = 3 (0110):	2870.24	21.298	6.75	32.89

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
10.00	249.90	0.1000	
86.00	248.10	0.1000 /0.0350	Main channel
88.00	246.81	0.0350	Main channel
107.00	247.20	0.0350	Main channel
112.00	248.90	0.0350 /0.0600	Main channel
132.00	247.90	0.0600	
164.00	249.40	0.0600	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.13	246.94	.133E+03	0.2	0.36	14.71
0.26	247.07	.532E+03	1.0	0.57	9.26
0.39	247.20	.120E+04	2.8	0.75	7.07
0.52	247.33	.201E+04	6.5	1.03	5.13
0.64	247.45	.285E+04	11.4	1.28	4.15
0.77	247.58	.371E+04	17.4	1.49	3.55
0.90	247.71	.460E+04	24.4	1.69	3.14
1.03	247.84	.551E+04	32.4	1.87	2.84
1.16	247.97	.648E+04	41.3	2.03	2.61
1.29	248.10	.767E+04	51.3	2.13	2.49
1.43	248.24	.942E+04	64.6	2.18	2.43
1.58	248.39	.117E+05	80.0	2.17	2.45
1.72	248.53	.146E+05	97.9	2.13	2.49
1.87	248.68	.181E+05	118.6	2.08	2.55
2.01	248.82	.222E+05	142.4	2.04	2.59
2.16	248.97	.268E+05	170.6	2.03	2.62
2.30	249.11	.318E+05	203.6	2.03	2.61
2.45	249.26	.373E+05	240.0	2.05	2.59
2.59	249.40	.432E+05	280.2	2.06	2.57

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0110)	2870.24	21.30	6.75	32.89	0.85	1.59
OUTFLOW: ID= 1 (****)	2870.24	21.30	6.83	32.89	0.84	1.59

CALIB
NASHYD (1700)
ID= 1 DT=10.0 min

Area (ha)= 21.80 Curve Number (CN)= 74.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.82

Unit Hyd Qpeak (cms)= 1.015

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PEAK FLOW (cms)= 1.081 (i)
 TIME TO PEAK (hrs)= 4.000
 RUNOFF VOLUME (mm)= 41.313
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.460

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0123)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (****):	2870.24	21.297	6.83	32.89
+ ID2= 2 (1700):	21.80	1.081	4.00	41.31
<hr/>				
ID = 3 (0123):	2892.04	21.478	6.75	32.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
 IN= 2----> OUT= 1 Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	251.28	0.0450	
32.00	250.70	0.0450	
84.00	249.60	0.0450	
91.00	249.10	0.0450 /0.0320	Main Channel
96.00	248.60	0.0320	Main Channel
100.00	248.90	0.0320 /0.0450	Main Channel
112.00	250.45	0.0450	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.07	248.68	.889E+01	0.0	0.28	8.17
0.15	248.75	.356E+02	0.1	0.44	5.14
0.22	248.82	.800E+02	0.3	0.58	3.93
0.30	248.90	.142E+03	0.7	0.70	3.24
0.40	249.00	.253E+03	1.7	0.90	2.50
0.51	249.11	.390E+03	3.1	1.07	2.12
0.61	249.21	.555E+03	5.1	1.25	1.81
0.71	249.31	.752E+03	7.7	1.39	1.63
0.82	249.42	.980E+03	10.9	1.50	1.50
0.92	249.52	.124E+04	14.6	1.60	1.41
1.02	249.62	.153E+04	19.0	1.68	1.35
1.13	249.73	.189E+04	23.9	1.72	1.32
1.23	249.83	.233E+04	29.9	1.74	1.30
1.33	249.93	.284E+04	37.0	1.76	1.28
1.44	250.04	.344E+04	45.3	1.79	1.26
1.54	250.14	.412E+04	55.0	1.81	1.25
1.64	250.24	.487E+04	66.1	1.84	1.23
1.75	250.35	.571E+04	78.7	1.87	1.21
1.85	250.45	.662E+04	93.0	1.90	1.19

	<---- hydrograph ---->	<-pipe / channel->
AREA (ha)	QPEAK (cms) TPEAK (hrs) R.V. (mm)	MAX DEPTH (m) MAX VEL (m/s)

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INFLOW : ID= 2 (0123) 2892.04 21.48 6.75 32.95 1.08 1.70
 OUTFLOW: ID= 1 (****) 2892.04 21.48 6.83 32.95 1.07 1.70

CALIB
 NASHYD (1800)
 ID= 1 DT=10.0 min

Area (ha)= 3.82 Curve Number (CN)= 78.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.10

Unit Hyd Qpeak (cms)= 1.459
 PEAK FLOW (cms)= 0.431 (i)
 TIME TO PEAK (hrs)= 3.167
 RUNOFF VOLUME (mm)= 35.071
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.391

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0130)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2892.04	21.477	6.83	32.95
+ ID2= 2 (1800):	3.82	0.431	3.17	35.07
<hr/>				
ID = 3 (0130):	2895.86	21.477	6.83	32.96

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0124)
 IN= 2---> OUT= 1

Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	251.01	0.0700	
76.16	250.14	0.0500	Main Channel
84.69	248.40	0.0500 /0.0700	Main Channel
92.28	246.41	0.0700	
100.53	248.07	0.0700	
119.66	248.85	0.0700	
150.39	250.47	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.20	246.61	.712E+02	0.0	0.11	62.27
0.40	246.81	.285E+03	0.1	0.17	39.23
0.60	247.01	.641E+03	0.4	0.23	29.94
0.80	247.21	.114E+04	0.8	0.28	24.71
1.00	247.41	.178E+04	1.4	0.32	21.30
1.19	247.60	.256E+04	2.3	0.36	18.86
1.39	247.80	.349E+04	3.4	0.40	17.02
1.59	248.00	.456E+04	4.9	0.44	15.57
1.79	248.20	.584E+04	6.2	0.43	15.75
1.99	248.40	.756E+04	8.0	0.43	15.82
2.22	248.63	.101E+05	11.2	0.45	15.05

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2.45	248.86	.133E+05	15.7	0.48	14.19
2.68	249.09	.171E+05	21.8	0.52	13.12
2.91	249.32	.214E+05	29.2	0.56	12.21
3.14	249.55	.262E+05	38.2	0.60	11.44
3.37	249.78	.316E+05	48.9	0.63	10.76
3.60	250.01	.374E+05	61.3	0.67	10.18
3.83	250.24	.439E+05	75.8	0.71	9.67
4.06	250.47	.525E+05	93.1	0.73	9.40

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0130)	2895.86	21.48	6.83	32.96	2.67	0.52
OUTFLOW:	ID= 1 (0124)	2895.86	21.32	6.92	32.96	2.66	0.52

CALIB					
NASHYD	(1900)	Area	(ha)= 10.25	Curve Number	(CN)= 80.0
ID= 1 DT=10.0 min		Ia	(mm)= 5.00	# of Linear Res.(N)=	3.00
		U.H. Tp	(hrs)= 0.33		

Unit Hyd Qpeak (cms)= 1.186

PEAK FLOW (cms)= 1.019 (i)
 TIME TO PEAK (hrs)= 3.333
 RUNOFF VOLUME (mm)= 48.296
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.538

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD	(0150)				
1 + 2 =	3	AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0124):		2895.86	21.321	6.92	32.96
+ ID2= 2 (1900):		10.25	1.019	3.33	48.30
ID = 3 (0150):		2906.11	21.332	6.92	33.01

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB					
NASHYD	(2000)	Area	(ha)= 125.00	Curve Number	(CN)= 67.0
ID= 1 DT=10.0 min		Ia	(mm)= 5.00	# of Linear Res.(N)=	3.00
		U.H. Tp	(hrs)= 1.50		

Unit Hyd Qpeak (cms)= 3.183

PEAK FLOW (cms)= 3.308 (i)
 TIME TO PEAK (hrs)= 4.833
 RUNOFF VOLUME (mm)= 34.258
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.381

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100YearSCS6hour Results.txt

ROUTE CHN (****) |
 | IN= 2---> OUT= 1 | Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	256.00	0.0700	
41.00	250.00	0.0500	Main Channel
126.00	249.50	0.0500 / 0.0700	Main Channel
131.00	249.00	0.0700	
136.00	249.50	0.0700	
217.00	250.00	0.0700	
283.00	251.30	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	249.10	.666E+02	0.0	0.14	77.86
0.20	249.20	.267E+03	0.1	0.23	49.05
0.30	249.30	.600E+03	0.3	0.30	37.43
0.40	249.40	.107E+04	0.6	0.36	30.90
0.50	249.50	.167E+04	1.0	0.42	26.63
0.63	249.63	.435E+04	2.0	0.30	36.91
0.76	249.76	.107E+05	5.9	0.37	30.24
0.89	249.89	.207E+05	14.0	0.45	24.61
1.01	250.01	.343E+05	27.9	0.54	20.52
1.14	250.14	.498E+05	50.9	0.68	16.32
1.27	250.27	.659E+05	79.4	0.80	13.83
1.40	250.40	.826E+05	113.3	0.91	12.16
1.53	250.53	.100E+06	152.3	1.01	10.95
1.66	250.66	.118E+06	196.3	1.11	10.02
1.79	250.79	.137E+06	245.3	1.20	9.28
1.91	250.91	.156E+06	299.3	1.28	8.68
2.04	251.04	.176E+06	358.1	1.36	8.18
2.17	251.17	.196E+06	421.8	1.43	7.76
2.30	251.30	.218E+06	490.5	1.50	7.39

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (2000)	125.00	3.31	4.83	34.26	0.67	0.32
OUTFLOW: ID= 1 (****)	125.00	3.02	5.50	34.26	0.66	0.32

CALIB
 NASHYD (2100) | Area (ha)= 34.30 | Curve Number (CN)= 80.0
 ID= 1 DT=10.0 min | Ia (mm)= 5.00 | # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.36

Unit Hyd Qpeak (cms)= 3.639
 PEAK FLOW (cms)= 3.253 (i)
 TIME TO PEAK (hrs)= 3.333
 RUNOFF VOLUME (mm)= 48.351
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.538

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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ADD HYD (0160)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (****):		125.00	3.019	5.50	34.26
+ ID2= 2 (0150):		2906.11	21.332	6.92	33.01
ID = 3 (0160):		3031.11	23.685	6.67	33.06

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0160)		AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1		(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0160):		3031.11	23.685	6.67	33.06
+ ID2= 2 (2100):		34.30	3.253	3.33	48.35
ID = 1 (0160):		3065.41	23.796	6.67	33.23

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB		Area	Curve Number
NASHYD (2200)		(ha)=	(CN)=
ID= 1 DT=10.0 min		10.21	78.0
		Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
		U.H. Tp(hrs)= 0.21	

Unit Hyd Qpeak (cms)= 1.857
 PEAK FLOW (cms)= 1.205 (i)
 TIME TO PEAK (hrs)= 3.167
 RUNOFF VOLUME (mm)= 44.965
 TOTAL RAINFALL (mm)= 89.800
 RUNOFF COEFFICIENT = 0.501

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0170)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0160):		3065.41	23.796	6.67	33.23
+ ID2= 2 (2200):		10.21	1.205	3.17	44.96
ID = 3 (0170):		3075.62	23.803	6.67	33.27

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

Timmins Results.txt

```

=====
=====
V   V   I   SSSSS  U   U   A   L
V   V   I   SS     U   U   A A  L
V   V   I   SS     U   U   AAAAA L
V   V   I   SS     U   U   A   A  L
VV    I   SSSSS  UUUUU  A   A  LLLLL

000   TTTT  TTTT  H   H   Y   Y   M   M   000   TM
O   O   T   T   H   H   Y   Y   MM  MM  O   O
O   O   T   T   H   H   Y   M   M   O   O
000   T   T   H   H   Y   M   M   000

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***** D E T A I L E D O U T P U T *****

Input filename: C:\Program Files (x86)\VO Suite 3.0\VO2\voin.dat

Output filename: C:\Users\GAL - Kevin\AppData\Local\Temp\52a2fbb8-fa04-4871-b666-0c0343464070\scenario.out

Summary filename: C:\Users\GAL - Kevin\AppData\Local\Temp\52a2fbb8-fa04-4871-b666-0c0343464070\scenario.sum

DATE: 04/01/2019

TIME: 02:47:54

USER:

COMMENTS: _____

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*****
** SIMULATION NUMBER: 0 **
*****

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| READ STORM | Filename: C:\Users\GAL - Kevin\AppData
|             | ata\Local\Temp\
| Ptotal=193.00 mm | 52a2fbb8-fa04-4871-b666-0c0343464070\6ac174c3
|             | Comments: Timmins Storm event mm/hr
-----

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
0.17	15.00	3.17	3.00	6.17	43.00	9.17	13.00
0.33	15.00	3.33	3.00	6.33	43.00	9.33	13.00
0.50	15.00	3.50	3.00	6.50	43.00	9.50	13.00
0.67	15.00	3.67	3.00	6.67	43.00	9.67	13.00
0.83	15.00	3.83	3.00	6.83	43.00	9.83	13.00
1.00	15.00	4.00	3.00	7.00	43.00	10.00	13.00
1.17	20.00	4.17	5.00	7.17	20.00	10.17	13.00
1.33	20.00	4.33	5.00	7.33	20.00	10.33	13.00

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1.50	20.00	4.50	5.00	7.50	20.00	10.50	13.00
1.67	20.00	4.67	5.00	7.67	20.00	10.67	13.00
1.83	20.00	4.83	5.00	7.83	20.00	10.83	13.00
2.00	20.00	5.00	5.00	8.00	20.00	11.00	13.00
2.17	10.00	5.17	20.00	8.17	23.00	11.17	8.00
2.33	10.00	5.33	20.00	8.33	23.00	11.33	8.00
2.50	10.00	5.50	20.00	8.50	23.00	11.50	8.00
2.67	10.00	5.67	20.00	8.67	23.00	11.67	8.00
2.83	10.00	5.83	20.00	8.83	23.00	11.83	8.00
3.00	10.00	6.00	20.00	9.00	23.00	12.00	8.00

MODIFY STORM
CASE= 1

MODIFYING PARAMETERS
Multiplication Factor= 0.97
Time shift (min) = 0.00

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
0.167	14.55	3.167	2.91	6.167	41.71	9.17	12.61
0.333	14.55	3.333	2.91	6.333	41.71	9.33	12.61
0.500	14.55	3.500	2.91	6.500	41.71	9.50	12.61
0.667	14.55	3.667	2.91	6.667	41.71	9.67	12.61
0.833	14.55	3.833	2.91	6.833	41.71	9.83	12.61
1.000	14.55	4.000	2.91	7.000	41.71	10.00	12.61
1.167	19.40	4.167	4.85	7.167	19.40	10.17	12.61
1.333	19.40	4.333	4.85	7.333	19.40	10.33	12.61
1.500	19.40	4.500	4.85	7.500	19.40	10.50	12.61
1.667	19.40	4.667	4.85	7.667	19.40	10.67	12.61
1.833	19.40	4.833	4.85	7.833	19.40	10.83	12.61
2.000	19.40	5.000	4.85	8.000	19.40	11.00	12.61
2.167	9.70	5.167	19.40	8.167	22.31	11.17	7.76
2.333	9.70	5.333	19.40	8.333	22.31	11.33	7.76
2.500	9.70	5.500	19.40	8.500	22.31	11.50	7.76
2.667	9.70	5.667	19.40	8.667	22.31	11.67	7.76
2.833	9.70	5.833	19.40	8.833	22.31	11.83	7.76
3.000	9.70	6.000	19.40	9.000	22.31	12.00	7.76

CALIB
NASHYD (0100)
ID= 1 DT=10.0 min

Area (ha)= 197.60
Ia (mm)= 5.00
U.H. Tp(hrs)= 2.63
Curve Number (CN)= 67.0
of Linear Res.(N)= 3.00

Unit Hyd Qpeak (cms)= 2.870
PEAK FLOW (cms)= 7.420 (i)
TIME TO PEAK (hrs)= 10.667
RUNOFF VOLUME (mm)= 108.034
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.577

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->
Distance Elevation Manning

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0.00	277.27	0.1000	
332.34	275.59	0.1000 /0.0500	Main Channel
352.82	273.81	0.0500	Main Channel
365.19	273.82	0.0500	Main Channel
387.54	274.15	0.0500	Main Channel
399.23	275.75	0.0500 /0.1000	Main Channel
500.73	277.20	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.18	273.99	.351E+04	0.8	0.24	73.47
0.36	274.17	.976E+04	3.3	0.37	48.89
0.53	274.34	.175E+05	8.3	0.51	35.01
0.71	274.52	.259E+05	15.2	0.63	28.39
0.89	274.70	.349E+05	23.9	0.73	24.39
1.07	274.88	.446E+05	34.3	0.82	21.66
1.25	275.06	.548E+05	46.5	0.91	19.66
1.42	275.23	.658E+05	60.5	0.99	18.11
1.60	275.41	.774E+05	76.4	1.06	16.86
1.78	275.59	.896E+05	94.2	1.13	15.84
1.96	275.77	.106E+06	116.5	1.18	15.12
2.14	275.95	.130E+06	143.5	1.18	15.11
2.32	276.13	.164E+06	175.1	1.15	15.58
2.50	276.31	.207E+06	212.2	1.10	16.22
2.67	276.48	.258E+06	255.6	1.06	16.86
2.85	276.66	.320E+06	305.9	1.02	17.42
3.03	276.84	.390E+06	363.8	1.00	17.87
3.21	277.02	.469E+06	429.9	0.98	18.20
3.39	277.20	.558E+06	504.8	0.97	18.43

	AREA (ha)	<---- hydrograph ---->			<-pipe / channel-->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0100)	197.60	7.42	10.67	108.03	0.50	0.48
OUTFLOW: ID= 1 (****)	197.60	7.36	11.17	108.03	0.50	0.47

CALIB			
NASHYD (0200)	Area (ha)= 107.20	Curve Number (CN)= 68.0	
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00	
	U.H. Tp(hrs)= 0.87		

Unit Hyd Qpeak (cms)= 4.706

PEAK FLOW (cms)= 5.975 (i)

TIME TO PEAK (hrs)= 7.500

RUNOFF VOLUME (mm)= 110.020

TOTAL RAINFALL (mm)= 187.210

RUNOFF COEFFICIENT = 0.588

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)	
IN= 2---> OUT= 1	Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning
0.00	279.83	0.1000

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204.39	277.60	0.0500	Main Channel
296.57	273.96	0.0500	Main Channel
461.97	273.75	0.0500	Main Channel
485.91	272.71	0.0500 /0.1000	Main Channel
798.40	272.85	0.1000	
877.72	273.64	0.1000	
1006.81	276.74	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.21	272.92	.916E+05	3.6	0.08	429.52
0.42	273.13	.237E+06	16.5	0.14	238.88
0.64	273.35	.393E+06	36.9	0.19	177.74
0.85	273.56	.561E+06	64.0	0.23	145.94
1.06	273.77	.739E+06	97.5	0.27	126.27
1.27	273.98	.964E+06	140.8	0.30	114.14
1.48	274.19	.122E+07	202.9	0.34	100.49
1.70	274.41	.149E+07	277.8	0.38	89.31
1.91	274.62	.176E+07	364.6	0.42	80.46
2.12	274.83	.204E+07	462.6	0.46	73.42
2.33	275.04	.232E+07	571.4	0.50	67.71
2.55	275.26	.261E+07	690.7	0.54	63.00
2.76	275.47	.291E+07	820.5	0.57	59.05
2.97	275.68	.321E+07	960.4	0.61	55.69
3.18	275.89	.352E+07	1110.4	0.64	52.79
3.39	276.10	.383E+07	1270.5	0.67	50.26
3.61	276.32	.415E+07	1440.5	0.70	48.03
3.82	276.53	.448E+07	1620.5	0.73	46.05
4.03	276.74	.481E+07	1810.4	0.76	44.28

	<---- hydrograph ---->	<-pipe / channel-->
	AREA (ha)	QPEAK TPEAK R.V. (cms) (hrs) (mm)
INFLOW : ID= 2 (0200)	107.20	5.97 7.50 110.02
OUTFLOW: ID= 1 (****)	107.20	2.53 11.83 110.00
		MAX DEPTH MAX VEL (m) (m/s)
		0.25 0.09
		0.15 0.08

ADD HYD (0020)	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
1 + 2 = 3				
ID1= 1 (****):	197.60	7.356	11.17	108.03
+ ID2= 2 (****):	107.20	2.533	11.83	110.00
=====				
ID = 3 (0020):	304.80	9.864	11.33	108.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)	ROUTING TIME STEP (min)
IN= 2---> OUT= 1	10.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
0.00	273.19	0.1000	
89.61	271.91	0.1000 /0.0500	Main channel
138.71	271.70	0.0500	Main channel
184.80	271.75	0.0500 /0.1000	Main channel
266.32	271.80	0.1000	

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 367.88 271.93 0.1000
 520.40 272.09 0.1000

----- TRAVEL TIME TABLE -----					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.02	271.72	.159E+03	0.0	0.01	*****
0.03	271.73	.634E+03	0.0	0.02	694.13
0.05	271.75	.143E+04	0.0	0.03	529.62
0.07	271.77	.306E+04	0.1	0.04	405.42
0.09	271.79	.551E+04	0.3	0.04	365.74
0.11	271.81	.873E+04	0.4	0.05	336.92
0.13	271.83	.124E+05	0.7	0.05	310.09
0.16	271.86	.166E+05	1.0	0.06	288.06
0.18	271.88	.211E+05	1.3	0.06	269.92
0.20	271.90	.262E+05	1.7	0.06	254.75
0.22	271.92	.317E+05	2.2	0.07	239.31
0.24	271.94	.376E+05	2.8	0.07	224.81
0.26	271.96	.439E+05	3.4	0.08	213.43
0.28	271.98	.507E+05	4.1	0.08	203.95
0.30	272.00	.579E+05	4.9	0.08	195.88
0.33	272.03	.656E+05	5.8	0.09	188.88
0.35	272.05	.738E+05	6.7	0.09	182.73
0.37	272.07	.824E+05	7.7	0.09	177.27
0.39	272.09	.915E+05	8.8	0.10	172.36

**** WARNING: TRAVEL TIME TABLE EXCEEDED

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0020)	304.80	9.86	11.33	108.72	0.39	0.10
OUTFLOW: ID= 1 (****)	304.80	7.98	12.83	108.70	0.37	0.09

CALIB	Area (ha)= 228.10	Curve Number (CN)= 67.0
NASHYD (0400)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT=10.0 min	U.H. Tp(hrs)= 1.65	

Unit Hyd Qpeak (cms)= 5.280

PEAK FLOW (cms)= 10.190 (i)
 TIME TO PEAK (hrs)= 9.333
 RUNOFF VOLUME (mm)= 108.033
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.577

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1 Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->		
Distance	Elevation	Manning
0.00	276.00	0.1000
91.20	274.69	0.1000
174.02	274.10	0.1000
210.03	273.92	0.1000
333.58	273.80	0.1000 /0.0500 Main channel

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368.08	273.64	0.0500	Main Channel
385.33	273.85	0.0500 / 0.1000	Main Channel
462.42	275.22	0.1000	
531.42	275.33	0.1000	

----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.08	273.72	.220E+03	0.1	0.07	54.86
0.16	273.80	.880E+03	0.4	0.11	34.56
0.25	273.89	.291E+04	1.6	0.13	29.37
0.34	273.98	.663E+04	4.2	0.15	26.31
0.43	274.07	.109E+05	8.0	0.17	22.70
0.52	274.16	.157E+05	13.0	0.19	20.01
0.61	274.25	.208E+05	19.2	0.21	18.01
0.70	274.34	.263E+05	26.5	0.23	16.50
0.79	274.43	.321E+05	34.9	0.25	15.32
0.88	274.52	.383E+05	44.5	0.27	14.36
0.97	274.61	.449E+05	55.2	0.28	13.57
1.06	274.70	.519E+05	67.1	0.30	12.88
1.15	274.79	.591E+05	80.7	0.32	12.21
1.24	274.88	.666E+05	95.5	0.33	11.62
1.33	274.97	.743E+05	111.4	0.35	11.11
1.42	275.06	.822E+05	128.5	0.36	10.66
1.51	275.15	.904E+05	146.8	0.38	10.26
1.60	275.24	.989E+05	165.2	0.39	9.97
1.69	275.33	.108E+06	183.2	0.39	9.85

	<---- hydrograph ---->	<-pipe / channel->
	AREA	QPEAK
	(ha)	(cms)
	TPEAK	R.V.
	(hrs)	(mm)
INFLOW : ID= 2 (0400)	228.10	10.19
OUTFLOW: ID= 1 (****)	228.10	10.07
	MAX DEPTH	MAX VEL
	(m)	(m/s)
	0.47	0.18
	0.47	0.18

CALIB	Area (ha)= 302.30	Curve Number (CN)= 67.0
NASHYD (0500)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT=10.0 min	U.H. Tp(hrs)= 1.31	

Unit Hyd Qpeak (cms)= 8.814

PEAK FLOW (cms)= 14.214 (i)

TIME TO PEAK (hrs)= 9.000

RUNOFF VOLUME (mm)= 108.032

TOTAL RAINFALL (mm)= 187.210

RUNOFF COEFFICIENT = 0.577

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

CALIB	Area (ha)= 308.80	Curve Number (CN)= 64.0
NASHYD (2300)	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
ID= 1 DT=10.0 min	U.H. Tp(hrs)= 1.85	

Unit Hyd Qpeak (cms)= 6.375

PEAK FLOW (cms)= 12.611 (i)

TIME TO PEAK (hrs)= 9.667

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RUNOFF VOLUME (mm)= 102.128
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.546

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****) |
 IN= 2---> OUT= 1 | Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	274.69	0.1000	
82.82	274.10	0.1000	
118.83	273.92	0.1000	
242.38	273.80	0.1000 /0.0500	Main Channel
276.88	273.64	0.0500	Main Channel
294.13	273.85	0.0500 /0.1000	Main Channel
371.22	275.22	0.1000	
440.22	275.33	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.05	273.69	.907E+03	0.0	0.05	711.92
0.11	273.75	.363E+04	0.1	0.08	448.48
0.16	273.80	.816E+04	0.4	0.10	342.25
0.22	273.86	.175E+05	1.0	0.12	298.74
0.27	273.91	.342E+05	2.0	0.12	287.79
0.33	273.97	.560E+05	3.5	0.13	266.60
0.38	274.02	.797E+05	5.5	0.15	242.26
0.44	274.08	.105E+06	7.9	0.16	222.10
0.49	274.13	.132E+06	10.7	0.17	205.22
0.55	274.19	.160E+06	14.0	0.19	191.05
0.60	274.24	.190E+06	17.7	0.20	179.33
0.66	274.30	.221E+06	21.7	0.21	169.47
0.72	274.36	.253E+06	26.2	0.22	161.07
0.77	274.41	.287E+06	31.1	0.23	153.82
0.83	274.47	.321E+06	36.3	0.24	147.48
0.88	274.52	.358E+06	42.0	0.25	141.88
0.94	274.58	.395E+06	48.1	0.26	136.90
0.99	274.63	.434E+06	54.6	0.27	132.43
1.05	274.69	.474E+06	61.5	0.28	128.38

<---- hydrograph ----> <-pipe / channel->

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (2300)	308.80	12.61	9.67	102.13	0.53	0.18
OUTFLOW: ID= 1 (****)	308.80	8.94	12.00	102.11	0.46	0.17

ADD HYD (0010)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	308.80	8.937	12.00	102.11
+ ID2= 2 (****):	228.10	10.073	9.67	108.03
===== ID = 3 (0010):	536.90	17.699	10.50	104.63

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

| ADD HYD (0010) |
| 3 + 2 = 1 |
    
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0010):	536.90	17.699	10.50	104.63
+ ID2= 2 (0500):	302.30	14.214	9.00	108.03
<hr/>				
ID = 1 (0010):	839.20	30.625	9.67	105.85

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

| ROUTE CHN (****) |
| IN= 2---> OUT= 1 |
    
```

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	272.10	0.1000	
34.80	271.88	0.0500	Main Channel
68.44	271.83	0.0500	Main Channel
76.43	271.69	0.0500	Main Channel
82.05	271.69	0.0500	Main Channel
110.40	271.81	0.0500 / 0.1000	Main Channel
127.77	271.89	0.1000	
150.00	272.05	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.02	271.71	.635E+02	0.0	0.05	165.35
0.03	271.72	.166E+03	0.0	0.07	112.65
0.05	271.74	.308E+03	0.1	0.08	89.85
0.07	271.76	.490E+03	0.1	0.10	76.31
0.09	271.78	.710E+03	0.2	0.11	67.08
0.10	271.79	.970E+03	0.3	0.13	60.27
0.12	271.81	.127E+04	0.4	0.14	55.00
0.14	271.83	.161E+04	0.6	0.16	48.44
0.16	271.85	.209E+04	0.7	0.15	49.64
0.18	271.87	.273E+04	0.9	0.15	50.05
0.20	271.89	.353E+04	1.2	0.16	47.38
0.22	271.91	.441E+04	1.7	0.18	42.48
0.24	271.93	.534E+04	2.3	0.20	38.91
0.26	271.95	.633E+04	2.9	0.21	36.19
0.28	271.97	.737E+04	3.6	0.22	34.02
0.30	271.99	.847E+04	4.4	0.24	32.26
0.32	272.01	.962E+04	5.2	0.25	30.78
0.34	272.03	.108E+05	6.1	0.26	29.53
0.36	272.05	.121E+05	7.1	0.27	28.45

**** WARNING: TRAVEL TIME TABLE EXCEEDED

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0010)	839.20	30.63	9.67	105.85	0.36	0.27
OUTFLOW: ID= 1 (****)	839.20	30.10	10.17	105.85	0.36	0.27

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ADD HYD (0030)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (****):		304.80	7.983	12.83	108.70
+ ID2= 2 (****):		839.20	30.097	10.17	105.85
=====					
ID = 3 (0030):		1144.00	35.796	10.67	106.61

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1 Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	273.19	0.1000	
89.61	271.91	0.1000 /0.0500	Main Channel
138.71	271.70	0.0500	Main Channel
184.80	271.75	0.0500 /0.1000	Main Channel
266.32	271.80	0.1000	
367.88	271.93	0.1000	
520.40	272.09	0.1000	
714.30	273.40	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.05	271.75	.365E+03	0.0	0.03	147.14
0.13	271.83	.275E+04	0.5	0.05	89.17
0.20	271.90	.688E+04	1.6	0.06	70.23
0.28	271.98	.124E+05	3.6	0.07	57.38
0.35	272.05	.195E+05	6.4	0.08	50.32
0.43	272.13	.278E+05	10.4	0.09	44.57
0.50	272.20	.366E+05	15.5	0.11	39.50
0.58	272.28	.457E+05	21.4	0.12	35.69
0.66	272.36	.552E+05	28.1	0.13	32.73
0.73	272.43	.649E+05	35.6	0.14	30.37
0.81	272.51	.750E+05	44.0	0.15	28.43
0.88	272.58	.854E+05	53.1	0.16	26.81
0.96	272.66	.961E+05	63.0	0.17	25.43
1.04	272.74	.107E+06	73.7	0.17	24.24
1.11	272.81	.118E+06	85.1	0.18	23.21
1.19	272.89	.130E+06	97.3	0.19	22.29
1.26	272.96	.142E+06	110.3	0.20	21.48
1.34	273.04	.154E+06	124.0	0.20	20.75
1.41	273.11	.167E+06	138.6	0.21	20.09

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0030)	1144.00	35.80	10.67	106.61	0.73	0.14
OUTFLOW: ID= 1 (****)	1144.00	34.96	11.00	106.61	0.72	0.14

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

CALIB (0300) Area (ha)= 315.50 Curve Number (CN)= 54.0

Timmins Results.txt

|ID= 1 DT=10.0 min | Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 2.03

Unit Hyd Qpeak (cms)= 5.936
 PEAK FLOW (cms)= 10.217 (i)
 TIME TO PEAK (hrs)= 10.000
 RUNOFF VOLUME (mm)= 83.297
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.445

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0125) |
 | 1 + 2 = 3 |

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	1144.00	34.960	11.00	106.61
+ ID2= 2 (0300):	315.50	10.217	10.00	83.30
===== ID = 3 (0125):	1459.50	44.736	11.00	101.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ROUTE CHN (****) |
 | IN= 2---> OUT= 1 |

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
133.75	272.89	0.1000	
157.66	271.71	0.0500 /0.1000	Main Channel
506.36	271.74	0.1000	
524.97	272.90	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.06	271.77	.787E+04	0.6	0.04	211.05
0.12	271.83	.183E+05	2.5	0.07	120.74
0.19	271.90	.288E+05	5.4	0.09	89.62
0.25	271.96	.394E+05	9.0	0.11	73.08
0.31	272.02	.500E+05	13.3	0.13	62.58
0.37	272.08	.607E+05	18.3	0.14	55.23
0.43	272.14	.715E+05	23.9	0.16	49.74
0.50	272.21	.823E+05	30.2	0.18	45.47
0.56	272.27	.932E+05	37.0	0.19	42.03
0.62	272.33	.104E+06	44.3	0.20	39.19
0.68	272.39	.115E+06	52.2	0.22	36.80
0.75	272.46	.126E+06	60.6	0.23	34.76
0.81	272.52	.137E+06	69.5	0.24	32.98
0.87	272.58	.149E+06	78.8	0.25	31.43
0.93	272.64	.160E+06	88.7	0.26	30.06
0.99	272.70	.171E+06	99.1	0.28	28.83
1.06	272.77	.183E+06	109.9	0.29	27.73
1.12	272.83	.194E+06	121.1	0.30	26.73
1.18	272.89	.206E+06	132.8	0.31	25.83

AREA <---- hydrograph ----> <-pipe / channel->
 QPEAK TPEAK R.V. MAX DEPTH MAX VEL

Timmins Results.txt

		(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0125)	1459.50	44.74	11.00	101.57	0.62	0.20
OUTFLOW:	ID= 1 (****)	1459.50	43.03	11.17	101.57	0.61	0.20

**** WARNING: COMPUTATIONS FAILED TO CONVERGE.

CALIB		Area	(ha)= 299.60	Curve Number	(CN)= 63.0
NASHYD	(0600)	Ia	(mm)= 5.00	# of Linear Res.(N)=	3.00
ID= 1	DT=10.0 min	U.H. Tp(hrs)=	1.85		

Unit Hyd Qpeak (cms)= 6.186

PEAK FLOW (cms)= 12.010 (i)
 TIME TO PEAK (hrs)= 9.667
 RUNOFF VOLUME (mm)= 100.187
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.535

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD	(0040)				
1 + 2 =	3	AREA	QPEAK	TPEAK	R.V.
		(ha)	(cms)	(hrs)	(mm)
+ ID1= 1	(****):	1459.50	43.027	11.17	101.57
+ ID2= 2	(0600):	299.60	12.010	9.67	100.19
ID = 3 (0040):		1759.10	53.767	10.92	101.34

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN	(****)	
IN= 2	OUT= 1	Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	280.66	0.1000	
230.75	272.35	0.0500 /0.1000	Main Channel
454.64	271.34	0.1000	
776.25	271.91	0.1000	
796.25	273.69	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
0.12	271.46	.111E+05	0.2	0.03	*****
0.25	271.59	.443E+05	1.1	0.05	681.82
0.37	271.71	.996E+05	3.2	0.06	520.33
0.49	271.83	.177E+06	6.9	0.07	429.52
0.62	271.96	.275E+06	12.8	0.09	359.68
0.74	272.08	.383E+06	21.2	0.10	301.05
0.87	272.21	.498E+06	31.8	0.12	261.00
0.99	272.33	.619E+06	44.5	0.13	231.74
1.11	272.45	.744E+06	60.8	0.15	204.11
1.24	272.58	.871E+06	79.5	0.17	182.72
1.36	272.70	.999E+06	100.2	0.18	166.24

Timmins Results.txt

1.48	272.82	.113E+07	122.8	0.20	153.09
1.61	272.95	.126E+07	147.3	0.22	142.33
1.73	273.07	.139E+07	173.7	0.23	133.33
1.86	273.20	.152E+07	201.8	0.24	125.68
1.98	273.32	.166E+07	231.7	0.26	119.08
2.10	273.44	.179E+07	263.2	0.27	113.32
2.23	273.57	.193E+07	296.4	0.28	108.24
2.35	273.69	.206E+07	331.3	0.30	103.73

		AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0040)	1759.10	53.77	10.92	101.34	1.06	0.14
OUTFLOW:	ID= 1 (****)	1759.10	38.72	12.83	101.32	0.93	0.13

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| CALIB
| NASHYD (0700)
| ID= 1 DT=10.0 min
|
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Area (ha)= 181.20      Curve Number (CN)= 60.0
Ia (mm)= 5.00         # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.89

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Unit Hyd Qpeak (cms)= 3.662

PEAK FLOW (cms)= 6.806 (i)
TIME TO PEAK (hrs)= 9.833
RUNOFF VOLUME (mm)= 94.442
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.504

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(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| CALIB
| NASHYD (1000)
| ID= 1 DT=10.0 min
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Area (ha)= 69.40      Curve Number (CN)= 67.0
Ia (mm)= 5.00         # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.06

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Unit Hyd Qpeak (cms)= 2.501

PEAK FLOW (cms)= 3.495 (i)
TIME TO PEAK (hrs)= 7.833
RUNOFF VOLUME (mm)= 108.030
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.577

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(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
| ADD HYD (0050)
| 1 + 2 = 3
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	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (1000):	69.40	3.495	7.83	108.03
+ ID2= 2 (****):	1759.10	38.721	12.83	101.32
=====	=====	=====	=====	=====
ID = 3 (0050):	1828.50	40.029	12.42	101.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Timmins Results.txt

ADD HYD (0050)
3 + 2 = 1

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0050):	1828.50	40.029	12.42	101.57
+ ID2= 2 (0700):	181.20	6.806	9.83	94.44
=====				
ID = 1 (0050):	2009.70	45.082	12.42	100.93

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
NASHYD (0800)
ID= 1 DT=10.0 min

Area (ha)= 183.20 Curve Number (CN)= 68.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.53

Unit Hyd Qpeak (cms)= 4.573

PEAK FLOW (cms)= 8.497 (i)
TIME TO PEAK (hrs)= 9.333
RUNOFF VOLUME (mm)= 110.029
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.588

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (0009)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
8.00	272.30	0.1000	
35.00	271.80	0.1000 /0.0500	Main Channel
50.00	271.50	0.0500	Main Channel
80.00	271.80	0.0500 /0.1000	Main Channel
142.00	272.20	0.1000	
150.00	272.10	0.1000	
228.00	273.20	0.1000	
288.00	275.23	0.1000	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.04	271.54	.150E+03	0.0	0.06	415.02
0.08	271.58	.599E+03	0.0	0.09	261.44
0.11	271.61	.135E+04	0.1	0.12	199.52
0.15	271.65	.240E+04	0.2	0.14	164.70
0.19	271.69	.374E+04	0.4	0.17	141.93
0.23	271.73	.539E+04	0.7	0.19	125.69
0.26	271.76	.734E+04	1.1	0.21	113.41
0.30	271.80	.958E+04	1.5	0.23	103.74
0.35	271.85	.128E+05	2.4	0.27	88.84
0.39	271.89	.166E+05	3.4	0.29	80.63
0.44	271.94	.210E+05	4.7	0.31	75.41
0.48	271.98	.261E+05	6.1	0.33	71.76
0.53	272.03	.318E+05	7.7	0.34	69.01
0.57	272.07	.380E+05	9.5	0.35	66.83

Timmins Results.txt

0.62	272.12	.450E+05	11.5	0.36	65.24
0.66	272.16	.528E+05	13.7	0.37	64.35
0.71	272.21	.618E+05	16.2	0.37	63.59
0.75	272.25	.713E+05	19.1	0.38	62.29
0.80	272.30	.812E+05	22.2	0.39	60.90

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0800)	183.20	8.50	9.33	110.03	0.55	0.35
OUTFLOW: ID= 1 (0009)	183.20	7.81	10.17	110.02	0.53	0.34

CALIB
NASHYD (0900)
ID= 1 DT=10.0 min

Area (ha)= 236.70 Curve Number (CN)= 64.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 1.97

Unit Hyd Qpeak (cms)= 4.589
PEAK FLOW (cms)= 9.453 (i)
TIME TO PEAK (hrs)= 9.833
RUNOFF VOLUME (mm)= 102.128
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.546

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0070)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0009):	183.20	7.809	10.17	110.02
+ ID2= 2 (0900):	236.70	9.453	9.83	102.13
===== ID = 3 (0070):	419.90	17.231	10.00	105.57

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

Distance	Elevation	Manning	
16.00	272.32	0.1000	
55.00	271.60	0.1000 /0.0500	Main Channel
64.00	270.90	0.0500	Main Channel
129.00	271.30	0.0500 /0.1000	Main Channel
151.00	271.51	0.1000	
193.00	271.75	0.1000	
296.00	272.52	0.1000	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.07	270.97	.364E+03	0.0	0.08	183.39
0.13	271.03	.146E+04	0.2	0.13	115.51

Timmins Results.txt

0.20	271.10	.328E+04	0.6	0.18	88.15
0.27	271.17	.582E+04	1.3	0.21	72.77
0.33	271.23	.910E+04	2.4	0.25	62.71
0.40	271.30	.131E+05	3.9	0.28	55.53
0.48	271.38	.186E+05	6.8	0.34	45.54
0.56	271.46	.247E+05	10.3	0.39	39.89
0.64	271.54	.316E+05	14.5	0.43	36.24
0.71	271.61	.394E+05	19.4	0.46	33.82
0.79	271.69	.485E+05	25.2	0.49	32.05
0.87	271.77	.589E+05	31.9	0.51	30.81
0.95	271.85	.705E+05	39.4	0.52	29.81
1.03	271.93	.831E+05	47.8	0.54	28.98
1.11	272.01	.968E+05	57.1	0.55	28.26
1.18	272.08	.112E+06	67.3	0.56	27.63
1.26	272.16	.127E+06	78.4	0.58	27.07
1.34	272.24	.144E+06	90.6	0.59	26.56
1.42	272.32	.162E+06	103.7	0.60	26.09

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<--- pipe / channel ---> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0070)	419.90	17.23	10.00	105.57	0.68	0.45
OUTFLOW: ID= 1 (****)	419.90	16.88	10.50	105.57	0.67	0.44

ADD HYD (0060)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	419.90	16.880	10.50	105.57
+ ID2= 2 (0050):	2009.70	45.082	12.42	100.93
===== ID = 3 (0060):	2429.60	60.277	11.92	101.73

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2 ---> OUT= 1

Routing time step (min)'= 10.00

Distance	Elevation	Manning	
90.00	276.61	0.1000	
140.00	273.00	0.1000	
152.00	271.10	0.1000 / 0.0500	Main Channel
160.00	271.10	0.0500 / 0.1000	Main Channel
168.00	271.51	0.1000	
230.00	271.51	0.1000	
252.00	274.18	0.1000	
280.00	276.18	0.1000	

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.27	271.37	.253E+04	0.4	0.13	104.52
0.53	271.63	.129E+05	1.8	0.11	120.57
0.80	271.90	.315E+05	5.7	0.15	92.29
1.07	272.17	.510E+05	11.5	0.19	73.61
1.34	272.44	.714E+05	19.1	0.22	62.18
1.60	272.70	.926E+05	28.3	0.25	54.48

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1.87	272.97	.115E+06	39.1	0.28	48.92
2.14	273.24	.138E+06	51.1	0.31	44.89
2.41	273.51	.162E+06	64.8	0.33	41.71
2.67	273.77	.188E+06	80.0	0.35	39.11
2.94	274.04	.215E+06	96.9	0.37	36.95
3.21	274.31	.243E+06	115.0	0.39	35.25
3.48	274.58	.273E+06	134.3	0.41	33.89
3.74	274.84	.305E+06	155.4	0.42	32.68
4.01	275.11	.338E+06	178.3	0.44	31.60
4.28	275.38	.373E+06	203.0	0.45	30.62
4.55	275.65	.409E+06	229.5	0.46	29.72
4.81	275.91	.448E+06	258.1	0.48	28.90
5.08	276.18	.487E+06	288.6	0.49	28.14

		AREA (ha)	<---- hydrograph ---->			<-pipe / channel->	
			QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW :	ID= 2 (0060)	2429.60	60.28	11.92	101.73	2.32	0.32
OUTFLOW:	ID= 1 (****)	2429.60	57.99	12.00	101.73	2.27	0.32

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CALIB
NASHYD (1100)
ID= 1 DT=10.0 min
    
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Area (ha)= 203.07
Ia (mm)= 5.00
U.H. Tp(hrs)= 1.74
Curve Number (CN)= 70.0
# of Linear Res.(N)= 3.00
    
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Unit Hyd Qpeak (cms)= 4.458
PEAK FLOW (cms)= 9.402 (i)
TIME TO PEAK (hrs)= 9.500
RUNOFF VOLUME (mm)= 114.064
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.609
    
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(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

ADD HYD (0080)
1 + 2 = 3
    
```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2429.60	57.990	12.00	101.73
+ ID2= 2 (1100):	203.07	9.402	9.50	114.06
ID = 3 (0080):	2632.67	64.899	12.00	102.68

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

ROUTE CHN (****)
IN= 2---> OUT= 1
    
```

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->				
Distance	Elevation	Manning		
44.00	272.20	0.0700		
75.00	270.40	0.0700		
76.00	268.80	0.0700 /0.0500		Main channel
80.00	268.70	0.0500		Main channel
84.00	268.10	0.0500		Main channel

Timmins Results.txt

88.00	269.90	0.0500 / 0.0700	Main Channel
135.00	271.98	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.17	268.27	.563E+02	0.0	0.34	20.26
0.35	268.45	.225E+03	0.3	0.54	12.76
0.52	268.62	.507E+03	0.9	0.71	9.74
0.70	268.80	.970E+03	1.6	0.68	10.11
0.91	269.01	.183E+04	4.4	1.00	6.87
1.12	269.22	.275E+04	8.4	1.26	5.46
1.34	269.44	.372E+04	13.4	1.49	4.64
1.55	269.65	.475E+04	19.3	1.68	4.10
1.76	269.86	.582E+04	26.2	1.86	3.71
1.97	270.07	.708E+04	34.7	2.03	3.40
2.18	270.28	.876E+04	44.9	2.12	3.25
2.40	270.50	.109E+05	56.8	2.16	3.20
2.61	270.71	.137E+05	71.3	2.15	3.21
2.82	270.92	.173E+05	88.8	2.12	3.25
3.03	271.13	.216E+05	109.9	2.10	3.28
3.24	271.34	.267E+05	135.0	2.09	3.30
3.46	271.56	.325E+05	164.4	2.09	3.29
3.67	271.77	.390E+05	198.6	2.11	3.27
3.88	271.98	.463E+05	238.0	2.13	3.24

	<---- hydrograph ---->	<-pipe / channel->
	AREA (ha)	QPEAK (cms) TPEAK (hrs) R.V. (mm)
INFLOW : ID= 2 (0080)	2632.67	64.90 12.00 102.68
OUTFLOW: ID= 1 (****)	2632.67	64.73 12.00 102.68
		MAX DEPTH MAX VEL (m) (m/s)
		2.51 2.15
		2.51 2.15

CALIB			
NASHYD (1200)	Area (ha)=	30.80	Curve Number (CN)= 78.0
ID= 1 DT=10.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.85	

Unit Hyd Qpeak (cms)= 1.384

PEAK FLOW (cms)= 2.084 (i)

TIME TO PEAK (hrs)= 7.500

RUNOFF VOLUME (mm)= 130.774

TOTAL RAINFALL (mm)= 187.210

RUNOFF COEFFICIENT = 0.699

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0090)				
1 + 2 = 3	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
	ID1= 1 (****):	2632.67	64.733	12.00
	+ ID2= 2 (1200):	30.80	2.084	7.50
	=====	=====	=====	=====
	ID = 3 (0090):	2663.47	65.557	12.00
				103.01

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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ROUTE CHN (****)
IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
18.00	268.20	0.0700	
29.00	266.80	0.0700	
50.50	266.10	0.0700	
57.00	264.70	0.0700 /0.0500	Main channel
60.50	264.60	0.0500	Main Channel
66.00	264.72	0.0500 /0.0700	Main Channel
77.80	267.30	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	264.70	.416E+03	0.1	0.28	61.42
0.24	264.84	.175E+04	1.1	0.64	26.84
0.37	264.97	.327E+04	2.9	0.90	19.08
0.51	265.11	.497E+04	5.3	1.11	15.51
0.65	265.25	.685E+04	8.5	1.28	13.40
0.78	265.38	.890E+04	12.4	1.43	11.98
0.92	265.52	.111E+05	16.9	1.57	10.95
1.06	265.66	.135E+05	22.2	1.69	10.16
1.19	265.79	.161E+05	28.2	1.80	9.53
1.33	265.93	.189E+05	34.9	1.90	9.01
1.47	266.07	.218E+05	42.4	2.00	8.58
1.61	266.21	.251E+05	49.7	2.04	8.42
1.74	266.34	.290E+05	58.3	2.07	8.30
1.88	266.48	.336E+05	68.3	2.09	8.21
2.02	266.62	.389E+05	79.9	2.11	8.13
2.15	266.75	.449E+05	93.0	2.13	8.05
2.29	266.89	.515E+05	108.5	2.17	7.91
2.43	267.03	.583E+05	126.0	2.22	7.71
2.56	267.16	.654E+05	145.1	2.28	7.51

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0090)	2663.47	65.56	12.00	103.01	1.84	2.08
OUTFLOW: ID= 1 (****)	2663.47	65.48	12.08	103.01	1.84	2.08

CALIB
NASHYD (1300)
ID= 1 DT=10.0 min

Area (ha)= 42.90 Curve Number (CN)= 80.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.53

Unit Hyd Qpeak (cms)= 3.092

PEAK FLOW (cms)= 3.583 (i)
TIME TO PEAK (hrs)= 7.167
RUNOFF VOLUME (mm)= 135.035
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.721

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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ADD HYD (0101)					
1 + 2 = 3					
	AREA	QPEAK	TPEAK	R.V.	
	(ha)	(cms)	(hrs)	(mm)	
ID1= 1 (****):	2663.47	65.476	12.08	103.01	
+ ID2= 2 (1300):	42.90	3.583	7.17	135.04	
=====					
ID = 3 (0101):	2706.37	66.496	11.75	103.51	

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
IN= 2---> OUT= 1 Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	259.27	0.0700	
224.90	256.32	0.0500 /0.0700	Main channel
234.22	255.44	0.0700	
241.28	255.24	0.0700	
245.63	256.44	0.0700	
278.81	257.64	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
0.10	255.34	.588E+02	0.0	0.11	46.94
0.20	255.44	.235E+03	0.1	0.17	29.57
0.33	255.57	.576E+03	0.5	0.28	17.82
0.46	255.70	.988E+03	1.2	0.37	13.64
0.59	255.83	.147E+04	2.2	0.44	11.35
0.72	255.96	.203E+04	3.4	0.51	9.86
0.85	256.09	.266E+04	5.0	0.57	8.80
0.98	256.22	.336E+04	7.0	0.63	7.99
1.11	256.35	.414E+04	9.4	0.69	7.32
1.24	256.48	.522E+04	12.2	0.71	7.12
1.36	256.60	.679E+04	15.2	0.68	7.45
1.49	256.73	.890E+04	19.6	0.67	7.57
1.62	256.86	.115E+05	25.5	0.67	7.55
1.75	256.99	.147E+05	33.0	0.68	7.42
1.88	257.12	.184E+05	42.3	0.70	7.23
2.01	257.25	.226E+05	53.6	0.72	7.01
2.14	257.38	.273E+05	67.0	0.74	6.79
2.27	257.51	.325E+05	82.7	0.77	6.56
2.40	257.64	.383E+05	100.8	0.80	6.34

<----- hydrograph ----->				<-pipe / channel->		
	AREA	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)	(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0101)	2706.37	66.50	11.75	103.51	2.14	0.74
OUTFLOW: ID= 1 (****)	2706.37	66.39	12.08	103.51	2.14	0.74

CALIB
NASHYD (1400)
ID= 1 DT=10.0 min

Area (ha)= 117.70 Curve Number (CN)= 74.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.97

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Unit Hyd Qpeak (cms)= 4.635

PEAK FLOW (cms)= 7.020 (i)
 TIME TO PEAK (hrs)= 7.667
 RUNOFF VOLUME (mm)= 122.299
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.653

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	259.27	0.0700	
224.90	256.32	0.0500 / 0.0700	Main channel
234.22	255.44	0.0700	
241.28	255.24	0.0700	
245.63	256.44	0.0700	
278.81	257.64	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV. TIME (min)
0.10	255.34	.130E+03	0.0	0.25	44.25
0.20	255.44	.521E+03	0.3	0.40	27.88
0.33	255.57	.127E+04	1.3	0.66	16.80
0.46	255.70	.219E+04	2.8	0.87	12.86
0.59	255.83	.326E+04	5.1	1.04	10.70
0.72	255.96	.449E+04	8.0	1.20	9.30
0.85	256.09	.588E+04	11.8	1.34	8.30
0.98	256.22	.743E+04	16.4	1.48	7.53
1.11	256.35	.915E+04	22.1	1.61	6.90
1.24	256.48	.115E+05	28.7	1.66	6.71
1.36	256.60	.150E+05	35.7	1.59	7.02
1.49	256.73	.197E+05	45.9	1.56	7.14
1.62	256.86	.255E+05	59.7	1.57	7.11
1.75	256.99	.325E+05	77.4	1.59	6.99
1.88	257.12	.406E+05	99.3	1.64	6.82
2.01	257.25	.499E+05	125.8	1.69	6.61
2.14	257.38	.604E+05	157.3	1.74	6.40
2.27	257.51	.720E+05	194.1	1.80	6.18
2.40	257.64	.848E+05	236.6	1.87	5.97

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (1400)	117.70	7.02	7.67	122.30	0.67	1.14
OUTFLOW: ID= 1 (****)	117.70	7.00	7.83	122.30	0.67	1.14

CALIB
 NASHYD (1500)
 ID= 1 DT=10.0 min

Area (ha)= 37.27 Curve Number (CN)= 74.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 0.72

unit Hyd Qpeak (cms)= 1.977

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PEAK FLOW (cms)= 2.518 (i)
 TIME TO PEAK (hrs)= 7.333
 RUNOFF VOLUME (mm)= 122.283
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.653

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0121)		AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3		(ha)	(cms)	(hrs)	(mm)
ID1= 1 (****):		2706.37	66.391	12.08	103.51
+ ID2= 2 (****):		117.70	6.997	7.83	122.30
ID = 3 (0121):		2824.07	69.968	11.75	104.30

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0121)		AREA	QPEAK	TPEAK	R.V.
3 + 2 = 1		(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0121):		2824.07	69.968	11.75	104.30
+ ID2= 2 (1500):		37.27	2.518	7.33	122.28
ID = 1 (0121):		2861.34	70.951	11.75	104.53

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)
 IN= 2----> OUT= 1 | Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->			
Distance	Elevation	Manning	
0.00	253.10	0.0700	
17.00	252.40	0.0500	Main Channel
29.00	251.60	0.0500	Main Channel
31.00	250.80	0.0500	Main Channel
35.00	251.00	0.0500	Main Channel
39.50	250.90	0.0500 / 0.0700	Main Channel
44.00	251.50	0.0700	
56.00	252.50	0.0700	
61.00	253.20	0.0700	

<----- TRAVEL TIME TABLE ----->					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	250.90	.294E+02	0.0	0.36	12.18
0.22	251.02	.226E+03	0.4	0.52	8.41
0.33	251.13	.543E+03	1.8	0.86	5.05
0.45	251.25	.895E+03	3.8	1.12	3.88
0.56	251.36	.128E+04	6.6	1.34	3.25
0.68	251.48	.170E+04	9.9	1.52	2.86
0.79	251.59	.217E+04	13.9	1.68	2.59
0.91	251.71	.270E+04	17.6	1.70	2.55
1.03	251.83	.333E+04	22.2	1.75	2.49

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1.14	251.94	.405E+04	27.9	1.80	2.42
1.26	252.06	.486E+04	34.7	1.86	2.33
1.37	252.17	.577E+04	42.8	1.93	2.25
1.49	252.29	.678E+04	52.2	2.01	2.17
1.61	252.41	.788E+04	63.0	2.09	2.08
1.72	252.52	.909E+04	77.8	2.23	1.95
1.84	252.64	.104E+05	94.4	2.37	1.84
1.95	252.75	.119E+05	112.7	2.48	1.75
2.07	252.87	.134E+05	132.8	2.59	1.68
2.18	252.98	.151E+05	154.7	2.68	1.62

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0121)	2861.34	70.95	11.75	104.53	1.67	2.16
OUTFLOW: ID= 1 (****)	2861.34	70.94	11.75	104.53	1.67	2.16

CALIB	Area (ha)=	8.90	Curve Number (CN)=	74.0
NASHYD (1600)	Ia (mm)=	5.00	# of Linear Res.(N)=	3.00
ID= 1 DT=10.0 min	U.H. Tp(hrs)=	0.78		

Unit Hyd Qpeak (cms)= 0.436

PEAK FLOW (cms)= 0.580 (i)
 TIME TO PEAK (hrs)= 7.333
 RUNOFF VOLUME (mm)= 122.289
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.653

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0110)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (****):	2861.34	70.941	11.75	104.53
+ ID2= 2 (1600):	8.90	0.580	7.33	122.29
ID = 3 (0110):	2870.24	71.182	11.75	104.59

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (****)	Routing time step (min)'=	10.00
IN= 2---> OUT= 1		

Distance	Elevation	Manning	
10.00	249.90	0.1000	
86.00	248.10	0.1000 /0.0350	Main Channel
88.00	246.81	0.0350	Main Channel
107.00	247.20	0.0350	Main Channel
112.00	248.90	0.0350 /0.0600	Main Channel
132.00	247.90	0.0600	
164.00	249.40	0.0600	

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TRAVEL TIME TABLE					
DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.13	246.94	.133E+03	0.2	0.36	14.71
0.26	247.07	.532E+03	1.0	0.57	9.26
0.39	247.20	.120E+04	2.8	0.75	7.07
0.52	247.33	.201E+04	6.5	1.03	5.13
0.64	247.45	.285E+04	11.4	1.28	4.15
0.77	247.58	.371E+04	17.4	1.49	3.55
0.90	247.71	.460E+04	24.4	1.69	3.14
1.03	247.84	.551E+04	32.4	1.87	2.84
1.16	247.97	.648E+04	41.3	2.03	2.61
1.29	248.10	.767E+04	51.3	2.13	2.49
1.43	248.24	.942E+04	64.6	2.18	2.43
1.58	248.39	.117E+05	80.0	2.17	2.45
1.72	248.53	.146E+05	97.9	2.13	2.49
1.87	248.68	.181E+05	118.6	2.08	2.55
2.01	248.82	.222E+05	142.4	2.04	2.59
2.16	248.97	.268E+05	170.6	2.03	2.62
2.30	249.11	.318E+05	203.6	2.03	2.61
2.45	249.26	.373E+05	240.0	2.05	2.59
2.59	249.40	.432E+05	280.2	2.06	2.57

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0110)	2870.24	71.18	11.75	104.59	1.50	2.17
OUTFLOW: ID= 1 (****)	2870.24	71.16	11.83	104.59	1.49	2.17

CALIB
NASHYD (1700)
ID= 1 DT=10.0 min

Area (ha)= 21.80 Curve Number (CN)= 74.0
Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= 0.82

Unit Hyd Qpeak (cms)= 1.015
PEAK FLOW (cms)= 1.396 (i)
TIME TO PEAK (hrs)= 7.500
RUNOFF VOLUME (mm)= 122.293
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.653

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0123)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2870.24	71.155	11.83	104.59
+ ID2= 2 (1700):	21.80	1.396	7.50	122.29
===== ID = 3 (0123):	2892.04	71.751	11.75	104.72

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

| ROUTE CHN (****) |

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 | IN= 2---> OUT= 1 | Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	251.28	0.0450	
32.00	250.70	0.0450	
84.00	249.60	0.0450	
91.00	249.10	0.0450 /0.0320	Main Channel
96.00	248.60	0.0320	Main Channel
100.00	248.90	0.0320 /0.0450	Main Channel
112.00	250.45	0.0450	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.07	248.68	.889E+01	0.0	0.28	8.17
0.15	248.75	.356E+02	0.1	0.44	5.14
0.22	248.82	.800E+02	0.3	0.58	3.93
0.30	248.90	.142E+03	0.7	0.70	3.24
0.40	249.00	.253E+03	1.7	0.90	2.50
0.51	249.11	.390E+03	3.1	1.07	2.12
0.61	249.21	.555E+03	5.1	1.25	1.81
0.71	249.31	.752E+03	7.7	1.39	1.63
0.82	249.42	.980E+03	10.9	1.50	1.50
0.92	249.52	.124E+04	14.6	1.60	1.41
1.02	249.62	.153E+04	19.0	1.68	1.35
1.13	249.73	.189E+04	23.9	1.72	1.32
1.23	249.83	.233E+04	29.9	1.74	1.30
1.33	249.93	.284E+04	37.0	1.76	1.28
1.44	250.04	.344E+04	45.3	1.79	1.26
1.54	250.14	.412E+04	55.0	1.81	1.25
1.64	250.24	.487E+04	66.1	1.84	1.23
1.75	250.35	.571E+04	78.7	1.87	1.21
1.85	250.45	.662E+04	93.0	1.90	1.19

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0123)	2892.04	71.75	11.75	104.72	1.69	1.85
OUTFLOW: ID= 1 (****)	2892.04	71.76	11.83	104.72	1.69	1.85

CALIB			
NASHYD (1800)	Area (ha)=	3.82	Curve Number (CN)= 78.0
ID= 1 DT=10.0 min	Ia (mm)=	5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)=	0.10	

Unit Hyd Qpeak (cms)= 1.459
 PEAK FLOW (cms)= 0.281 (i)
 TIME TO PEAK (hrs)= 7.000
 RUNOFF VOLUME (mm)= 99.787
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.533

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

| ADD HYD (0130) |

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	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	2892.04	71.756	11.83	104.72
+ ID2= 2 (1800):	3.82	0.281	7.00	99.79
=====				
ID = 3 (0130):	2895.86	71.814	11.83	104.71

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ROUTE CHN (0124)
IN= 2----> OUT= 1 | Routing time step (min)'= 5.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	251.01	0.0700	
76.16	250.14	0.0500	Main Channel
84.69	248.40	0.0500 / 0.0700	Main Channel
92.28	246.41	0.0700	
100.53	248.07	0.0700	
119.66	248.85	0.0700	
150.39	250.47	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.20	246.61	.712E+02	0.0	0.11	62.27
0.40	246.81	.285E+03	0.1	0.17	39.23
0.60	247.01	.641E+03	0.4	0.23	29.94
0.80	247.21	.114E+04	0.8	0.28	24.71
1.00	247.41	.178E+04	1.4	0.32	21.30
1.19	247.60	.256E+04	2.3	0.36	18.86
1.39	247.80	.349E+04	3.4	0.40	17.02
1.59	248.00	.456E+04	4.9	0.44	15.57
1.79	248.20	.584E+04	6.2	0.43	15.75
1.99	248.40	.756E+04	8.0	0.43	15.82
2.22	248.63	.101E+05	11.2	0.45	15.05
2.45	248.86	.133E+05	15.7	0.48	14.19
2.68	249.09	.171E+05	21.8	0.52	13.12
2.91	249.32	.214E+05	29.2	0.56	12.21
3.14	249.55	.262E+05	38.2	0.60	11.44
3.37	249.78	.316E+05	48.9	0.63	10.76
3.60	250.01	.374E+05	61.3	0.67	10.18
3.83	250.24	.439E+05	75.8	0.71	9.67
4.06	250.47	.525E+05	93.1	0.73	9.40

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	<-pipe / channel-> MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0130)	2895.86	71.81	11.83	104.71	3.77	0.70
OUTFLOW: ID= 1 (0124)	2895.86	71.62	11.92	104.71	3.76	0.70

CALIB	Area (ha)=	Curve Number (CN)=
NASHYD (1900)	10.25	80.0
ID= 1 DT=10.0 min	Ia (mm)= 5.00	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= 0.33	

Unit Hyd Qpeak (cms)= 1.186

Timmins Results.txt

PEAK FLOW (cms)= 0.959 (i)
 TIME TO PEAK (hrs)= 7.000
 RUNOFF VOLUME (mm)= 134.579
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.719

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0150)
 1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0124):	2895.86	71.622	11.92	104.71
+ ID2= 2 (1900):	10.25	0.959	7.00	134.58
<hr/>				
ID = 3 (0150):	2906.11	71.835	11.92	104.82

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

CALIB
 NASHYD (2000)
 ID= 1 DT=10.0 min

Area (ha)= 125.00 Curve Number (CN)= 67.0
 Ia (mm)= 5.00 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.50

Unit Hyd Qpeak (cms)= 3.183

PEAK FLOW (cms)= 5.725 (i)
 TIME TO PEAK (hrs)= 9.167
 RUNOFF VOLUME (mm)= 108.033
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.577

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ROUTE CHN (****)
 IN= 2---> OUT= 1

Routing time step (min)'= 10.00

<----- DATA FOR SECTION (1.1) ----->

Distance	Elevation	Manning	
0.00	256.00	0.0700	
41.00	250.00	0.0500	Main Channel
126.00	249.50	0.0500 /0.0700	Main Channel
131.00	249.00	0.0700	
136.00	249.50	0.0700	
217.00	250.00	0.0700	
283.00	251.30	0.0700	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
0.10	249.10	.666E+02	0.0	0.14	77.86
0.20	249.20	.267E+03	0.1	0.23	49.05
0.30	249.30	.600E+03	0.3	0.30	37.43
0.40	249.40	.107E+04	0.6	0.36	30.90
0.50	249.50	.167E+04	1.0	0.42	26.63
0.63	249.63	.435E+04	2.0	0.30	36.91
0.76	249.76	.107E+05	5.9	0.37	30.24

Timmins Results.txt

0.89	249.89	.207E+05	14.0	0.45	24.61
1.01	250.01	.343E+05	27.9	0.54	20.52
1.14	250.14	.498E+05	50.9	0.68	16.32
1.27	250.27	.659E+05	79.4	0.80	13.83
1.40	250.40	.826E+05	113.3	0.91	12.16
1.53	250.53	.100E+06	152.3	1.01	10.95
1.66	250.66	.118E+06	196.3	1.11	10.02
1.79	250.79	.137E+06	245.3	1.20	9.28
1.91	250.91	.156E+06	299.3	1.28	8.68
2.04	251.04	.176E+06	358.1	1.36	8.18
2.17	251.17	.196E+06	421.8	1.43	7.76
2.30	251.30	.218E+06	490.5	1.50	7.39

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (2000)	125.00	5.72	9.17	108.03	0.75	0.36
OUTFLOW: ID= 1 (****)	125.00	5.64	9.50	108.03	0.75	0.36

CALIB
NASHYD (2100)
ID= 1 DT=10.0 min

Area (ha)= 34.30
Ia (mm)= 5.00
U.H. Tp(hrs)= 0.36

Curve Number (CN)= 80.0
of Linear Res.(N)= 3.00

Unit Hyd Qpeak (cms)= 3.639

PEAK FLOW (cms)= 3.163 (i)
TIME TO PEAK (hrs)= 7.000
RUNOFF VOLUME (mm)= 134.734
TOTAL RAINFALL (mm)= 187.210
RUNOFF COEFFICIENT = 0.720

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0160)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (****):	125.00	5.642	9.50	108.03
+ ID2= 2 (0150):	2906.11	71.835	11.92	104.82
ID = 3 (0160):	3031.11	76.138	11.83	104.95

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

ADD HYD (0160)
3 + 2 = 1

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0160):	3031.11	76.138	11.83	104.95
+ ID2= 2 (2100):	34.30	3.163	7.00	134.73
ID = 1 (0160):	3065.41	76.917	11.58	105.28

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

Timmins Results.txt

```

-----
| CALIB                                     |
| NASHYD      (2200)                       | Area   (ha)= 10.21  Curve Number (CN)= 78.0
| ID= 1 DT=10.0 min                       | Ia     (mm)=  5.00  # of Linear Res.(N)= 3.00
|-----|
|                                     | U.H. Tp(hrs)=  0.21

```

Unit Hyd Qpeak (cms)= 1.857

PEAK FLOW (cms)= 0.947 (i)
 TIME TO PEAK (hrs)= 7.000
 RUNOFF VOLUME (mm)= 127.937
 TOTAL RAINFALL (mm)= 187.210
 RUNOFF COEFFICIENT = 0.683

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
| ADD HYD      (0170)                       |
| 1 + 2 = 3                                     |
|-----|
| ID1= 1 (0160): 3065.41 76.917 11.58 105.28 |
| + ID2= 2 (2200): 10.21  0.947  7.00 127.94 |
|-----|
| ID = 3 (0170): 3075.62 77.121 11.58 105.36 |

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

FINISH

Appendix F
Sensitivity Analyses - Hydrology

Hydrologic Sensitivity Analyses

The hydrologic model was tested for sensitivity for the input parameters in the list below. Input parameters were modified by varying degrees as outlined below for the Regional Storm event only (Timmins Event). The increase/decrease in peak flows from the base scenario at a number of key nodes was noted to establish a level of confidence in peak flow estimations. This was done to assess flood elevation sensitivity relative to the accuracy of peak flow estimates in the hydraulic modelling. The following parameters were tested for sensitivity:

- Curve Number (CN*) (+/- 20%);
- Initial Abstraction (+/- 50%);
- Model Time Step (+/- 50%);
- Removal of Channel Routing;
- Channel Routing Length (+/- 20%);
- Subcatchment Travel Length (+/- 20%); and
- Model Time Step (DT (+/- 50%).

Curve Number (CN*)

Flows at key nodes were investigated to see the impact of changing the CN* value. Increasing CN* by 20% resulted in an average increase in peak flow of 27% at all key flow nodes during the Timmins storm event. Decreasing CN* by 20% resulted in an average decrease in peak flow of 24% at all key flow nodes during the Timmins storm event. Because there is a significant difference in peak flow values as a result of modifying the CN* value, it is imperative to get an accurate CN* value.

CN* is determined by land use and soil type. Soil type information is extracted from the digitized Victoria County soils map originally produced as a joint venture by the Federal Department of Agriculture and the Ontario Agricultural College. Land use is derived from the City of Kawartha Lakes' Secondary Plan and zoning maps as well as the 2010 Ecological Land Classification (ELC) mapping. Aerial orthophotography was reviewed to confirm land use throughout the watershed. This base data is valid, and therefore any calculated value (such as CN*) based on this data truly represents the land.

Initial abstraction (I_a)

Initial abstraction is a parameter that accounts for losses such as infiltration, evaporation, surface depression storage etc. prior to the occurrence of any runoff. This value is typically very small in comparison to the volume of rainfall for a larger storm event and has a larger effect on smaller storm events. Therefore, it is expected that initial abstraction would have little to no effect on a substantial event such as the Timmins storm.

Increasing Initial Abstraction by 50% resulted in an average decrease in peak flow of 2% at all key flow nodes during the Timmins storm event. Decreasing initial abstraction by 50% resulted in an average increase in peak flow of less than 1% at all key flow nodes during the Timmins storm event. Therefore, changing the initial abstraction does not result in significantly different flows.

Subcatchment Travel Length (TL)

The travel length is used to determine the flow time of concentration for a subcatchment area. A small travel length increases peak flows, as smaller travel lengths also reduce the overland flow gradient which can also increase peak flow. Flow lengths were delineated automatically using GIS

software, and was revised based aerial topography and engineering judgement (by straightening flow paths or realigning flow paths to channels, municipal drains or swales).

Increasing subcatchment travel length by 20% resulted in an average decrease in peak flow of 3% at all key flow nodes during the Timmins storm event. Decreasing subcatchment travel length by 20% resulted in an average increase in peak flow of 2% at all key flow nodes during the Timmins storm event. Changing the subcatchment travel length is considered to be significant for the study area.

Channel Routing Removed

Channel routing accounts for the storage of flow as it is conveyed along the watercourse and its floodplain. This results in the attenuation of flows through a watercourse. The overall watershed involves a variety of intricate watercourses connecting subcatchments together, and therefore it is expected that removing any channel routing would result in a substantial increase in peak flows. Removal of channel routing assumes that peak flows from catchments occurs at one point, and therefore does not consider the effect of storage and travel time as flow travels between flow nodes.

A scenario was created by removing all channel routing within the model. Removing all channel routing resulted in an average increase in peak flow of 75% at all key flow nodes during the Timmins storm event. Therefore, channel routing has a substantial effect on peak flows throughout the watershed. Eliminating all channel routing would not be considered valid, as the watershed is very long with a number of watercourses between each catchment.

Channel Routing Lengths

Channel routing lengths were varied by +/- 20% to determine the effects storage on peak flows. A smaller channel routing length would result in an increased slope and lower storage volume, therefore resulting in a reduced travel time and peak flow attenuation from node to node. Channel routing lengths were delineated automatically using GIS software, and was revised based aerial topography, known water courses and engineering judgement.

Increasing channel routing lengths by 20% resulted in an average decrease in peak flow of 13% at all key flow nodes during the Timmins storm event. Decreasing channel routing length by 20% resulted in an average increase in peak flow of 14% at all key flow nodes during the Timmins storm event. Therefore, changing the channel routing length results is somewhat significant.

Channel routing lengths can be considered relatively accurate, as watercourses can be visually confirmed via aerial orthophotography or official watercourses. Therefore, there is confidence that acceptable channel routing lengths were applied.

Model Time Step (DT)

The model time step of 10 minutes was modified by changing it by +/- 5 minutes at all subcatchments and channel routing. There was little to no affect on peak flows at all flow nodes during the Timmins Storm Event (less than 0.5%). Therefore, time step has no effect on the regulatory flows.

Regional Event Peak Flow (m3/s)

Location	Hydrologic Flow Node	Base	Curve Number		Initial Abstraction		Subcatchment Travel Length		Channel Routing			Time Step	
			CN+20%	CN-20%	IA+50%	IA-50%	TL+20%	TL-20%	No RC	RC+20%	RC-20%	DT+50%	DT-50%
			Top of System, US of Sturgeon	90	65.6	83.66	50.07	64.5	66.3	63.7	67.0	114.0	57.3
DS of Community Centre	101	66.5	84.66	50.06	65.3	67.2	64.4	67.9	116.2	58.0	75.9	66.5	66.5
DS of HWY 36 (W)	121	71.0	89.97	54.06	69.5	71.6	68.6	72.4	124.2	62.0	80.5	70.9	70.9
DS of Cedar Glen Road	110	71.2	90.27	54.24	69.7	71.9	68.8	72.7	124.6	62.2	80.8	71.1	71.1
DS of HWY 36 (E)	123	71.8	90.97	54.68	70.3	71.4	69.3	73.3	125.7	62.8	81.4	71.7	71.7
DS of Herons Landing	130	71.8	91.04	54.71	70.3	72.5	69.3	73.4	125.8	62.8	81.5	71.8	71.8
DS of Herons Landing 2	150	71.8	91.07	54.84	70.5	72.6	69.5	73.5	126.3	62.7	81.3	71.9	71.9

Location	Hydrologic Flow Node	Curve Number		Initial Abstraction		Subcatchment Travel Length		Channel Routing			Time Step		
		CN+20%	CN-20%	IA+50%	IA-50%	TL+20%	TL-20%	No RC	RC+20	RC-20	DT+50%	DT-50%	
		Top of System, US of Sturgeon	90	27.6%	-23.6%	-1.6%	1.2%	-2.9%	2.1%	74%	-13%	14%	0%
DS of Community Centre	101	27.3%	-24.7%	-1.8%	1.1%	-3.2%	2.1%	75%	-13%	14%	0%	0%	
DS of HWY 36 (W)	121	26.8%	-23.8%	-2.1%	0.9%	-3.4%	2.1%	75%	-13%	14%	0%	0%	
DS of Cedar Glen Road	110	26.8%	-23.8%	-2.1%	1.0%	-3.3%	2.1%	75%	-13%	14%	0%	0%	
DS of HWY 36 (E)	123	26.8%	-23.8%	-2.0%	-0.4%	-3.4%	2.2%	75%	-13%	14%	0%	0%	
DS of Herons Landing	130	26.8%	-23.8%	-2.0%	1.0%	-3.5%	2.2%	75%	-13%	13%	0%	0%	
DS of Herons Landing 2	150	26.8%	-23.7%	-1.8%	1.0%	-3.3%	2.4%	76%	-13%	13%	0%	0%	
		<i>Minimum =</i>	<i>26.8%</i>	<i>-24.7%</i>	<i>-2.1%</i>	<i>-0.4%</i>	<i>-3.5%</i>	<i>2.1%</i>	<i>73.8%</i>	<i>-12.7%</i>	<i>13.2%</i>	<i>-0.1%</i>	<i>-0.1%</i>
		<i>Average =</i>	<i>27.0%</i>	<i>-23.9%</i>	<i>-1.9%</i>	<i>0.8%</i>	<i>-3.3%</i>	<i>2.2%</i>	<i>75.0%</i>	<i>-12.6%</i>	<i>13.6%</i>	<i>0.0%</i>	<i>0.0%</i>
		<i>Maximum =</i>	<i>27.6%</i>	<i>-23.6%</i>	<i>-1.6%</i>	<i>1.2%</i>	<i>-2.9%</i>	<i>2.4%</i>	<i>75.8%</i>	<i>-12.5%</i>	<i>14.1%</i>	<i>0.0%</i>	<i>0.0%</i>

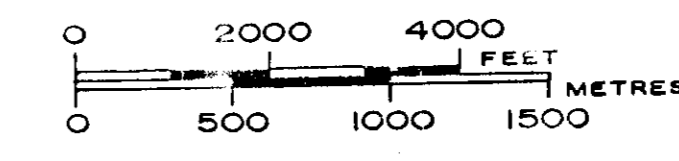
Appendix G
Official & Secondary Plan Maps

THE CORPORATION OF THE
TOWNSHIP OF VERULAM
SCHEDULE 'A'
TO
ZONING BY-LAW NO. 6-87
AS AMENDED

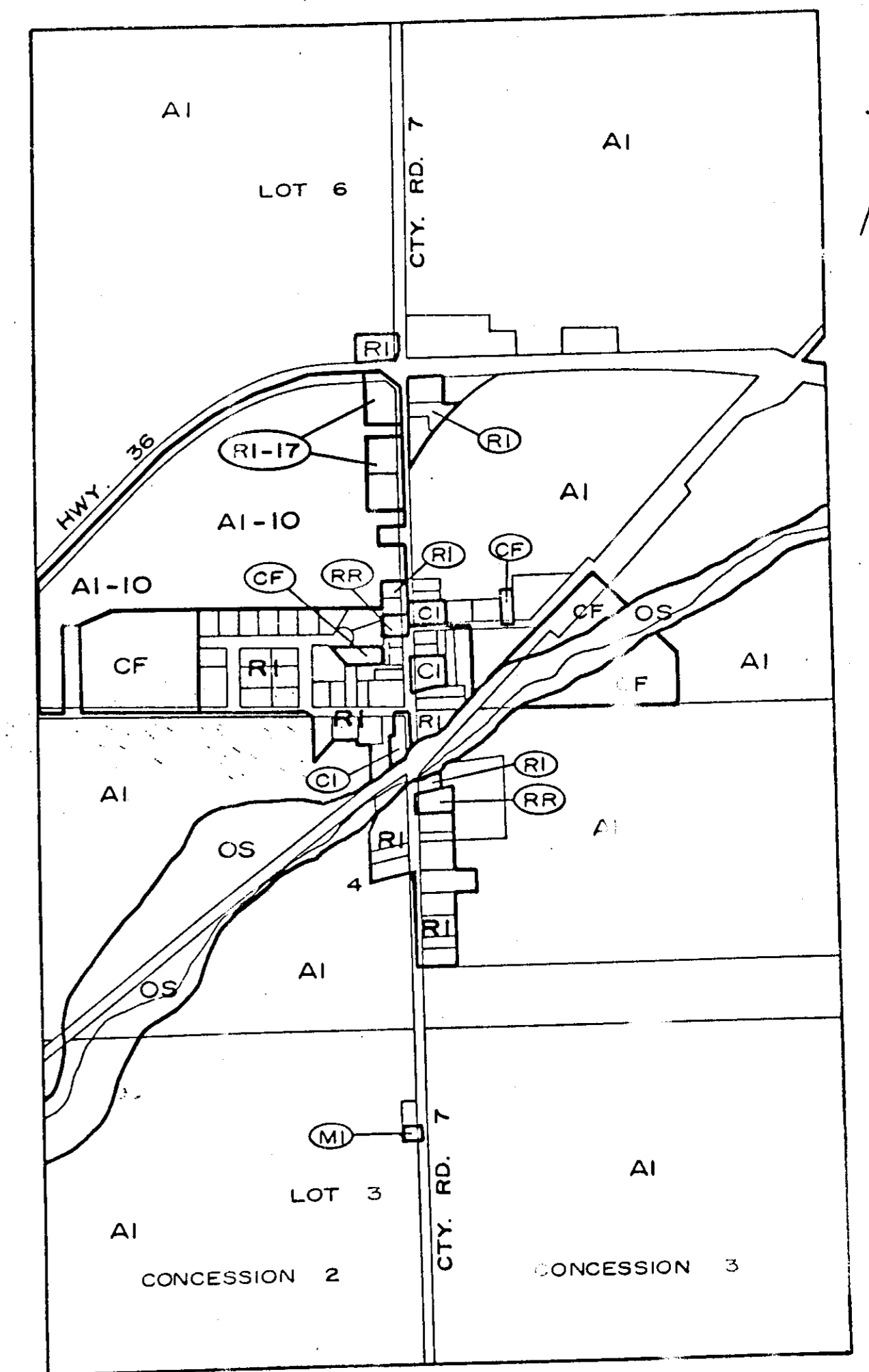
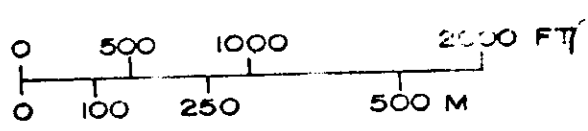
CONSOLIDATED APRIL 2009

ZONES SYMBOLS

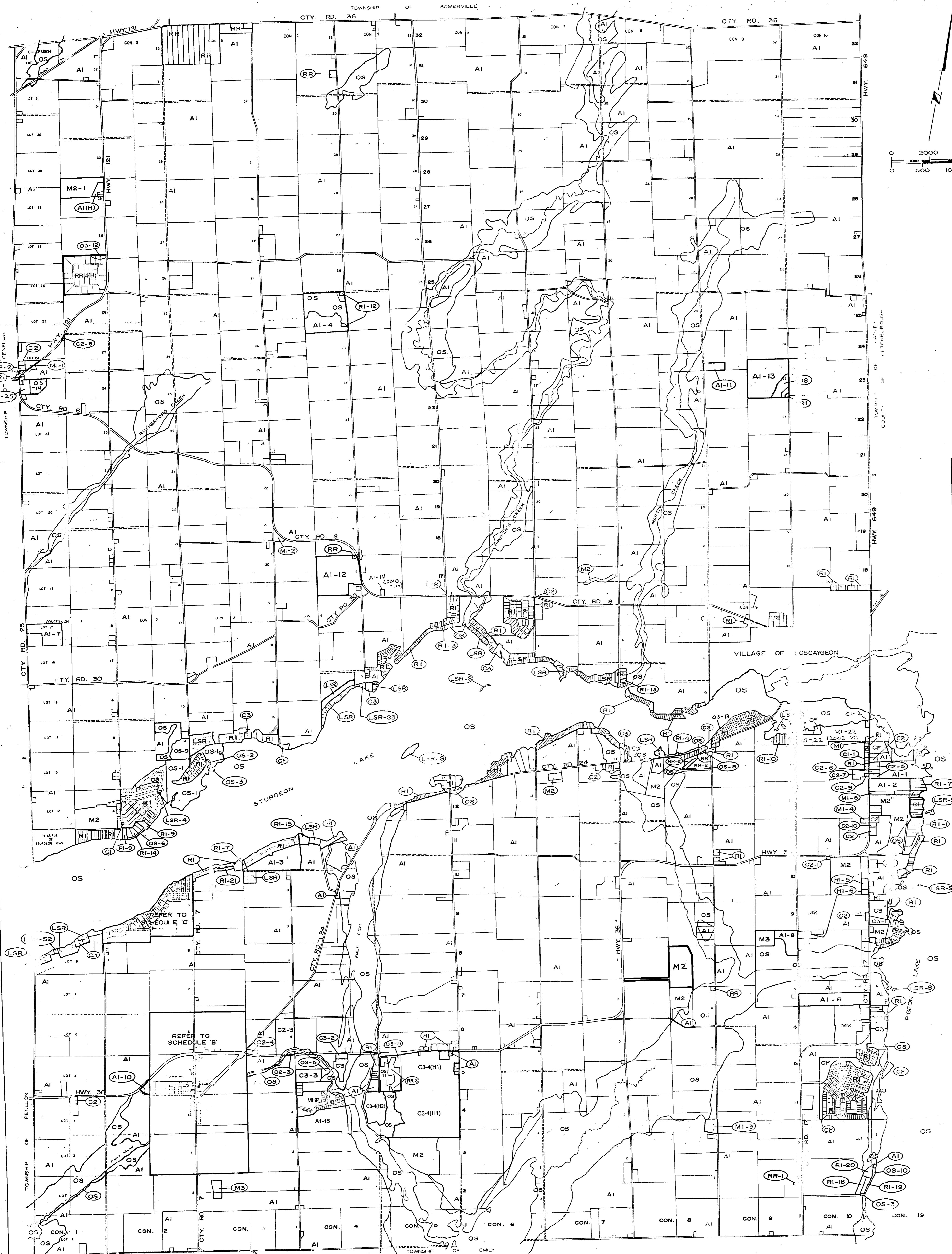
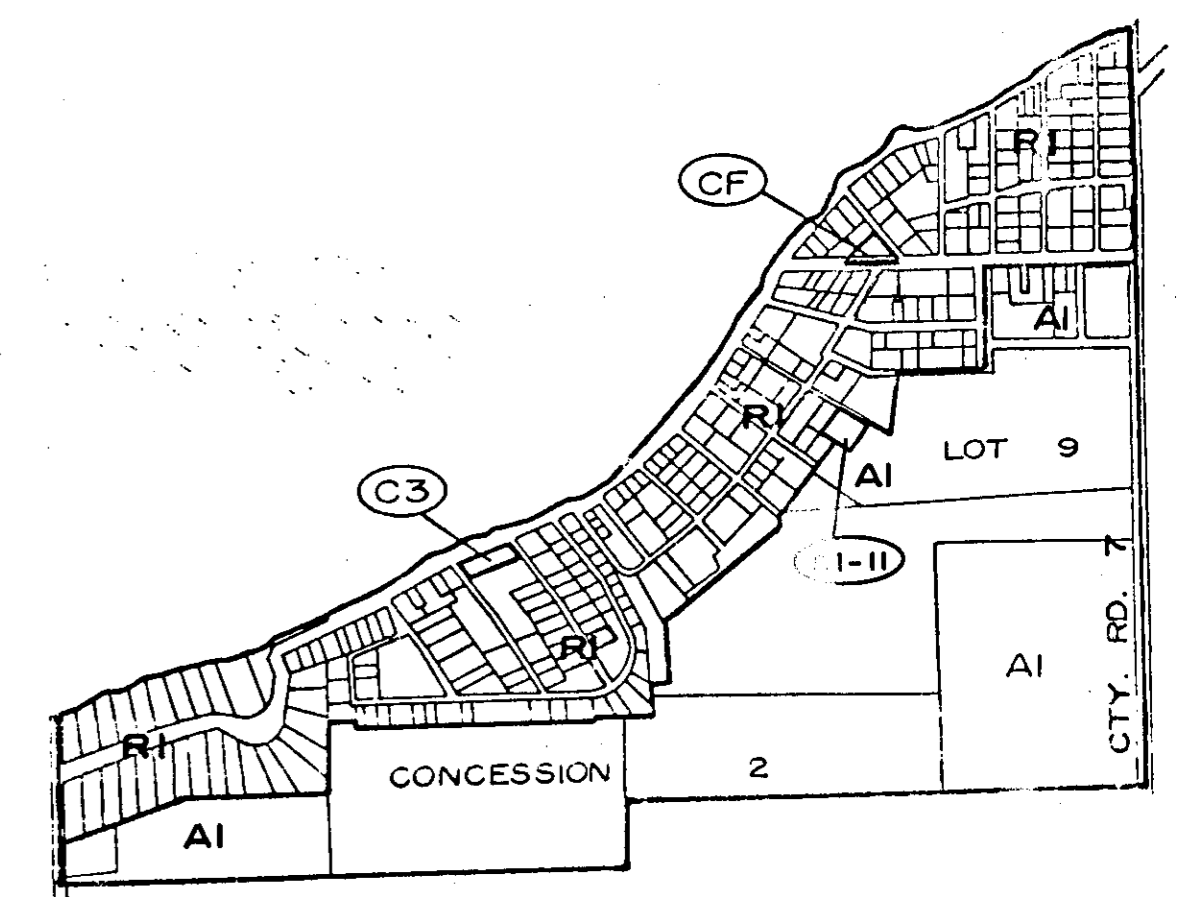
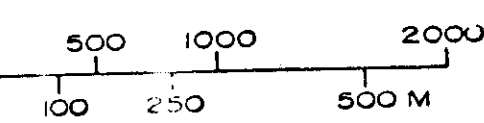
RESIDENTIAL ZONES	
Rural Residential Zone	RR
Residential Type One Zone	R1
Residential Type Two Zone	R2
Limited Service Residential Zone	LSR
COMMERCIAL ZONES	
General Commercial Zone	C1
Highway Commercial Zone	C2
Recreational Commercial Zone	C3
INDUSTRIAL ZONES	
General Industrial Zone	M1
Extractive Industrial Zone	M2
Disposal Industrial Zone	M3
COMMUNITY FACILITY ZONE	
CF	CF
OPEN SPACE ZONE	
OS	OS
RURAL ZONES	
General Rural Zone	A1
MOBILE HOME PARK ZONE	
MHP	MHP



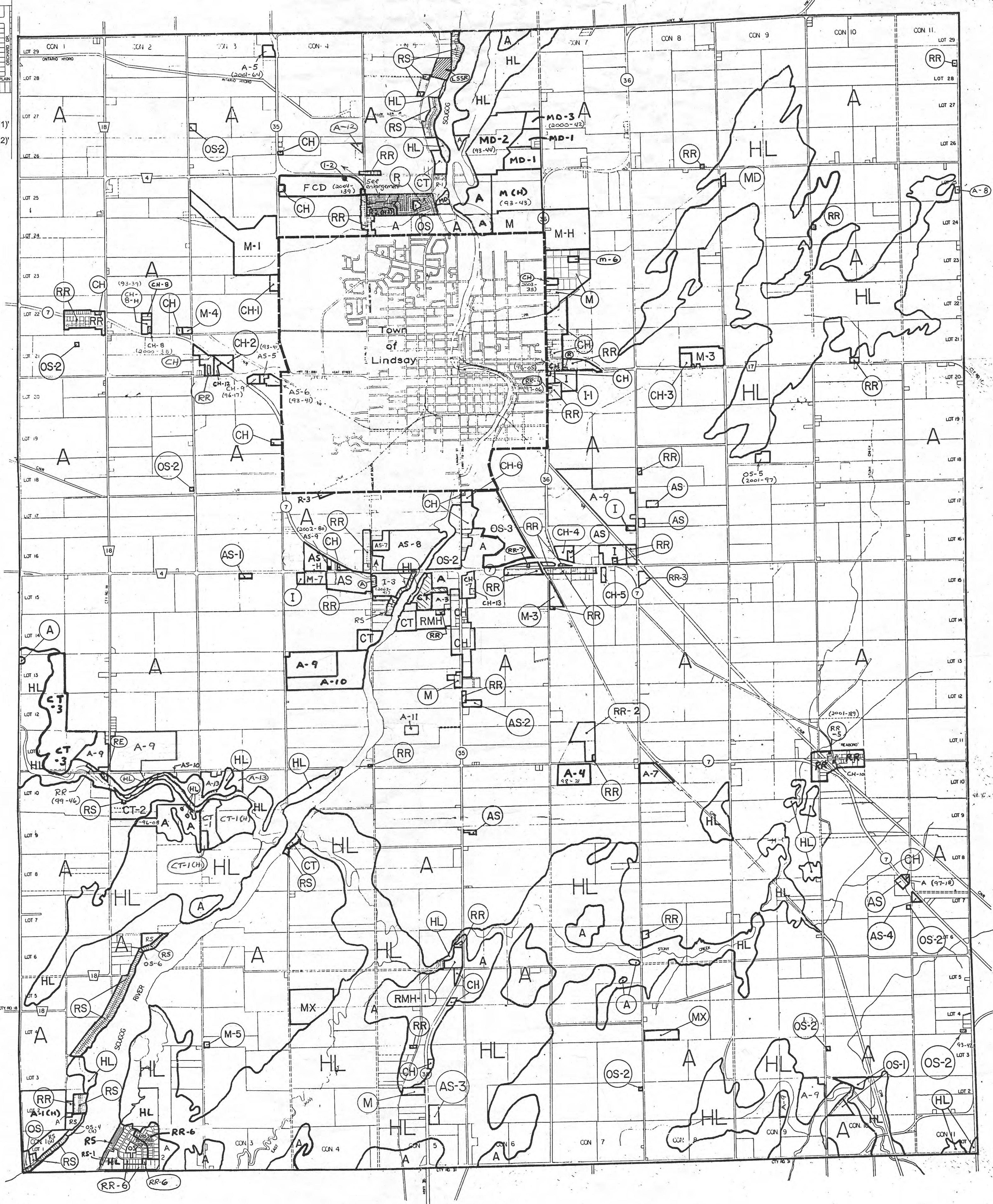
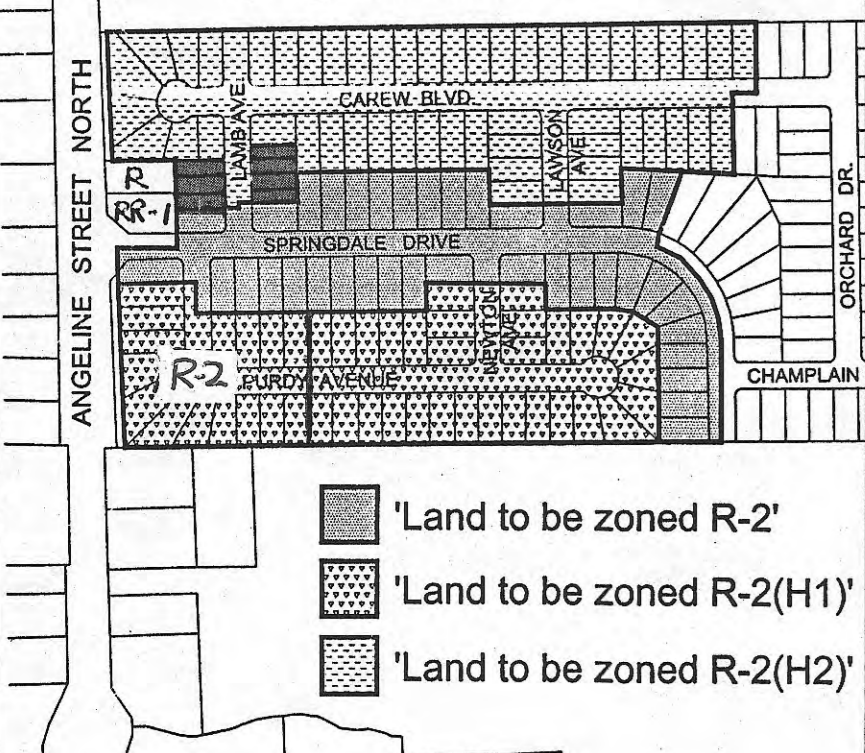
'DUNSFORD'
SCHEDULE 'B'



'GREENHURST - THURSTONIA'
SCHEDULE 'C'



'Springdale Gardens'



Schedule "A" Township of Ops Zoning By-Law

THIS SCHEDULE REFLECTS A DRAFT CONSOLIDATION AND REFERENCE SHOULD BE HAD TO THE ACTUAL AMENDING BY-LAWS FOR COMPLETE ACCURACY.

CONSOLIDATED 2012

This is Schedule "A" to By-Law No. 93-30
Passed the 20th day of September, 1993

Sharon McCree
Reeve

Sandra Bickel
Clerk

LEGEND

- Town of Lindsay Boundary
- Zone Boundary
- Provincial Highway
- County Road
- Township Road

ZONE

- Estate Residential RE
- Rural Residential RR
- Shoreline Residential RS
- Residential R
- Mobile Home Residential RMH
- Institutional I
- Highway Commercial CH
- Tourist Commercial CT
- General Industrial M
- Extractive Industrial MX
- Disposal Industrial MD
- Open Space OS
- Agricultural A
- Agricultural Support AS
- Hazard Land HZ
- Future Community Development FCD
- Lands not subject to By-law
- LIMITED SERVICE SHORELINE RESIDENTIAL LSSR

SYMBOL

- RE
- RR
- RS
- R
- RMH
- I
- CH
- CT
- M
- MX
- MD
- OS
- A
- AS
- HZ
- FCD
-

Number	Revision	Revised By	Date
1	MINOR CHANGES	JMTCHELL	AUG 17/93
2	CHANGES	JMTCHELL	JUNE 22/93
Drawn By: JMTCHELL Checked By: Date: JUNE 7, 1993 Scale: 1:1000 0 2000 4000 FT			
115 Collier Street Markham, Ontario L4M 1R3 (705) 737-4512		50 Yorkville Avenue Suite 200 Toronto, Ontario M4W 1L4 (416) 975-1556	

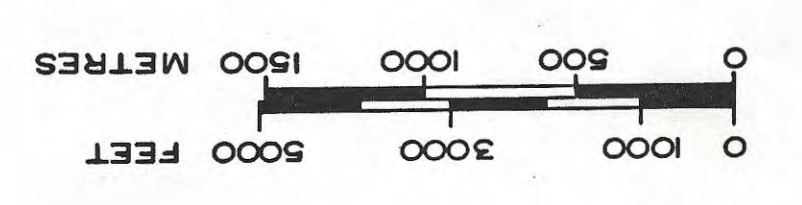
THIS SCHEDULE REFLECTS A DRAFT
CONSOLIDATION AND REFERENCE SHOULD
BE MADE TO THE ACTUAL AMENDING
BY-LAWS FOR COMPLETE ACCURACY.

THE CORPORATION OF THE
TOWNSHIP OF FENELON
SCHEDULE 'A'

TO
ZONING BY-LAW NO. 12-95

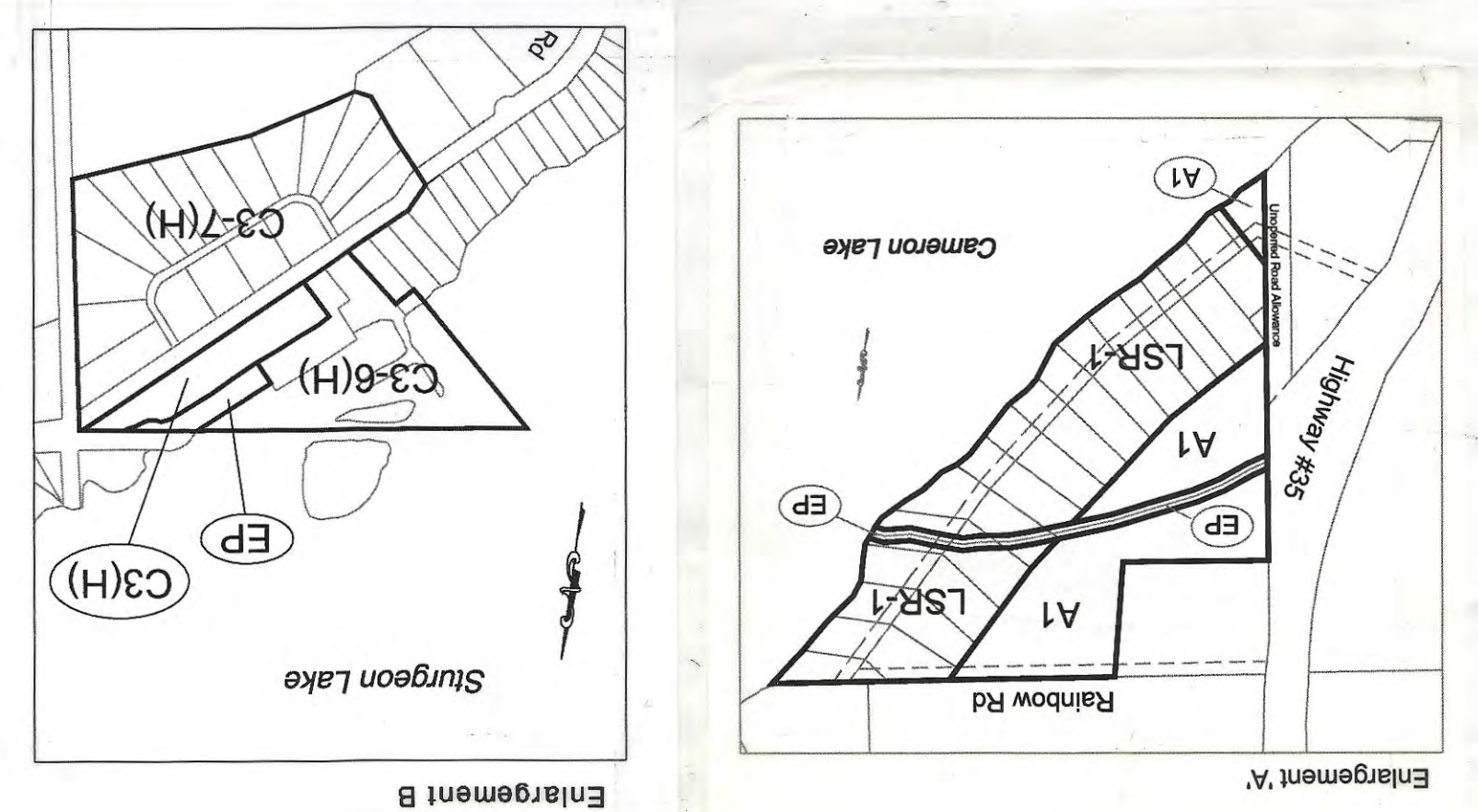
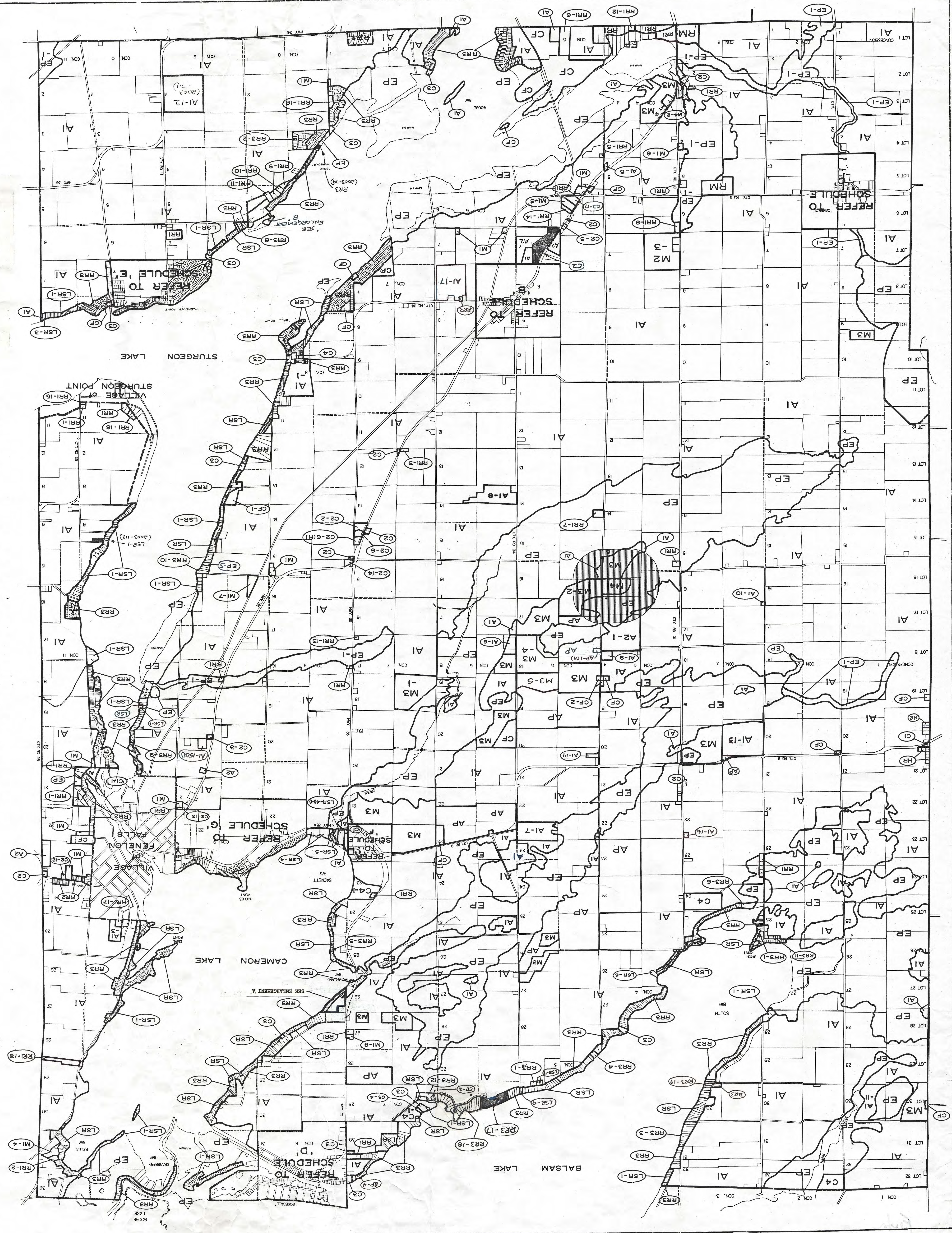
AS AMENDED

CONSOLIDATED JANUARY 2014



LEGEND

- | | |
|-------------------------|------------------------------|
| Symbol | Zone |
| EP | ENVIRONMENTAL PROTECTION |
| AP | AGGREGATE PROTECTION |
| CF | COMMUNITY FACILITY |
| A1 | AGRICULTURAL |
| A2 | RURAL GENERAL |
| HR | HAMLET RESIDENTIAL |
| RRI | RURAL RESIDENTIAL TYPE ONE |
| RR2 | RURAL RESIDENTIAL TYPE TWO |
| RR3 | RURAL RESIDENTIAL TYPE THREE |
| RM | RESIDENTIAL MOBILE HOME PARK |
| LSR | LIMITED SERVICE RESIDENTIAL |
| C1 | GENERAL COMMERCIAL |
| C2 | HIGHWAY COMMERCIAL |
| C3 | TOURIST COMMERCIAL |
| C4 | CAMPGROUND COMMERCIAL |
| M1 | RESTRICTED INDUSTRIAL |
| M2 | GENERAL INDUSTRIAL |
| M3 | EXTRACTIVE INDUSTRIAL |
| M4 | DISPOSAL INDUSTRIAL |
| (H) | REFER TO SECTION 3.8.1 |
| (H) with diagonal lines | REFER TO SECTION 3.18.1.4 |
| — | ZONE BOUNDARY |



AS AMENDED IN ACCORDANCE WITH THE
DECISION OF THE ONTARIO MUNICIPAL BOARD.
(FILE NO. R950145) AUGUST 23, 1995

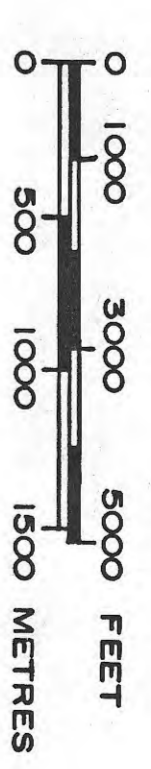
THE CORPORATION OF THE
TOWNSHIP OF EMILY

SCHEDULE 'A'

TO
ZONING BY-LAW NO. 1996-30
AS AMENDED

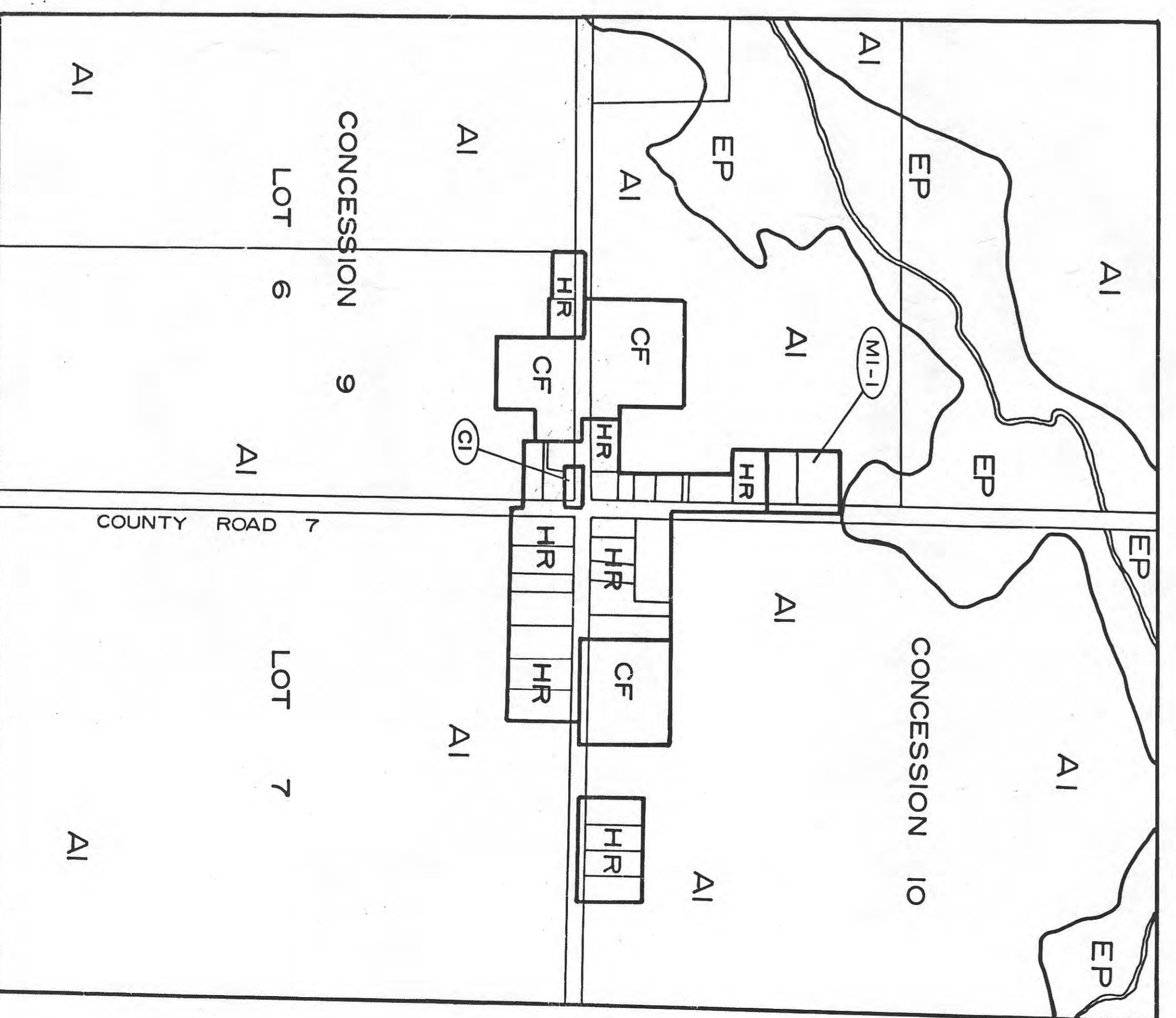
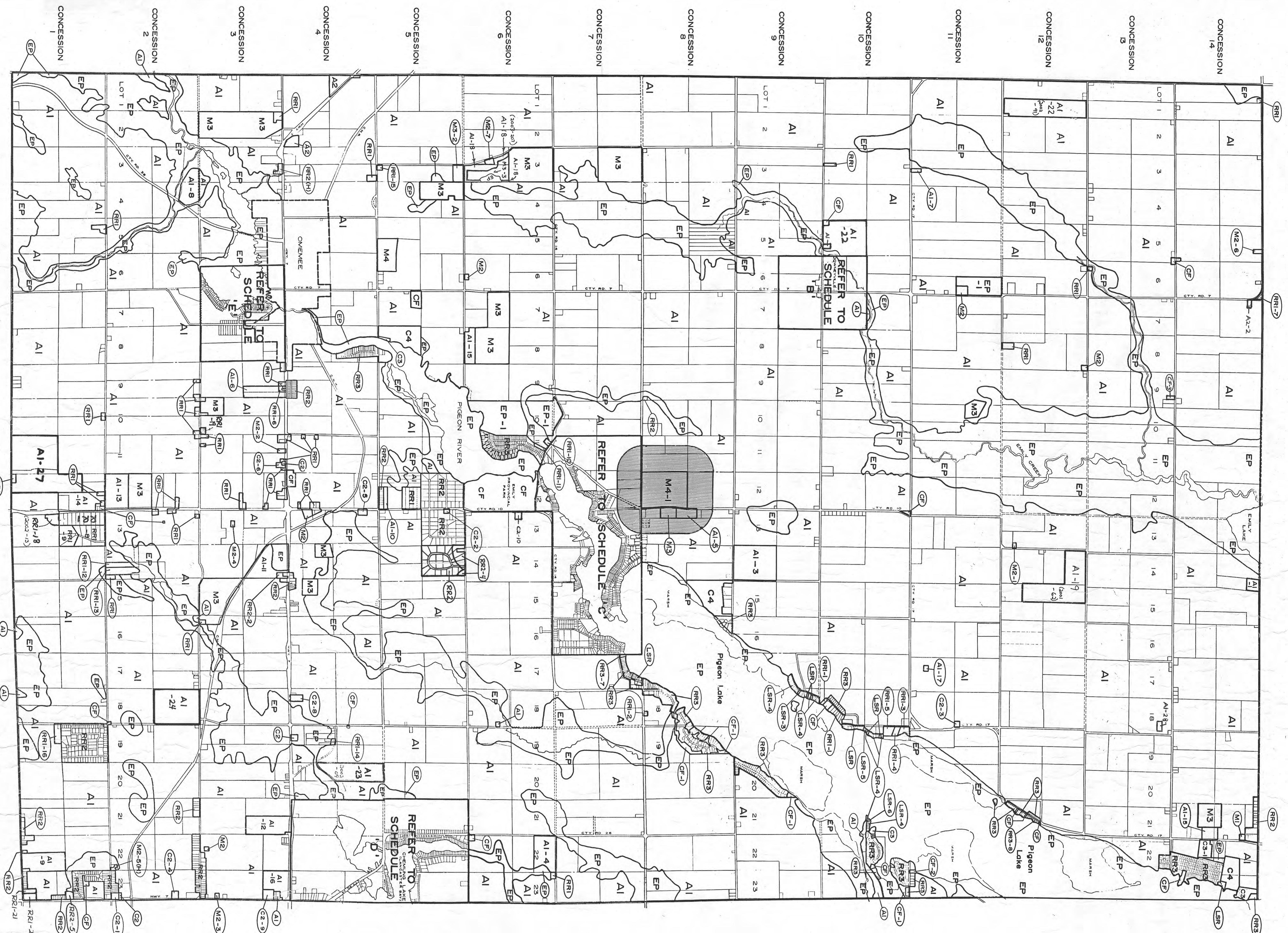
CONSOLIDATION JULY 2012

THIS SCHEDULE REFLECTS A DRAFT
CONSOLIDATION OF THE ACTUAL
BY-LAWS FOR COMPLETE ACCURACY.



ZONES

- EP — ENVIRONMENTAL PROTECTION ZONE
- CF — COMMUNITY FACILITY ZONE
- AI — AGRICULTURAL ZONE
- A2 — RURAL GENERAL ZONE
- HR — HAMLET RESIDENTIAL ZONE
- RRI — RURAL RESIDENTIAL TYPE ONE ZONE
- RR2 — RURAL RESIDENTIAL TYPE TWO ZONE
- RR3 — RURAL RESIDENTIAL TYPE THREE ZONE
- LSR — LIMITED SERVICE RESIDENTIAL ZONE
- C1 — GENERAL COMMERCIAL ZONE
- C2 — HIGHWAY COMMERCIAL ZONE
- C3 — RECREATION COMMERCIAL ZONE
- C4 — CAMPGROUND COMMERCIAL ZONE
- M1 — RESTRICTED INDUSTRIAL ZONE
- M2 — GENERAL INDUSTRIAL ZONE
- M3 — EXTRACTIVE INDUSTRIAL ZONE
- M4 — DISPOSAL INDUSTRIAL ZONE
- (H) — REFER TO SECTION 3.18.1.4
- (H) — ZONE BOUNDARY
- (H) — REFER TO SECTION 3.8



THIS IS SCHEDULE 'B' TO BY-LAW NO. 1996-30
AS AMENDED



DOWNEYVILLE AREA

Appendix H
Cross-Section Photo Inventory



Downstream



Upstream



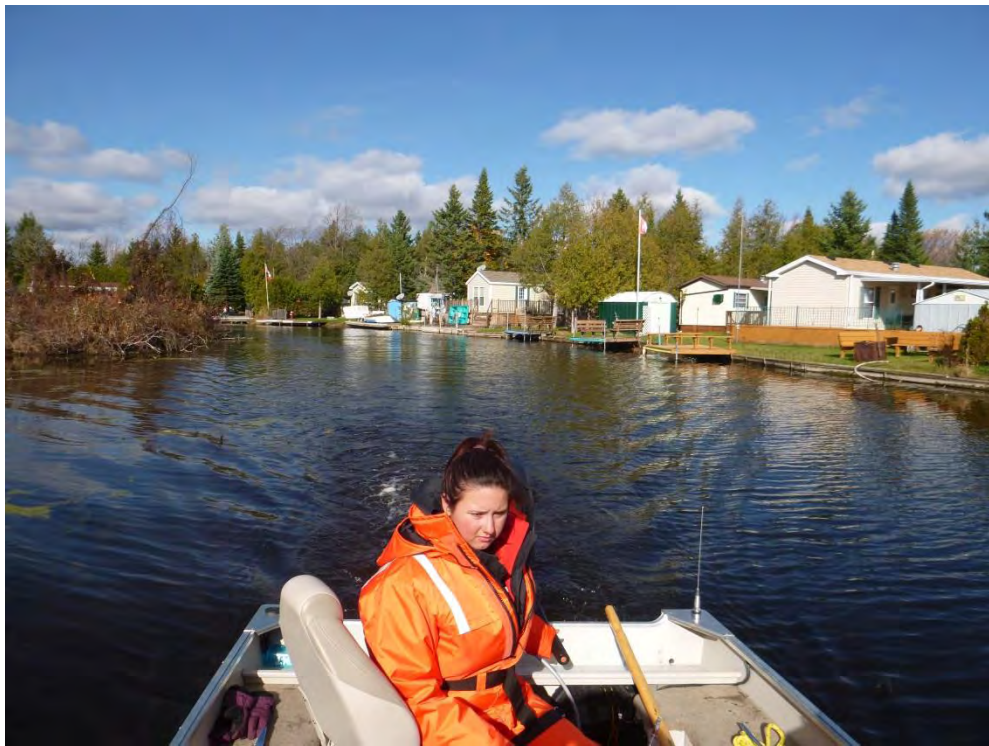
Downstream



Upstream



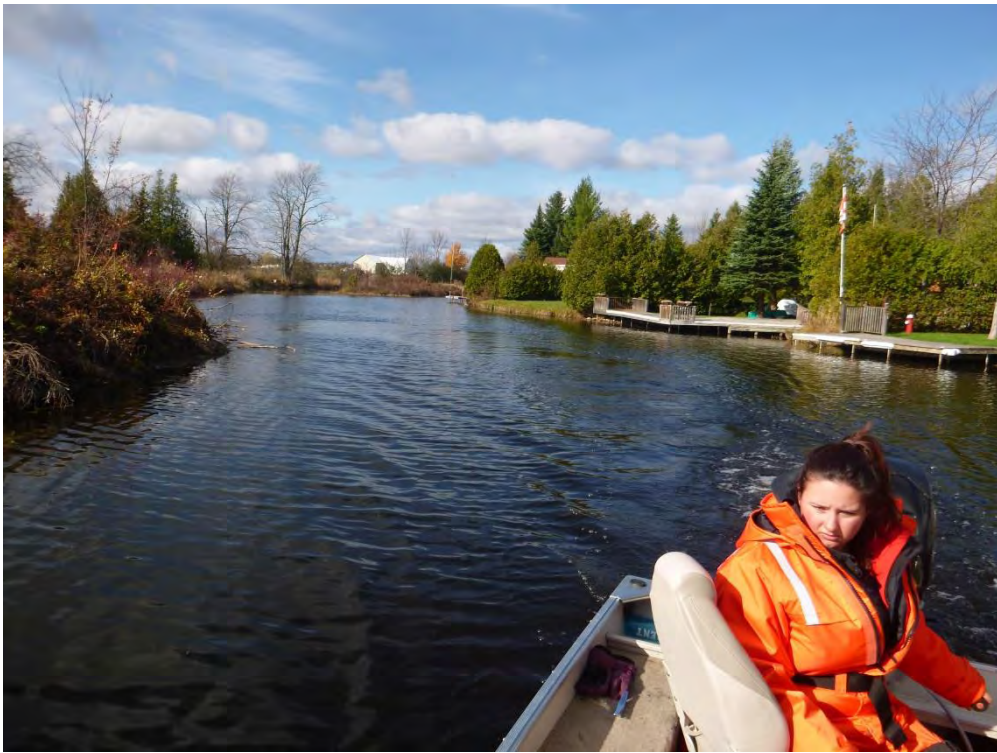
Downstream



Upstream



Downstream



Upstream



Downstream



Upstream

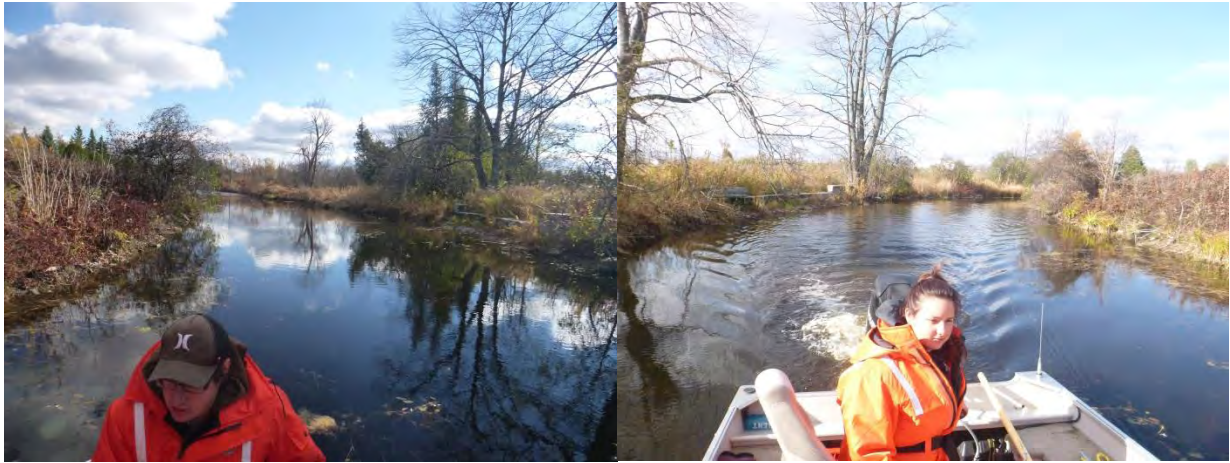
466, 487, 504



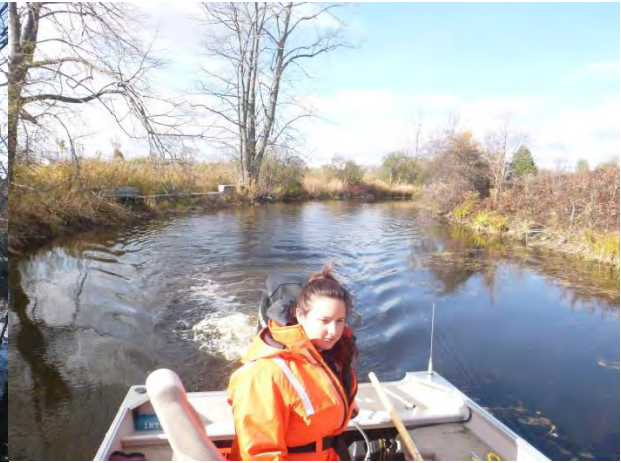
Downstream East Side



Upstream East Side



Downstream West Side



Upstream Westside



551



Downstream



Upstream

606



Downstream



Upstream



Downstream



Upstream

704



Downstream



Upstream

755, 760



Downstream



Upstream

767,774



Downstream



Upstream



Downstream



Upstream

883, 889



Downstream



Upstream

902, 935



Downstream



Upstream

935



Downstream



Upstream

970



Downstream



Upstream

978



Downstream



Upstream

1048



Downstream



Upstream

1111



Downstream



Upstream

1147



Downstream



Upstream

1162



Downstream



Upstream

1186, 1202



Downstream



Upstream

1222



Downstream



Upstream

1233, 1240



Downstream



Upstream

1259, 1269



Downstream



Upstream

1320, 1330



Downstream



Upstream

1395



Downstream



Upstream

1458



Downstream



Upstream

1497, 1508



Downstream



Upstream

1519, 1524



Downstream



Upstream

1534



Downstream



Upstream

1590



Downstream



Upstream

1699, 1767



Downstream



Upstream

1801, 1815, 1823



Downstream



Upstream

1843, 1851



Downstream



Upstream

1944



Downstream



Upstream

1997



Downstream



Upstream

2262



Downstream



Upstream

2570



Downstream



Upstream

2886, 2900



Downstream



Upstream

2915, 2930



Downstream



Upstream

2985, 2997, 3007



Downstream



Middle



Upstream

3127



Downstream



Upstream

3233



Downstream



Upstream

3289



Downstream



Upstream

3445, 3483, 3492



Downstream



Upstream

3510, 3533



Downstream



Upstream

Appendix I
Structure Photo Inventory Record

Dunsford Creek

Structure Photo Inventory

April 2017



List of Figures

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Structure 6: Dunsford Community Centre Crossing.....9

Structure 7: Dunsford Culvert.....10

Structure 1: Heron's Landing South Crossing

HecRas #: 763

Upstream Invert Elevation: 247.638 m

Downstream Invert Elevation: 247.011 m

Structure Length: 3.035 m

Span: 13.43 m

Rise: 1.28 m

Bridge/Shape: Pedestrian Bridge

Material: Steel and Concrete

Bottom Material: Concrete Pad



Upstream facing Downstream



Downstream facing Upstream



Looking Upstream under Bridge

Structure 2: Heron's Landing North Crossing

HecRas #: 891

Upstream Invert Elevation: 247.439 m

Downstream Invert Elevation: 247.444 m

Structure Length: 4.649 m

Span: 5.2 m

Rise: 1.97 m

Culvert Type/Shape: Bridge

Material: Concrete/Wood/Railway Ties

Bottom Material: Open Bottom



Upstream facing Downstream



Downstream facing Upstream



Upstream end of Culvert

Structure 3: Culvert Under Hwy 36 (E)

HecRas #: 1249

Upstream Invert Elevation: 250.343 m

Downstream Invert Elevation: 250.127 m

Structure Length: 16.276 m

Span: 6.85 m

Rise: 1.95 m

Culvert Type/Shape: Box (Rectangular)

Material: Concrete

Bottom Material: Open Bottom



Upstream facing Downstream



Upstream end of Culvert



Downstream facing Upstream

Structure 4: Culvert under Cedar Glen Road

HecRas #: 1513

Upstream Invert Elevation: 253.342 m

Downstream Invert Elevation: 253.247 m

Structure Length: 9.575 m

Span: 4.00 m

Rise: 2.1 m

Culvert Type/Shape: Pipe Arch

Material: Corrugated Galvanized Steel/Concrete

Bottom Material: Open Bottom/Bedrock



Upstream facing Downstream



Downstream facing Upstream



Upstream end of Culvert

Structure 5: Culvert Under Hwy 36 U/S (W)

HecRas #: 1834

Upstream Invert Elevation: 256.448 m

Downstream Invert Elevation: 256.37 m

Structure Length: 16.66m

Span: 6.0m

Rise: 2.5 m

Culvert Type/Shape: Box (Rectangular)

Material: Concrete

Bottom Material: Open Bottom



Upstream Facing Downstream



Downstream facing Upstream



Upstream end of Culvert

Structure 6: Dunsford Community Centre Crossing

HecRas #: 2906

Upstream Invert Elevation A: 267.311 m
Downstream Invert Elevation A: 267.303 m

Upstream Invert Elevation B: 267.337 m
Downstream Invert Elevation B: 267.309 m

Upstream Invert Elevation C: 267.38 m
Downstream Invert Elevation C: 267.363 m

Structure Length A: 11.543 m
Structure Length B: 9.885 m
Structure Length C: 9.28 m

Span A: 0.86 m
Rise A: 0.84 m

Span B: 0.90 m
Rise B: 0.83 m

Span C: 0.90 m
Rise C: 0.77 m

Culvert Type/Shape: Corrugated Metal/Circular

Material: Corrugated Galvanized Steel

Bottom Material: Same as Tops and Sides



Downstream facing Upstream



Upstream facing Downstream



Upstream end of Culverts

Structure 7: Culvert under Sturgeon Raod

HecRas #: 3503

Upstream Invert Elevation: 269.247 m

Downstream Invert Elevation: 269.132 m

Structure Length: 15.709 m

BOX DIMENSIONS

Span: 4.9 m

Rise: 1.53 m

Culvert Type/Shape: Arch with box extensions

Material: Concrete

Bottom Material: Open Bottom



Upstream Facing Downstream



Downstream facing Upstream



Upstream end of Culvert

Appendix J
Sensitivity Analyses - Hydraulic

Hydraulic Sensitivity Analyses

The hydraulic model was tested for sensitivity to input parameters in the list below. Input parameters were modified by varying degrees as outlined below for the Regional Storm event only (Timmins Event). The increase/decrease in flood elevation from the base scenario were noted to establish a level of confidence in flood elevation estimations. The following parameters were tested for sensitivity:

- Manning roughness coefficient (+/- 20%)
- Peak Regulatory Flow (+/- 30%)
- Downstream Boundary Condition (+/- 1.0 m)

Manning roughness coefficient

Flood elevations throughout the project reach were investigated to determine the impact of changing the Manning roughness coefficient. The Manning's number indicates the friction factor in a cross section. The higher the number, the rougher is the surface against which water flows. For instance, a smooth concrete pipe has a Manning's n of 0.013 whereas a forest has a Manning's n value of 0.1.

By increasing the Manning's n by 20%, the flow is being subject to a watercourse with greater friction forces acting upon it. It was found that the average increase in the regional water surface elevation throughout the 83 cross section was 5 cm, and the highest was 20 cm, at cross section 2570.

By decreasing the Manning's n by 20%, the flow is being subject to a watercourse with lower friction forces acting upon it. It was found that the average decrease in the regional water surface elevation throughout the 83 cross section was 5 cm, and the greatest was 31 cm, at cross section 1997.9.

Due to a minimal affect on the average, overall flood elevation throughout the study reach, it can be determined that the Manning roughness coefficients are acceptable.

Peak Regulatory Flow

Flood elevations throughout the project reach were investigated to determine the impact of changing the regional (Timmins Storm) peak flows. This was completed to account for uncertainty and assumptions as per the hydrologic modelling. From the hydrology sensitivity analysis, regional peak flow varied by up to 27%, therefore peak flows within the hydraulic model were varied by +/-30%.

By increasing the peak flows, it was found that the average increase in regional flood elevation throughout the 83 cross sections was 19 cm, with the highest greatest of 79 cm at cross section 1147. Cross section 1147 has a relatively narrow cross section, with limited floodplain access. Therefore, increases in flood elevations are significant due to an entrenched channel.

By decreasing the peak flows, it was found that the average decrease in regional flood elevation throughout the 83 cross sections was 24 cm, with the greatest decrease of 65 cm at cross section 1233.

Cross section 1233 is located immediately downstream of the Highway 36 bridge crossing. During the base scenario, Timmins flood elevation is immediately above an ineffective flow area

(associated with the bridge). As flows are reduced, the flood elevation decreases below the ineffective flow area, causing flood elevations to decrease significantly.

While the flood elevations are somewhat sensitive to the peak flow rate, the variability of 30% in peak flow is also significant. Therefore, with lower assumptions on variability of peak flow, the flood elevations are considered reasonable.

Downstream Boundary Condition

The Dunsford Creek flows into the Emily Creek, a tributary to Sturgeon Lake. Due to the lack of known water levels immediately at the confluence of Dunsford Creek and Emily Creek, a downstream boundary condition was based on the Sturgeon Lake normal operating level of 247.76 m, as a flow gauge is located approximately 10.5 km north easterly in Bobcaygeon.

Due to the uncertainty of the starting water elevation, a sensitivity analysis was completed by varying the starting water level by +/- 1.0m. For most of the cross sections, the regional flood elevation remained unchanged. When increasing the downstream boundary condition to 248.76m, only the 10 downstream cross sections had a change in flood elevations, with an average of 32 cm through these sections. The limit of this backwater effect ends at cross section 755.

The most downstream cross section (181) has a channel invert of 246.59 m. Therefore, when decreasing the downstream boundary condition to 246.76 m. The most downstream cross section's flood elevation decreased by 16 cm with the remainder unchanged.

Due to the limited effects on flood elevations throughout the entire watershed, the starting water elevation is considered acceptable for the study area.

HEC-RAS Cross Section	Base (m)	Regional Flood Elevation (m)						Delta (from Base)					
		Discharge		Downstream Boundary Condition		Manning n		Discharge		Downstream Boundary Condition		Manning n	
		+30%	-30%	+1.0m	-1.0m	+20%	-20%	+30%	-30%	+1.0m	-1.0m	+20%	-20%
3532	272.00	272.18	271.83	272.00	272.00	272.01	272.00	0.18	-0.17	0.00	0.00	0.01	0.00
3510	271.56	271.69	271.32	271.56	271.56	271.56	271.56	0.13	-0.24	0.00	0.00	0.00	0.00
3492	271.35	271.59	271.07	271.35	271.35	271.48	271.21	0.24	-0.28	0.00	0.00	0.13	-0.14
3483	271.35	271.58	271.07	271.35	271.35	271.47	271.21	0.23	-0.28	0.00	0.00	0.12	-0.14
3446	271.33	271.56	271.06	271.33	271.33	271.46	271.19	0.23	-0.27	0.00	0.00	0.13	-0.14
3445	271.30	271.54	271.01	271.30	271.30	271.43	271.15	0.24	-0.29	0.00	0.00	0.13	-0.15
3289	271.05	271.29	270.73	271.05	271.05	271.17	270.89	0.24	-0.32	0.00	0.00	0.12	-0.16
3233	270.90	271.13	270.60	270.90	270.90	271.01	270.75	0.23	-0.30	0.00	0.00	0.11	-0.15
3127	270.40	270.58	270.21	270.40	270.40	270.51	270.34	0.18	-0.19	0.00	0.00	0.11	-0.06
3007	270.35	270.51	270.17	270.35	270.35	270.38	270.34	0.16	-0.18	0.00	0.00	0.03	-0.01
2985	270.34	270.49	270.17	270.34	270.34	270.36	270.33	0.15	-0.17	0.00	0.00	0.02	-0.01
2930	270.31	270.45	270.14	270.31	270.31	270.31	270.31	0.14	-0.17	0.00	0.00	0.00	0.00
2915	270.28	270.40	270.13	270.28	270.28	270.28	270.28	0.12	-0.15	0.00	0.00	0.00	0.00
2900	269.60	269.82	269.34	269.60	269.60	269.57	269.57	0.22	-0.26	0.00	0.00	-0.03	-0.03
2886	269.08	269.31	268.80	269.08	269.08	269.20	269.08	0.23	-0.28	0.00	0.00	0.12	0.00
2571	267.43	267.67	267.07	267.43	267.43	267.58	267.36	0.24	-0.36	0.00	0.00	0.15	-0.07
2570	266.39	266.60	266.22	266.39	266.39	266.59	266.24	0.21	-0.17	0.00	0.00	0.20	-0.15
2264	266.05	266.20	265.78	266.05	266.05	266.05	266.05	0.15	-0.27	0.00	0.00	0.00	0.00
2263.7	265.76	265.87	265.56	265.76	265.76	265.83	265.63	0.11	-0.20	0.00	0.00	0.07	-0.13
2263.4	265.36	265.54	265.18	265.36	265.36	265.47	265.36	0.18	-0.18	0.00	0.00	0.11	0.00
2263	264.89	265.07	264.66	264.89	264.89	264.89	264.89	0.18	-0.23	0.00	0.00	0.00	0.00
2262	263.04	263.29	262.79	263.04	263.04	263.11	262.99	0.25	-0.25	0.00	0.00	0.07	-0.05
1998	262.59	262.88	262.22	262.59	262.59	262.70	262.59	0.29	-0.37	0.00	0.00	0.11	0.00
1997.9	262.43	262.80	262.03	262.43	262.43	262.58	262.12	0.37	-0.40	0.00	0.00	0.15	-0.31
1997.8	261.95	262.29	261.69	261.95	261.95	261.95	261.95	0.34	-0.26	0.00	0.00	0.00	0.00
1997.7	261.85	262.07	261.37	261.85	261.85	261.85	261.85	0.22	-0.48	0.00	0.00	0.00	0.00
1997	260.12	260.36	259.70	260.12	260.12	260.12	260.12	0.24	-0.42	0.00	0.00	0.00	0.00
1944	260.12	260.36	259.64	260.12	260.12	260.12	260.12	0.24	-0.48	0.00	0.00	0.00	0.00
1851	260.12	260.36	259.64	260.12	260.12	260.12	260.12	0.24	-0.48	0.00	0.00	0.00	0.00
1818	260.10	260.34	259.62	260.10	260.10	260.10	260.10	0.24	-0.48	0.00	0.00	0.00	0.00
1816.1	258.07	258.20	257.77	258.07	258.07	258.07	258.07	0.13	-0.30	0.00	0.00	0.00	0.00
1815	257.94	258.03	257.77	257.94	257.94	257.94	257.94	0.09	-0.17	0.00	0.00	0.00	0.00
1767	257.39	257.51	257.17	257.39	257.39	257.46	257.23	0.12	-0.22	0.00	0.00	0.07	-0.16
1699	256.91	257.06	256.88	256.91	256.91	257.03	256.91	0.15	-0.03	0.00	0.00	0.12	0.00
1590	256.36	256.46	256.04	256.36	256.36	256.36	256.36	0.10	-0.32	0.00	0.00	0.00	0.00
1534	256.13	256.21	256.04	256.13	256.13	256.13	256.13	0.08	-0.09	0.00	0.00	0.00	0.00
1499	256.13	256.21	256.04	256.13	256.13	256.13	256.13	0.08	-0.09	0.00	0.00	0.00	0.00
1498	255.30	255.44	255.07	255.30	255.30	255.30	255.30	0.14	-0.23	0.00	0.00	0.00	0.00
1458	253.97	254.15	253.88	253.97	253.97	254.01	253.93	0.18	-0.09	0.00	0.00	0.04	-0.04
1395	253.97	254.15	253.88	253.97	253.97	254.01	253.93	0.18	-0.09	0.00	0.00	0.04	-0.04
1242	253.97	254.15	253.88	253.97	253.97	254.01	253.93	0.18	-0.09	0.00	0.00	0.04	-0.04
1241.8	253.97	254.14	253.88	253.97	253.97	254.00	253.93	0.17	-0.09	0.00	0.00	0.03	-0.04
1241.6	253.95	254.12	253.87	253.95	253.95	253.99	253.92	0.17	-0.08	0.00	0.00	0.04	-0.03
1241.3	253.90	254.05	253.85	253.90	253.90	253.92	253.87	0.15	-0.05	0.00	0.00	0.02	-0.03
1241	253.87	253.99	253.84	253.87	253.87	253.87	253.87	0.12	-0.03	0.00	0.00	0.00	0.00
1240.9	253.87	253.99	253.84	253.87	253.87	253.87	253.87	0.12	-0.03	0.00	0.00	0.00	0.00
1240.7	253.87	253.99	253.84	253.87	253.87	253.87	253.87	0.12	-0.03	0.00	0.00	0.00	0.00
1240.6	253.87	253.99	253.84	253.87	253.87	253.87	253.87	0.12	-0.03	0.00	0.00	0.00	0.00
1233	253.55	253.80	252.90	253.55	253.55	253.59	253.53	0.25	-0.65	0.00	0.00	0.04	-0.02
1186	253.55	253.80	252.90	253.55	253.55	253.58	253.53	0.25	-0.65	0.00	0.00	0.03	-0.02
1162	253.40	253.62	252.75	253.40	253.40	253.43	253.38	0.22	-0.65	0.00	0.00	0.03	-0.02
1147	252.35	253.14	252.07	252.35	252.35	252.35	252.35	0.79	-0.28	0.00	0.00	0.00	0.00
1111	251.91	252.11	251.69	251.91	251.91	251.91	251.91	0.20	-0.22	0.00	0.00	0.00	0.00
1048	251.10	251.25	250.95	251.10	251.10	251.15	251.10	0.15	-0.15	0.00	0.00	0.05	0.00
978	250.89	251.02	250.73	250.89	250.89	250.91	250.87	0.13	-0.16	0.00	0.00	0.02	-0.02
970	250.69	250.84	250.54	250.69	250.69	250.69	250.69	0.15	-0.15	0.00	0.00	0.00	0.00
935	250.62	250.83	250.33	250.62	250.62	250.66	250.58	0.21	-0.29	0.00	0.00	0.04	-0.04
902	250.22	250.45	250.07	250.22	250.22	250.25	250.22	0.23	-0.15	0.00	0.00	0.03	0.00
893	250.22	250.45	250.07	250.22	250.22	250.25	250.22	0.23	-0.15	0.00	0.00	0.03	0.00
889	250.13	250.45	249.95	250.13	250.13	250.21	250.13	0.32	-0.18	0.00	0.00	0.08	0.00
883	250.05	250.19	249.87	250.05	250.05	250.08	250.02	0.14	-0.18	0.00	0.00	0.03	-0.03
839	250.05	250.19	249.87	250.05	250.05	250.08	250.02	0.14	-0.18	0.00	0.00	0.03	-0.03
774	249.97	250.10	249.81	249.97	249.97	249.98	249.97	0.13	-0.16	0.00	0.00	0.01	0.00
761	249.92	249.96	249.78	249.92	249.92	249.92	249.92	0.04	-0.14	0.00	0.00	0.00	0.00
760	249.44	249.59	249.08	249.44	249.44	249.44	249.44	0.15	-0.36	0.00	0.00	0.00	0.00
755	249.39	249.52	249.06	249.39	249.39	249.40	249.39	0.13	-0.33	0.00	0.00	0.01	0.00
704	249.24	249.44	248.90	249.29	249.24	249.37	249.10	0.20	-0.34	0.05	0.00	0.13	-0.14
657	249.1	249.28	248.76	249.17	249.10	249.24	248.89	0.18	-0.34	0.07	0.00	0.14	-0.21
606	248.88	249.09	248.62	248.98	248.88	249.01	248.71	0.21	-0.26	0.10	0.00	0.13	-0.17
551	248.76	248.96	248.51	248.93	248.76	248.89	248.65	0.20	-0.25	0.17	0.00	0.13	-0.11
504	248.76	248.96	248.49	248.93	248.76	248.86	248.65	0.20	-0.27	0.17	0.00	0.10	-0.11
487	248.7	248.95	248.42	248.92	248.71	248.82	248.58	0.25	-0.28	0.22	0.01	0.12	-0.12
466	248.6	248.85	248.30	248.88	248.60	248.74	248.41	0.25	-0.30	0.28	0.00	0.14	-0.19
437	248.38	248.52	248.18	248.82	248.38	248.53	248.20	0.14	-0.20	0.44	0.00	0.15	-0.18
247	248.11	248.28	247.95	248.80	248.12	248.17	248.05	0.17	-0.16	0.69	0.01	0.06	-0.06
181	247.76	247.76	247.76	248.76	247.60	247.76	247.76	0.00	0.00	1.00	-0.16	0.00	0.00

Appendix K
HEC – RAS Output

Main Channel	1816.1	100Yr-SCS-	19.84	256.21	257.63	257.2	257.71	0.002118	1.34	17.37	29.44
Main Channel	1815	100Yr-SCS-	21.23	256.27	257.46	257.46	257.66	0.008647	2.41	14.97	41.36
Main Channel	1767	100Yr-SCS-	21.23	255.81	256.81	256.67	256.93	0.007016	1.57	13.53	25.08
Main Channel	1699	100Yr-SCS-	21.23	255.24	256.24	256.13	256.42	0.008394	1.9	11.21	18.56
Main Channel	1590	100Yr-SCS-	21.23	254.34	255.77	255.35	255.88	0.003113	1.48	14.36	15.7
Main Channel	1534	100Yr-SCS-	21.23	253.4	255.84		255.84	0.000041	0.3	137.26	181.79
Main Channel	1499	100Yr-SCS-	21.23	253.39	255.84	254.49	255.84	0.000047	0.32	151.49	213.57
Main Channel	1498.5	Cedar Glen Rd	Culvert								
Main Channel	1498	100Yr-SCS-	21.3	253.25	254.47	254.47	254.86	0.013979	2.76	7.7	9.86
Main Channel	1458	100Yr-SCS-	21.3	252.6	253.28	253.28	253.52	0.015364	2.2	9.91	21.13
Main Channel	1395	100Yr-SCS-	21.3	251.76	253.04		253.08	0.00096	0.92	24.8	26.7
Main Channel	1242	100Yr-SCS-	21.3	252.19	253.01		253.07	0.002177	1.02	21.06	32.11
Main Channel	1241.8	100Yr-SCS-	21.3	252.22	252.99		253.04	0.002482	1.04	20.92	34.49
Main Channel	1241.6	100Yr-SCS-	21.3	252.26	252.95		253.01	0.002848	1.08	19.88	34.32
Main Channel	1241.3	100Yr-SCS-	21.3	252.24	252.71	252.71	252.9	0.016482	1.96	10.94	28.45
Main Channel	1241	100Yr-SCS-	21.3	250.96	252.2	252	252.43	0.006915	2.13	10.02	11.26
Main Channel	1240.9	100Yr-SCS-	21.3	250.99	252.21	251.94	252.35	0.00483	1.65	12.92	16.85
Main Channel	1240.7	100Yr-SCS-	21.3	250.78	252.18		252.22	0.001292	0.93	22.95	26.4
Main Channel	1240.6	100Yr-SCS-	21.3	250.34	252.17	251.39	252.21	0.000998	0.87	24.51	169.06
Main Channel	1237.34	Cty Rd 36 (E)	Culvert								
Main Channel	1233	100Yr-SCS-	21.3	250.29	251.98	251.67	252.13	0.004217	1.72	12.4	26.79
Main Channel	1186	100Yr-SCS-	21.48	250.49	251.91	251.52	251.96	0.001725	1.28	23.37	28.03
Main Channel	1162	100Yr-SCS-	21.48	250.32	251.75		251.9	0.003849	2.02	13.87	15.39
Main Channel	1147	100Yr-SCS-	21.48	249.79	251.29	251.29	251.78	0.013269	3.16	7.29	7.86
Main Channel	1111	100Yr-SCS-	21.48	249.81	251.03	250.9	251.34	0.008054	2.48	9.1	10.85
Main Channel	1048	100Yr-SCS-	21.48	249.35	250.53	250.53	250.78	0.010055	2.75	12.23	27.42
Main Channel	978	100Yr-SCS-	21.48	248.99	250.37		250.45	0.002726	1.67	25.4	50
Main Channel	970	100Yr-SCS-	21.48	248.72	250.2	250.2	250.41	0.007427	2.41	16.29	40.44
Main Channel	935	100Yr-SCS-	21.48	248.52	249.75		249.88	0.004794	2.07	18.68	53.94
Main Channel	902	100Yr-SCS-	21.48	248	249.7		249.79	0.001734	1.38	16.82	21.22
Main Channel	893	100Yr-SCS-	21.48	247.44	249.69	248.83	249.77	0.001396	1.29	19.75	31.17
Main Channel	891	Heron's Landing	Bridge								
Main Channel	889	100Yr-SCS-	21.48	247.44	249.47	249.13	249.73	0.007865	2.3	10.27	22.35
Main Channel	883	100Yr-SCS-	21.48	247.44	249.5	249.12	249.65	0.003721	1.76	15.38	40.91
Main Channel	839	100Yr-SCS-	21.48	247.67	249.55		249.57	0.000415	0.65	41.13	59.28

Main Channel	774	100Yr-SCS-	21.48	247.33	249.52		249.54	0.000395	0.74	42.66	64.35
Main Channel	761	100Yr-SCS-	21.48	247.64	249.51	248.71	249.54	0.000546	0.8	37.65	58.27
Main Channel	760.5	Heron's Landir	Bridge								
Main Channel	760	100Yr-SCS-	21.48	247.01	248.7	248.26	248.86	0.004161	1.81	11.9	11.29
Main Channel	755	100Yr-SCS-	21.33	247.16	248.44	248.44	248.77	0.014165	2.58	8.27	12.1
Main Channel	704	100Yr-SCS-	21.33	247.07	248.26		248.32	0.001669	1.12	19.1	20
Main Channel	657	100Yr-SCS-	21.33	246.41	248.19	247.46	248.25	0.001305	1.14	18.75	16.13
Main Channel	606	100Yr-SCS-	21.33	246.22	248.11	247.38	248.18	0.001426	1.17	18.27	15.82
Main Channel	551	100Yr-SCS-	21.33	246.33	248.05	247.29	248.11	0.001191	1.09	19.72	17.49
Main Channel	504	100Yr-SCS-	21.33	246.66	248.01		248.05	0.001047	0.83	25.79	29.29
Main Channel	487	100Yr-SCS-	21.33	246.3	247.98		248.03	0.001262	0.95	22.39	23.62
Main Channel	466	100Yr-SCS-	21.33	246.46	247.91		247.99	0.002962	1.23	17.36	23.99
Main Channel	437	100Yr-SCS-	21.33	246.44	247.87	247.31	247.92	0.001317	1.02	20.88	20.66
Main Channel	247	100Yr-SCS-	21.33	245.81	247.8		247.81	0.000299	0.44	49.36	60.1
Main Channel	181	100Yr-SCS-	21.33	246.59	247.76	247.12	247.78	0.000616	0.6	35.53	45.46

Froude # Chl
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Main Channel	1816.1	Regional-Timmins	66.5	256.21	258.07	258.07	258.34	0.005047	2.6	41.87	80.72
Main Channel	1815	Regional-Timmins	70.95	256.27	257.94	257.94	258.18	0.008654	3.17	45.9	94.73
Main Channel	1767	Regional-Timmins	70.95	255.81	257.39	257.23	257.67	0.006545	2.38	32.47	79.72
Main Channel	1699	Regional-Timmins	70.95	255.24	256.91	256.91	257.24	0.006663	2.67	34.73	64.99
Main Channel	1590	Regional-Timmins	70.95	254.34	256.36	256.36	256.59	0.004499	2.34	49.66	116.87
Main Channel	1534	Regional-Timmins	70.95	253.4	256.13		256.14	0.000179	0.68	191	190.51
Main Channel	1499	Regional-Timmins	70.95	253.39	256.13	255.1	256.13	0.000204	0.74	216.88	236.03
Main Channel	1498.5	Cedar Glen Road	Culvert								
Main Channel	1498	Regional-Timmins	71.18	253.25	255.3	255.3	255.62	0.008296	2.83	37.76	138.88
Main Channel	1458	Regional-Timmins	71.18	252.6	253.89	253.89	254.4	0.01133	3.22	23.95	25.3
Main Channel	1395	Regional-Timmins	71.18	251.76	253.97		254.08	0.001171	1.54	59	53.63
Main Channel	1242	Regional-Timmins	71.18	252.19	253.97		254.06	0.001168	1.35	57.66	46.48
Main Channel	1241.8	Regional-Timmins	71.18	252.22	253.97		254.05	0.001085	1.28	61.74	50.56
Main Channel	1241.6	Regional-Timmins	71.18	252.26	253.95		254.03	0.001089	1.28	59.58	47.1
Main Channel	1241.3	Regional-Timmins	71.18	252.24	253.9		254.01	0.001558	1.51	50.19	37.39
Main Channel	1241	Regional-Timmins	71.18	250.96	253.73	252.97	253.96	0.002643	2.11	34.17	83.59
Main Channel	1240.9	Regional-Timmins	71.18	250.99	253.84	252.7	253.9	0.000631	1.19	78.61	158.2
Main Channel	1240.7	Regional-Timmins	71.18	250.78	253.87		253.88	0.000116	0.54	193.89	140.16
Main Channel	1240.6	Regional-Timmins	71.18	250.34	253.87	252.13	253.87	0.000015	0.21	465.7	260.59
Main Channel	1237.34	Cty Rd 36 (E)	Culvert								
Main Channel	1233	Regional-Timmins	71.18	250.29	253.55	252.48	253.69	0.00127	1.81	48.61	90.88
Main Channel	1186	Regional-Timmins	71.75	250.49	253.55	252.03	253.61	0.000584	1.33	73.35	33.11
Main Channel	1162	Regional-Timmins	71.75	250.32	253.4		253.58	0.001809	2.41	50.65	36.98
Main Channel	1147	Regional-Timmins	71.75	249.79	252.35	252.35	253.43	0.014277	4.9	17.57	13.19
Main Channel	1111	Regional-Timmins	71.75	249.81	251.91	251.91	252.4	0.007359	3.5	28.85	32.35
Main Channel	1048	Regional-Timmins	71.75	249.35	251.1	251.1	251.38	0.009101	3.51	38.98	61.72
Main Channel	978	Regional-Timmins	71.75	248.99	250.89		250.99	0.003125	2.26	70.81	108.34
Main Channel	970	Regional-Timmins	71.75	248.72	250.69	250.69	250.95	0.008001	3.24	46.32	95.59
Main Channel	935	Regional-Timmins	71.75	248.52	250.62		250.68	0.001752	1.82	84.2	129.46
Main Channel	902	Regional-Timmins	71.75	248	250.18	250.05	250.56	0.005217	2.96	33.31	49.16
Main Channel	893	Regional-Timmins	71.75	247.44	250.22	250.04	250.45	0.003371	2.44	46.08	68.65
Main Channel	891	Heron's Landing	Bridge								
Main Channel	889	Regional-Timmins	71.75	247.44	250.13	250.13	250.44	0.006728	2.96	37.4	59.58
Main Channel	883	Regional-Timmins	71.81	247.44	249.95	249.95	250.34	0.00766	3.19	36.62	49.11
Main Channel	839	Regional-Timmins	71.81	247.67	250.05		250.11	0.000977	1.24	84.23	99.9

Main Channel	774	Regional-Timmins	71.81	247.33	249.97		250.04	0.001074	1.45	84.4	115.75
Main Channel	761	Regional-Timmins	71.81	247.64	249.92	249.41	250.02	0.001801	1.72	67.68	99.93
Main Channel	760.5	Heron's Landing	Bridge								
Main Channel	760	Regional-Timmins	71.81	247.01	249.44	249.44	249.79	0.005749	2.85	34.85	51.95
Main Channel	755	Regional-Timmins	71.84	247.16	249.39	249.39	249.66	0.005069	2.55	42.36	82.74
Main Channel	704	Regional-Timmins	71.84	247.07	249.24		249.36	0.001427	1.64	53.61	47.39
Main Channel	657	Regional-Timmins	71.84	246.41	249.1	248.29	249.28	0.001914	1.98	49.69	58.63
Main Channel	606	Regional-Timmins	71.84	246.22	248.88	248.26	249.15	0.002946	2.32	32.57	44.87
Main Channel	551	Regional-Timmins	71.84	246.33	248.74	248.11	248.99	0.002834	2.24	34.45	41.52
Main Channel	504	Regional-Timmins	71.84	246.66	248.76		248.84	0.001575	1.33	59.33	67.11
Main Channel	487	Regional-Timmins	71.84	246.3	248.7		248.81	0.001918	1.52	60.35	121.16
Main Channel	466	Regional-Timmins	71.84	246.46	248.6		248.75	0.003555	1.79	48.48	91.97
Main Channel	437	Regional-Timmins	71.84	246.44	248.38	247.94	248.64	0.003826	2.25	33.05	53.36
Main Channel	247	Regional-Timmins	71.84	245.81	248.11		248.16	0.001403	1.02	72.62	91.31
Main Channel	181	Regional-Timmins	71.84	246.59	247.76	247.6	247.97	0.006993	2.02	35.53	45.46

Froude # Chl
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HEC-RAS Cross Section	Regional Flood Elevation (m)	100 Year Flood Elevation (m)
3532	272.00	271.28
3510	271.56	271.11
3503 Sturgeon Road	0.00	0.00
3492	271.35	270.55
3483	271.35	270.55
3446	271.33	270.55
3445	271.30	270.49
3289	271.05	270.19
3233	270.90	270.08
3127	270.40	269.83
3007	270.35	269.82
2985	270.34	269.82
2930	270.31	269.81
2915	270.28	269.81
2906 Community Centre	0.00	0.00
2900	269.60	268.74
2886	269.08	268.35
2571	267.43	266.53
2570	266.39	265.71
2264	266.05	265.33
2263.7	265.76	265.21
2263.4	265.36	264.83
2263	264.89	264.10
2262	263.04	262.15
1998	262.59	261.73
1997.9	262.43	261.47
1997.8	261.95	261.14
1997.7	261.85	260.93
1997	259.96	259.14
1944	260.11	258.34
1851	260.12	258.26
1818	260.10	258.23
1816.5 Cty Rd 36 (W)	0.00	0.00
1816.1	258.07	257.63
1815	257.94	257.46
1767	257.39	256.81
1699	256.91	256.24
1590	256.36	255.77
1534	256.13	255.84
1499	256.13	255.84
1498.5 Cedar Glen Road	0.00	0.00
1498	255.30	254.47
1458	253.89	253.28
1395	253.97	253.04
1242	253.97	253.01
1241.8	253.97	252.99

1241.6	253.95	252.95
1241.3	253.90	252.71
1241	253.73	252.20
1240.9	253.84	252.21
1240.7	253.87	252.18
1240.6	253.87	252.17
1237.34 Cty Rd 36 (E)	0.00	0.00
1233	253.55	251.98
1186	253.55	251.91
1162	253.40	251.75
1147	252.35	251.29
1111	251.91	251.03
1048	251.10	250.53
978	250.89	250.37
970	250.69	250.20
935	250.62	249.75
902	250.18	249.70
893	250.22	249.69
891 Heron's Landing	0.00	0.00
889	250.13	249.47
883	249.95	249.50
839	250.05	249.55
774	249.97	249.52
761	249.92	249.51
760.5 Heron's Landing	0.00	0.00
760	249.44	248.70
755	249.39	248.44
704	249.24	248.26
657	249.10	248.19
606	248.88	248.11
551	248.74	248.05
504	248.76	248.01
487	248.70	247.98
466	248.60	247.91
437	248.38	247.87
247	248.11	247.80
181	247.76	247.76